



FLOOD RISK AND DRAINAGE ASSESSMENT

**Cleator Mill,
Proposed Residential Development,
Flood Risk Assessment.**

Reference

RO/FRA/RES/19002.1

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Version

5

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CONTENTS

Confidentiality Statement

Document History

1.0	Executive summary	1
2.0	Introduction	2
3.0	The Site	3
4.0	Proposed development	3
5.0	Flood Risk	4
	River Ehen	4
	River Ehen – Climate Change Impact	8
	Flood History	10
	Flood Defence Overtopping	10
	Flood Defence Breaching	11
	Unnamed Watercourse to Northeast	14
	Surface Water Flooding	14
6.0	Recommended Development Area	18
7.0	Safe access and egress	19
8.0	Ground conditions	19
9.0	receiving waters	21
10.0	Surface Water Management Plan	22
	Soil Infiltration	22
11.0	Conclusions	23

APPENDICES

Appendix A	Site Location Plan
Appendix B	Strategic Flood Map
Appendix C	Topographical Survey and Site Sections
Appendix D	Flood Defence Survey
Appendix E	Envireau Water Breach Analysis
Appendix F	Watercourse Model
Appendix G	Environment Agency Flood Data
Appendix H	Topographical Survey
Appendix I	Overland Flow Route
Appendix J	Soil Infiltration Test Results

CONFIDENTIALITY STATEMENT

This report is addressed to and may be relied upon by the following:

Gleeson Regeneration Ltd
Rural Enterprise Centre
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This report has been prepared for the sole use and reliance of the above-named parties. This report shall not be relied upon or transferred to any other parties without the express written authorisation of RWO Associates Limited. No responsibility will be accepted where this report is used, either in its entirety or in part, by any other party.

DOCUMENT HISTORY

VERSION	PURPOSE/DESCRIPTION	DATE
1	Draft Issue – for client comment	04.11.2020
2	Amended following Environment Agency comments	12.07.2021
3	Amended following addition flood modelling, LLFA & EA comments.	31.08.2022
4	Updated to suit the revised layout and unnamed watercourse flood modelling.	21.06.2023
5	Site developable area amended and risk assessed for new area.	28.11.2023

1.0 EXECUTIVE SUMMARY

This assessment has looked at the implications of the proposed Residential developments in relation to flood risk, including breach analysis as agreed with the Environment Agency during meetings in June 2019.

The proposed development site is shown as being in Flood Zone 1.2 & 3a on the Environment Agency flood maps. When reviewing the defended flood modelling undertaken by the Environment Agency the site is afforded protection for all events up to and including the 1:200 year return period.

The flow rates and water levels for varying events have been considered including the upper central and higher and flow rates are comparable to the 1:1000 year return period, giving a clear indication of potential water levels on the site when looking at the modelled results.

It is proposed to only develop the site outside of the 1:1000yr modelled flood level. This will be subject to further overland flood modelling from the unnamed watercourse to the northeast, once an agreement on the developable area has been reached considering flood risk from the River Ehen.

The Environment Agency surface water flood maps have been reviewed against the topography with flows shown coming over the site in a low-risk event. When reviewing the contours and local topography we believe that surface water flows would follow the road, given the kerb phase and raised levels to the site on the boundary as opposed to running straight across the site. As such surface water overland flow can be managed with the route maintained around the perimeter of the development site.

Safe access and egress have been established via the new proposed access road onto the A5086. The overland flood flow routes do not impede the proposed access/egress for the development's new entrance.

The Environment Agency does not provide a Flood Warning Service for Cleator. It is noted that the site is covered by the River Ehen, Calder, Irt and Esk Flood Alert areas, it would therefore be recommended this be included within the homeowner's packs.

A Surface Water Management Plan (SWMP) has been identified including the levels of treatment required to ensure the River Ehen water quality remains protected.

Any potential impact of the development can be adequately addressed by good drainage design.

2.0 INTRODUCTION

RWO Associates Ltd (RWO) has been instructed by Gleeson Regeneration to prepare a Flood Risk Assessment to support a planning application for a proposed residential development at Cleator in Cumbria.

This assessment is reviewing the available information which includes;

- The Strategic Flood Risk Assessment.
- Environment Agency Flood Maps, including flood modelling information (River Ehen 2015 model, released in 2016)
- Envireau Water Breach Analysis.
- Envireau Water Flood Modelling from the unnamed main river to the Northeast.

This site is covered by a Strategic Flood Risk Assessment (by Jacobs dated 2007 and published on the local authority website [Strategic Flood Risk Assessment | Copeland Borough Council](#)) commissioned by Copeland Borough Council. This, more detailed, site-specific Flood Risk Assessment supplements the findings of the Strategic Flood Risk Assessment. It is also covered by the more recent Draft Copeland Borough Council, Level 1 SFRA. For clarity and reference purposes, this report has utilised the latest Draft SFRA dated 2018 to ensure the latest SFRA maps are utilised and considered as part of this FRA.

Envireau Water has been utilised to undertake a Breach Analysis of the existing flood defences located on the North and Eastern boundaries, with the locations agreed with the Environment Agency during a meeting in June 2019. Envireau Water has also modelled the flooding from the unnamed watercourse to the northeast of the development, which ultimately discharges into the River Ehen.

The site is currently Greenfield, and the client wishes to create residential development; location plans are included in Appendix A.

This report will review the risks associated with the River Ehen, the unnamed watercourse and other published risks. Recommendations as to the developable area and any mitigation requirements will also be made.

3.0 THE SITE

The proposed development site is located to the east of Cleator, about 300m to the south of Cleator Moor and immediately to the west of the Lake District National Park; Figure 1 below shows the site location.



Figure 1 – Site Location (Redline indicates approximate extents)

The River Ehen forms the eastern and southern boundary, with residential dwellings located to the west and north. To the immediate south of the proposed development site is the former Kangol factory, with the building varying in age between the early 19th Century and the 1960s. The original building was a linen mill in the 19th Century. The eastern portion of the site historically had a derelict factory located on it, which has since been demolished and it currently utilised as a Park & Ride. The A5086 is on the north-western boundary of the proposed development site.

4.0 PROPOSED DEVELOPMENT

It is proposed to consider the site for residential development and consider the number of dwellings that can be safely accommodated without increasing flood risk to others or creating a risk for the proposed development. Based upon the available information the extent of land ownership is located in Flood Zone 1, 2 & 3a, it is noted that the latest Environment Agency flood maps for planning identify the development site has flood defences located to the northeast and east. An extract of the

strategic flood map can be seen below in Figure 2 (area identified as E8) with the full map included in Appendix B.

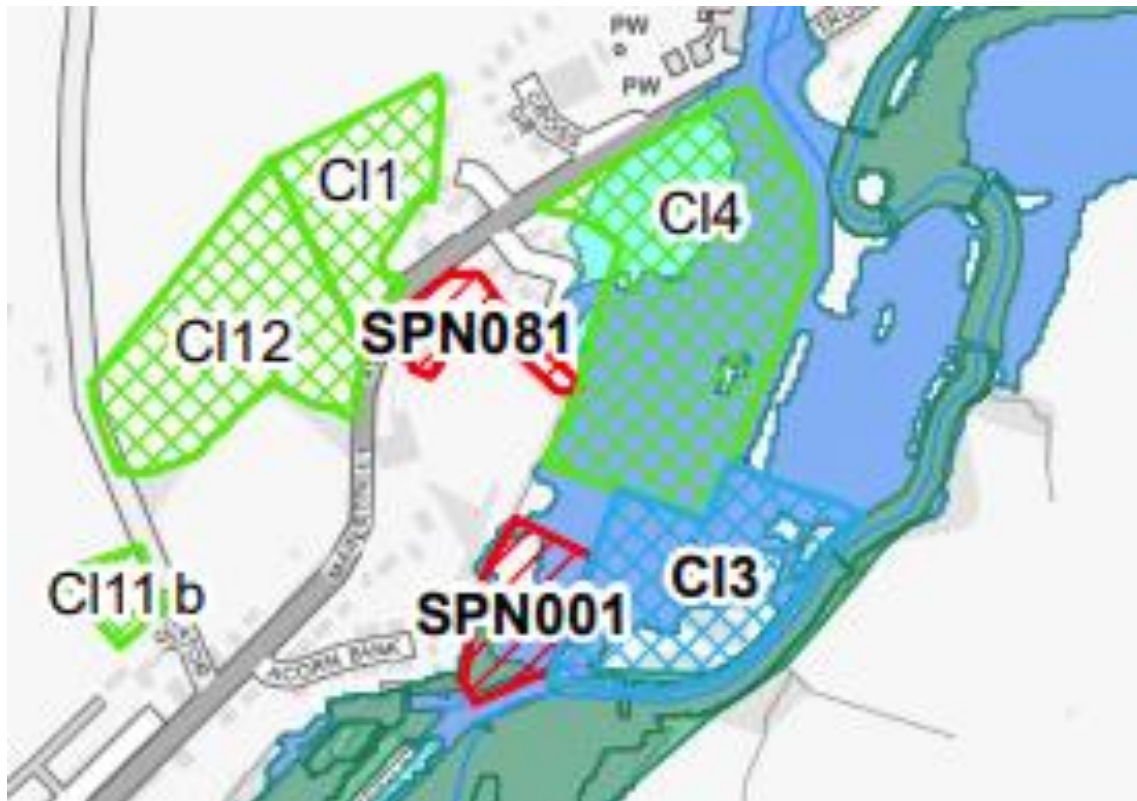


Figure 2 – Draft Copeland SFRA 2018 Extract

As the development site is shown as being located in Flood Zone 1, 2 and 3a with an annual probability of flooding of greater than 1:1000 year, between 1:100 and 1:1000 years and 1:100 years [$>1\%$], it will therefore be subject to the sequential and exception test in accordance with NPPF Technical Guidance should any development fall within flood zone 3a.

A topographical survey is included in Appendix C, along with site sections through the flood defences with the various flood levels indicated as taken from the Environment Agency Model.

5.0 FLOOD RISK

River Ehen

The site is located adjacent to the River Ehen, to the west, within flood zone 3a and 2 as identified by the Copeland Strategic Flood Risk Assessment, map included in Appendix B. Modelled flood levels have been reviewed based upon the Environment Agency hydraulic modelling with further breach analysis undertaken by Envireau Water on behalf of the developer, it is noted that the required climate change allowance has been amended since the agreement with the Environment Agency, therefore this has been reviewed separately as an extension to the breach analysis. Envireau Water has utilised the Environment Agency model from 2016, further details noted within the Envireau Water report are included in Appendix E. The unnamed watercourse to the northeast has also been modelled by Envireau Water and this has been included in Appendix F. The Environment Agency modelled flood levels are included below in Table 1.

Cross Section reference	10 Year	25 Year	50 Year	75 Year	100 Year	100+CC Year	200 Year	1000 Year
1896	63.74	63.852	63.898	63.941	63.972	64.029	64.7	64.939
1726	62.013	62.223	62.32	62.42	62.472	62.692	63.383	63.685
1806	63.052	63.284	63.418	63.553	63.621	63.823	63.779	64.135
1606	60.846	61.066	61.219	61.368	61.427	61.658	61.61	62.193
1502	60.275	60.504	60.626	60.744	60.808	61.001	60.953	61.398
1406	59.892	60.118	60.224	60.379	60.451	60.559	60.56	61.039
1299	59.379	59.549	59.64	59.733	59.775	59.912	60.56	61.039
1206	58.826	58.938	58.992	59.044	59.056	59.075	59.071	59.234

Table 1 – Modelled Flood Levels (defended)

Figure 3 below shows the positions of the modelled node cross sections referenced above;

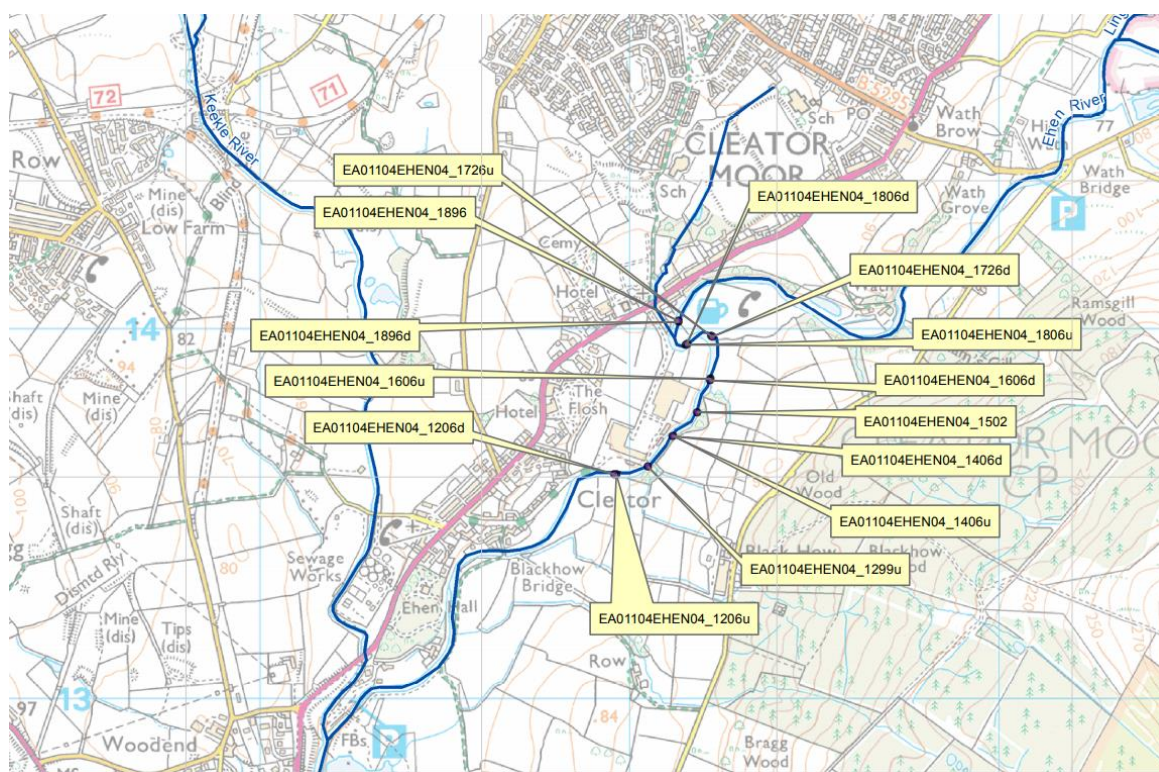


Figure 3 – Modelled Node Locations

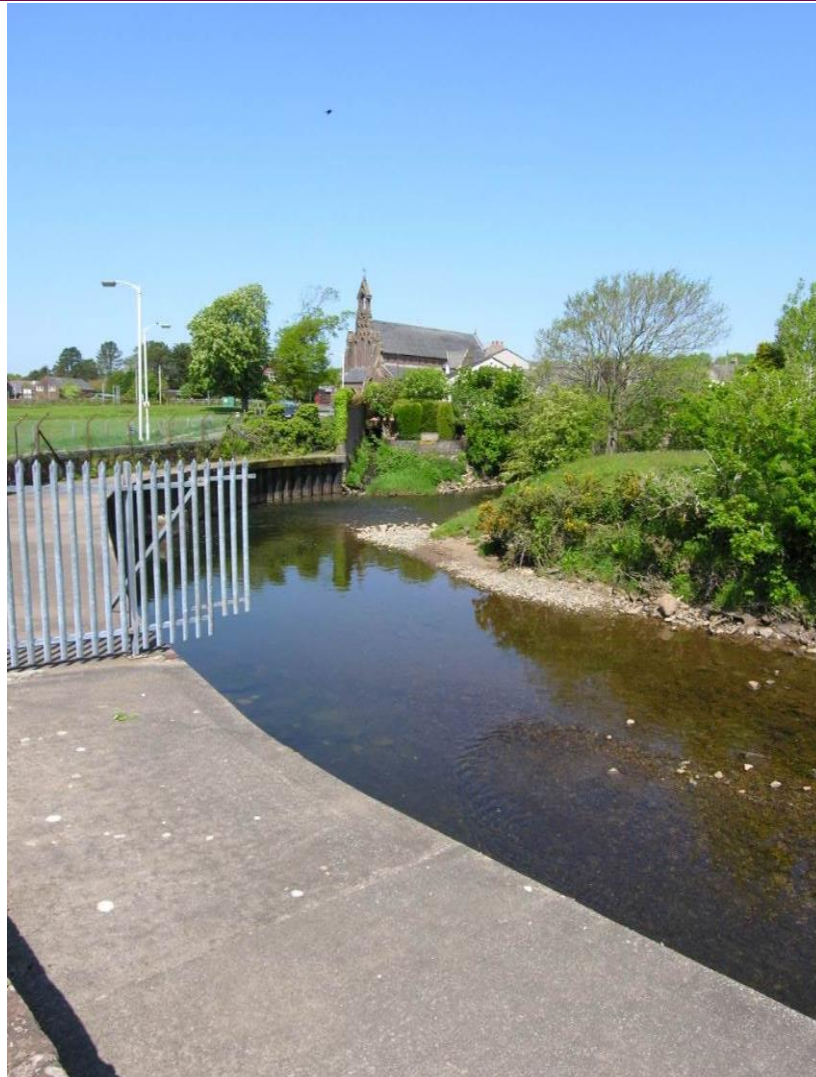


Photo 1 – Hard flood defences between 1896 & 1726

The proposed development has engineered hard flood defences to the northeastern extent, downstream of the hard defences, soft earth defences exist continuing north to the extents of the Kangol Factory/premises. These defences afford the site a level of protection to the 1:200-year modelled return period, which is confirmed by the Environment Agency River Ehen model from 2016. The location of the modelled reference points has been cross-referenced against a topographical survey undertaken; this is included in Appendix C; which includes sections showing the flood levels against the existing ground levels. Given the reliance of flood defences RAB Consultants were appointed to update the previous condition survey undertaken, A copy of the report is included in Appendix D.

The survey identifies various works which need undertaken immediately and within 1 year, it is recommended these works are carried out prior to works commencing, the total estimate value is £25,300 for the works as identified in the RAB report (RAB; 2869). It is then recommended that a condition survey be completed every 5 years as part of the management company's duties and the results are shared with the Environment Agency to ensure the flood defences are maintained and any further defects are rectified as part of the Environment Agencies' powers, should the Environment Agency deem that improvement/maintenance works necessary. At the most vulnerable point, on the northern boundary with the River Ehen hard defences are located on the right boundary located between modelled node points 1896 and 1726, as can be seen in Figure 3. The Environment Agency data shows these hard defences are at a 1:200-year standard. Based upon their model and information supplied as part of Product 4. These conditions are generally identified as being condition grade 2, which is a Good state of repair, except for some minor vegetation which is noted as condition grade 3. The vegetation should be dealt with and made good to ensure this

0.5% AEP Defended = No Data

0.5% AEP Defended = No Data

0.5% AEP Defended = No Data

0.5% AEP Defended = No Data

Flood water is shown as breaching the site on the 1 in the 1000 year return period, in the defended scenario impacting approximately 50% of the site as can be seen in the below extract;

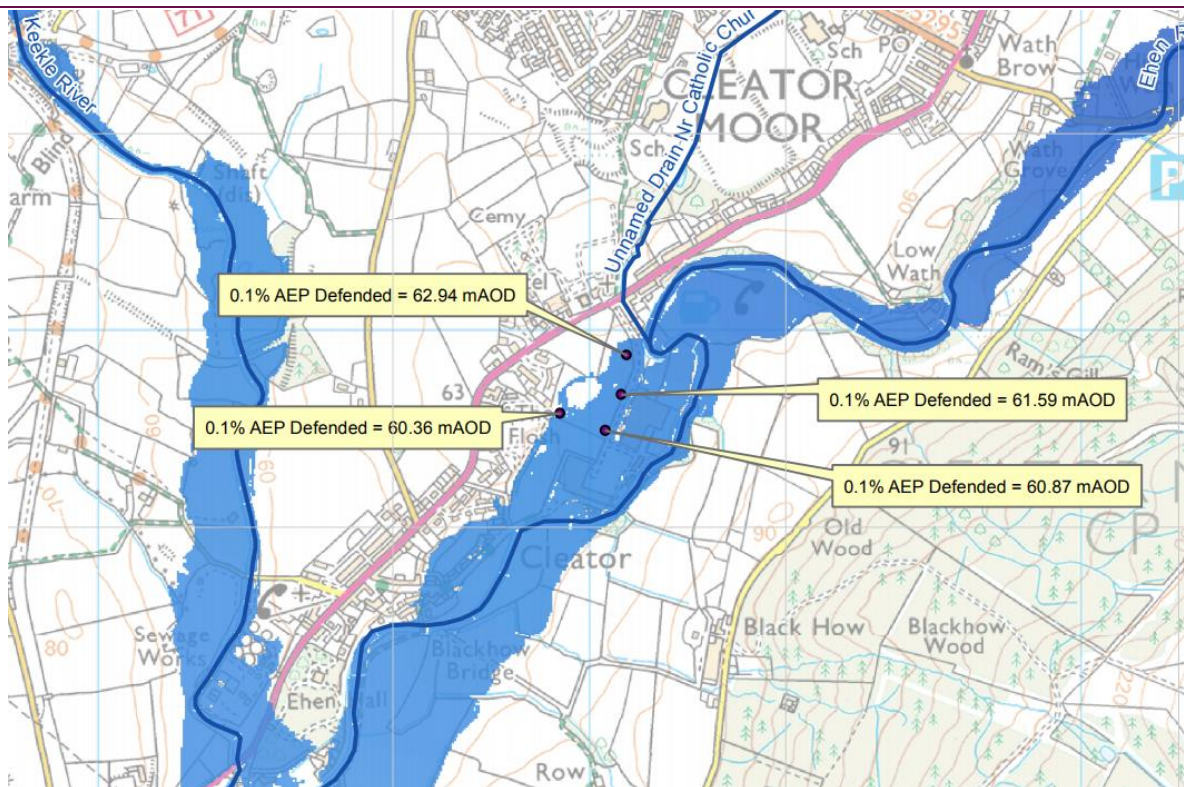


Figure 5 – Extract of Product 4 1:1000 Year return period flooding. Defended Scenario

Based upon the defended scenario the site is afforded protection to an equivalent standard as being located Flood Zone 2.

To assess the flood risk associated with the proposed development site climate change needs assessing under the Environment Agency guidance for Southwest Lakes Management Catchment with a 30% central allowance requiring consideration.

River Ehen – Climate Change Impact

As per the Environment Agency request, the higher central and upper-end allowances for the North West river basin district has been considered. As there is not an Environment Agency model for these climate change uplifts this has been calculated utilising the available data from the Environment Agency data and then compared for sensitivity based upon the peak flow rate increase against the 100-year return period event and comparing the calculated water level.

Node Reference	Water Level	Flow	Water Level	Flow	Flow	Water Level
	100yr	100yr	100yr + 20%CC	100yr + 20%CC	1% increase	1% increase
1896	63.972	96.513	64.029	101.484	0.24855	0.00285
1726	62.472	127.207	62.692	143.88	0.83365	0.011
1806	63.621	91.358	63.823	93.242	0.0942	0.0101
1606	61.427	126.737	61.666	145.965	0.9614	0.01195
1502	60.808	129.137	61.001	151.25	1.10565	0.00965
1406	60.451	128.097	60.559	149.927	1.0915	0.0054
Values taken from Environment Agency Model						

Table 2 – Climate Change increase of water level and flow for each 1% from 100yr to 100yr + 20% CC

Table 2 above shows the increase for each 1% uplift of climate change from the 100 year return period to the 100 year plus 20% climate change, in accordance with the Environment Agency requirements the central 30% climate change will be calculated.

South West Lakes Management Catchment peak river flow allowances (X)

	Central	Higher	Upper
2020s	12%	14%	22%
2050s	17%	23%	38%
2080s	30%	39%	63%

Extract 1 – Table 1: peak river flow allowances by river basin district

	Water Level	Flow	Water Level	Flow	Water Level	Flow	Flow	Water Level	Flow	Water level Increase
	100yr	100yr	100yr + 20%CC	100yr + 20%CC	100yr + 30%CC	100yr + 30%CC	1000yr	1000yr	1000yr vs 100 yr + 30% CC	1000yr vs 100 yr + 30% CC
1896	63.972	96.513	64.029	101.484	64.0575	103.9695	147.259	64.939	-43.2895	-0.8815
1726	62.472	127.207	62.692	143.88	62.802	152.2165	173.534	63.685	-21.3175	-0.883
1806	63.621	91.358	63.823	93.242	63.924	94.184	100.247	64.135	-6.063	-0.211
1606	61.427	126.737	61.666	145.965	61.7855	155.579	165.107	62.193	-9.528	-0.4075
1502	60.808	129.137	61.001	151.25	61.0975	162.3065	198.323	61.398	-36.0165	-0.3005
1406	60.451	128.097	60.559	149.927	60.613	160.842	202.596	61.039	-41.754	-0.426

Values taken from Environment Agency Model

Table 3 – Climate Change increase of 30% as per central value in Extract 1 above.

Table 3 above gives the increased flow rate for the climate change variation which increases the applied climate change in the River Ehen model from 20% to 30% in accordance with current guidance. The calculated increase in water depth and a comparison between the modelled Environment Agency 1000-year return period and the calculated 100-year plus 30% climate change. It is worth noting that the calculated water level for the 100-year plus 30% Climate Change is a linear arrangement and assumes the channel profile remains as the water level for the 100-year modelled return period, on this basis, the approach is conservative as the channel, in reality, widens when looking at the surrounding topography.

	Water Level	Flow	Flow	Water Level	Flow	Water level Increase
	100yr + 30%CC	100yr + 30%CC	1000yr	1000yr	1000yr vs 100 yr + 30% CC	1000yr vs 100 yr + 30% CC
1896	64.0575	103.9695	147.259	64.939	-43.2895	-0.8815
1726	62.802	152.2165	173.534	63.685	-21.3175	-0.883
1806	63.924	94.184	100.247	64.135	-6.063	-0.211
1606	61.7855	155.579	165.107	62.193	-9.528	-0.4075
1502	61.0975	162.3065	198.323	61.398	-36.0165	-0.3005
1406	60.613	160.842	202.596	61.039	-41.754	-0.426
Values taken from Environment Agency Model						

Extract 2 – Extract of Table 2, showing the calculated 100-year +30% CC vs the 1000-year Environment Agency modelled flood data

The nodes show a tangible arrangement between flow rate and predicted depth of water for the 100yr + 30% climate change event for example node 1806 has a 100yr + 30% climate change flow rate of 94.184, with the 1000 year being 100.247 with the predicted 100yr + 30% climate change given a reduced water depth of 0.211m over the 1000-year modelled result.

As such flood risk for the proposed development will consider the 100yr + 30% climate change event and the 1000yr event, to ensure the development is afforded protection.

Flood History

The fact flood defences have been formed along the boundary with the River Ehen suggests a historic flooding problem. It is understood the flood defences in their current form were constructed in 1978 by English Industrial Estates.

It is noted that the Copeland SFRA states there was some flooding from the River Ehen that caused damage to the factory in the autumn of 2000. A previously prepared FRA noted that the site warden had been interviewed and could not recall any flooding in his 15 years, this was in March 2010. As such if any flooding did occur or to what extent it is unknown. It was noted during our site walkover that outfalls to the River Ehen did not have tidal flaps/non-return valves installed and as such, it may have been possible for waters to back up the onsite drainage system causing localised flooding.

Having reviewed available data and previously prepared reports it is understood during the extensive flooding in Cumbria during 2008 & 2009 this site was not affected.

Critically, when reviewing the Environment Agency's historic flood maps there are no recorded events on the site.

Flood Defence Overtopping

Flood defences afford the site protection from the risk of flooding, as identified in Appendix D, with a condition survey undertaken by Rab Consultants in 2022. The hard flood defences are substantial and appear to be in an operational condition which is confirmed by the independent condition survey, with the hard defences being given a grade of 3 which is defined as being Fair. The soft defences and the riverbank have also been assessed as part of the condition survey, which are also given a grade of 3, confirming they are in Fair condition.

A condition survey undertaken by RAB Consultants, is included in Appendix D.

Based on the condition of the flood defences the overtopping scenario is considered within the River Ehen 2016 flood model with no flooding identifiable for the development site prior to the 0.1% AEP / 1000yr return period.

The RAB Consultants condition survey identifies various works which need undertaken immediately and within 1 year, it is recommended these works are carried out prior to works commencing, the total estimate value is £25,300 for the works as identified in the RAB report (RAB; 2869). It is then recommended that a condition survey be completed every 5 years as part of the management company's duties and the results are shared with the Environment Agency to ensure the flood defences are maintained and any further defects are rectified as part of the Environment Agencies' powers, should the Environment Agency deem that improvement/maintenance works necessary.

The original agreed scope with the Environment Agency did not require overtopping to be considered in relation to FD2320 and given the flood modelling which the Environment Agency have already produced.

Flood Defence Breaching

A detailed breach analysis has been prepared by Envireau Water, with the breach locations agreed in the meeting with the Environment Agency on the 20th June 2019, in their Penrith offices. The two agreed two locations were set as per the original locations agreed with Mott MacDonald who undertook the modelling in October 2013 for the previous application which was approved. In addition to the location, the required storm event was also agreed with the Environment Agency before progressing with the site-specific breach modelling, undertaken by Envireau Water. The purpose of the breach analysis was to determine flood extents, depths, velocities and hazard ratings for the site for the 1:100-year return period with climate change as required under NPPF Technical Guidance. Figure 4 below shows the two breach locations which have been utilised and previously agreed with the Environment Agency.

It is important to highlight the breach analysis has been prepared based on 100yr + 20% CC allowance, as agreed with the Environment Agency in 2019. During the planning process the national standards have been amended and the current standards require analysis on the 100yr + 30% CC allowance. The current breach analysis will be reviewed, and a margin of safety considered, which subject to planning will need a new breach analysis to current standards undertaken.

The flood defence breach modelling has been updated in June 2022, to include the latest topographical survey and ensure a realistic representation of flows in the event of flood defence failure.



A breach in the gabion baskets north of the site has been considered for the 1:100 year plus climate change return period. The approximate location of the breach event is indicated in Figure 4. It should be noted

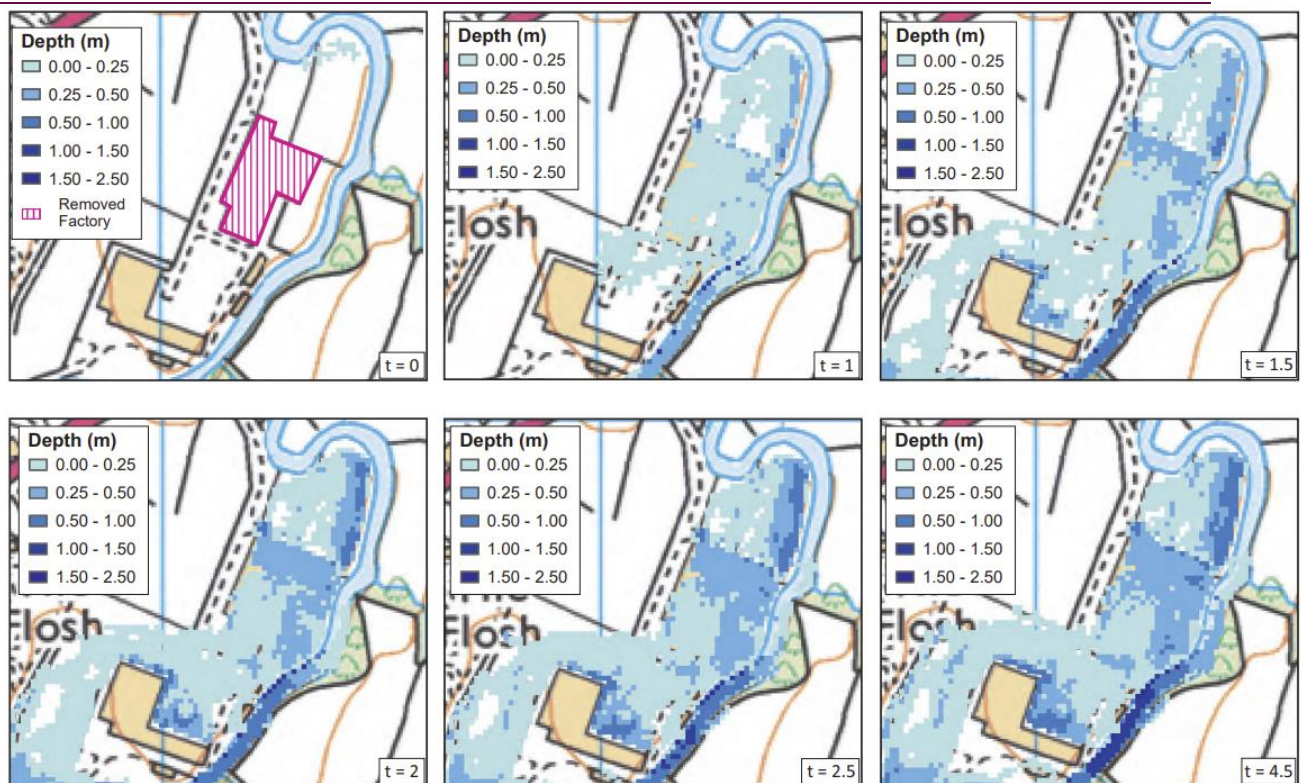


Figure 5 – Extract from Envireau Water of Breach 1

As this breach location does not impact the land within our clients ownerships a hazard rating has not been considered.

This analysis has been undertaken utilising the River Ehen model which was published in 2016 and is the current latest model for this location.

Breach 2

A breach in the earth embankment to the east of the site has been considered for the 1:100 year plus climate change return period. The approximate location of the breach event is indicated in Figure 4. During this breach event, the only building impacted upon is the Kangol Factory which does not form part of this application. As such the risk of the site flooding from a breach at this location is deemed low.

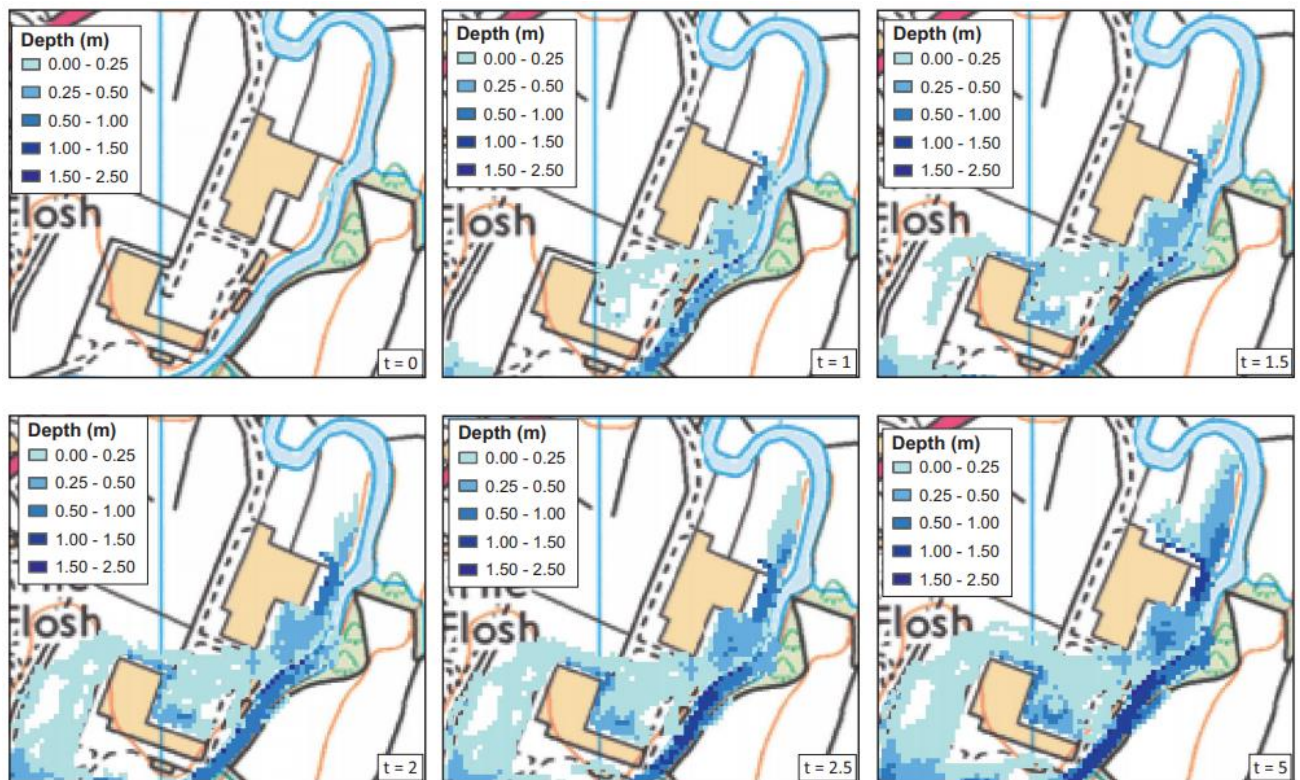


Figure 6 – Extract from Envireau Water of Breach 2

The Envireau Water report 'Updated Flood Risk Modelling – Cleator Mills Site' is included in Appendix F.

As this breach location does not impact the land within our clients ownerships a hazard rating has not been considered.

Unnamed Watercourse to Northeast

The watercourse to the North East of the development site has been modelled by Envireau Water with the results included in Appendix F, along with velocity maps. It should be noted that the velocities are low as would be anticipated given the low flow depths. The overland flow route from the unnamed watercourse does not vary in terms of depth for all events up to the 100-year return period, this includes the risk associated with 90% blockage of the culvert which would convey flows to the River Ehen. The depth of water across the site is between 0.01m and 0.1m, so a maximum of 100mm.

Once a developable area has been agreed the flood routing will need to be assessed with updated modelling. The development will aim to deliver an improvement over the current scenario and control overland flows to further reduce risk when they are within the site boundary.

Surface Water Flooding

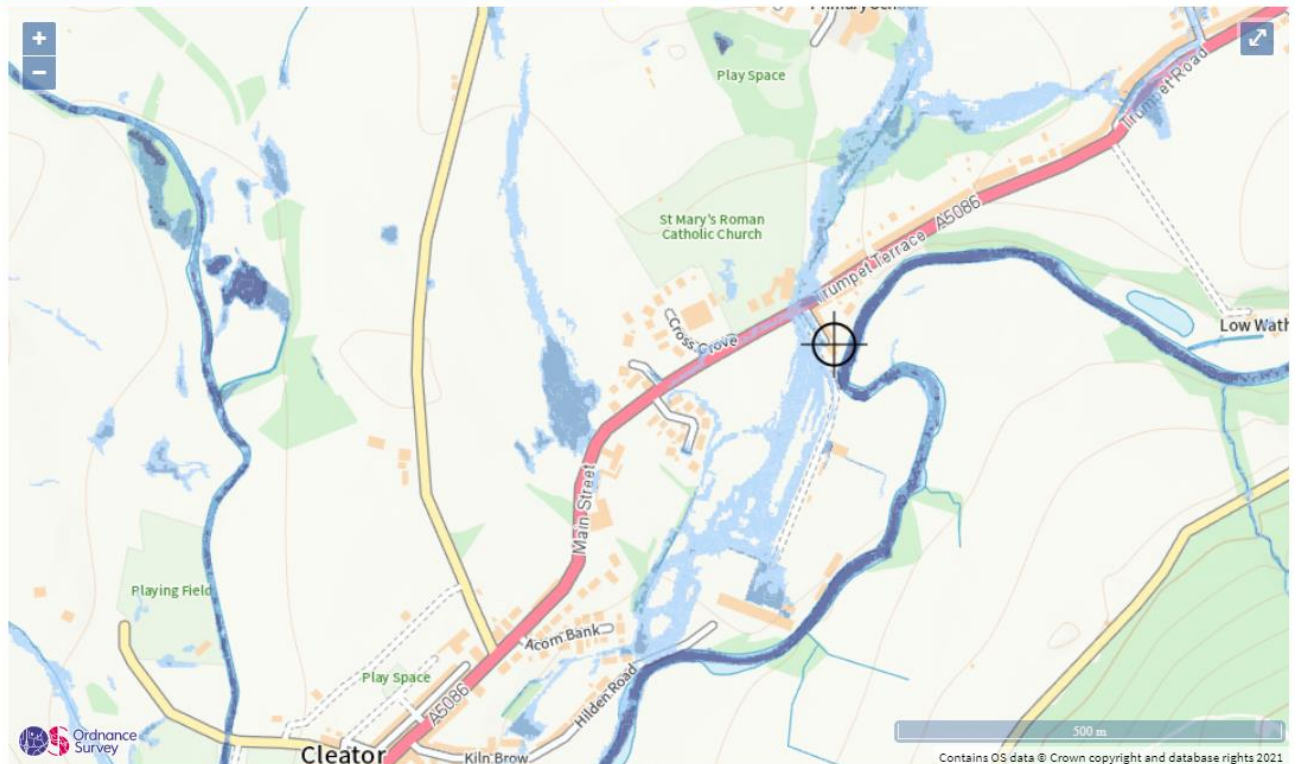
The surface water flood map available on the Environment Agency website (see Figure 7) indicated that part of the site is at risk of flooding due to surface water. The proposed residential development is at low risk of flows being conveyed across the site as identified by the Environment Agencies' own flood maps.

Flood risk

Low risk: depth

Location

Enter a place or postcode



Surface water flood risk: water depth in a low risk scenario

Flood depth (millimetres)

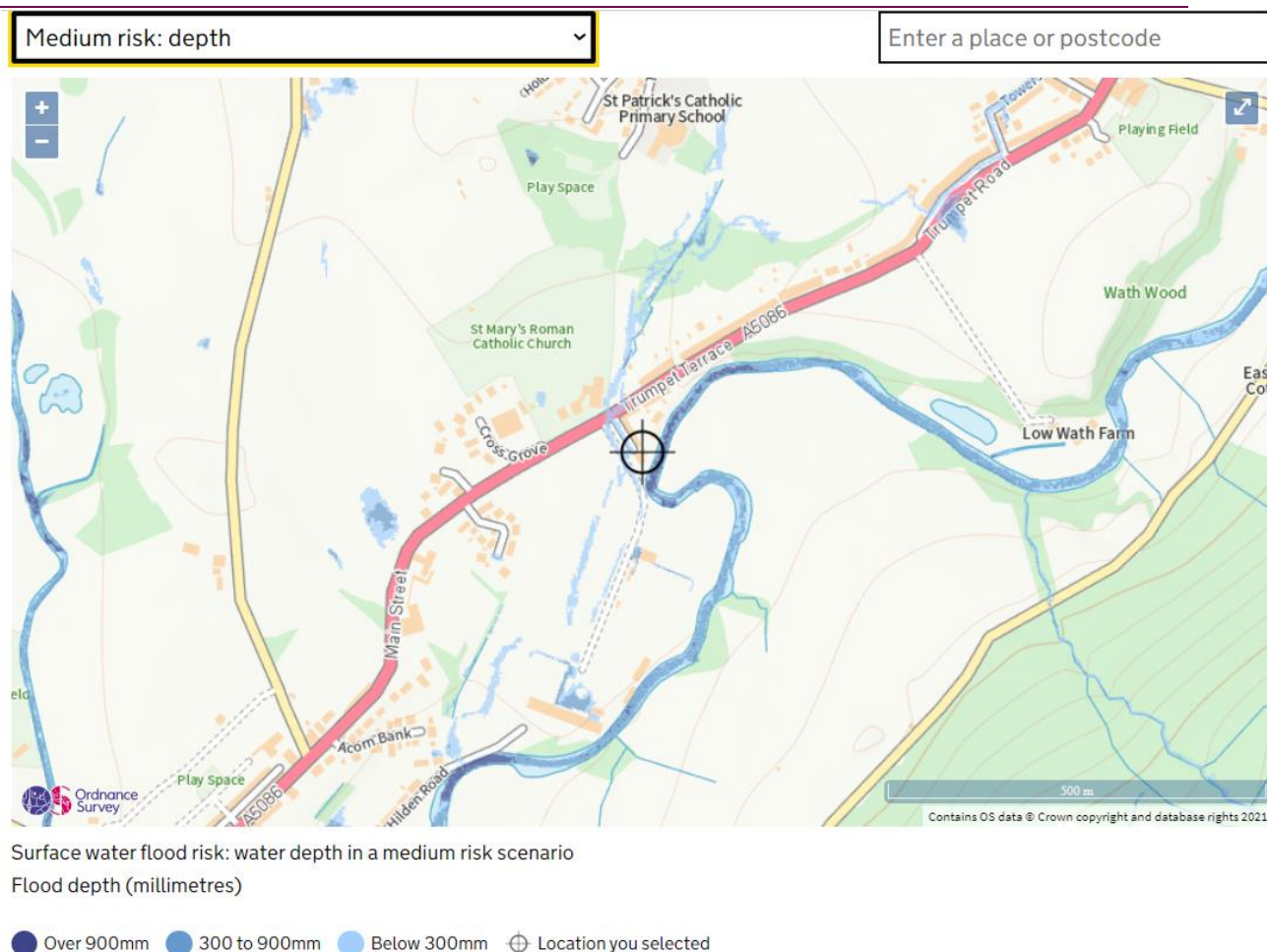
Over 900mm 300 to 900mm Below 300mm Location you selected

Extract 3 – Environment Agency Low-Risk Surface Water flood maps (17.07.2021)

The flow route itself is somewhat questionable given the topography given the kerb face along the road is circa 100mm and the route of flows appears to follow a raised mound as can be seen in picture 2 below;

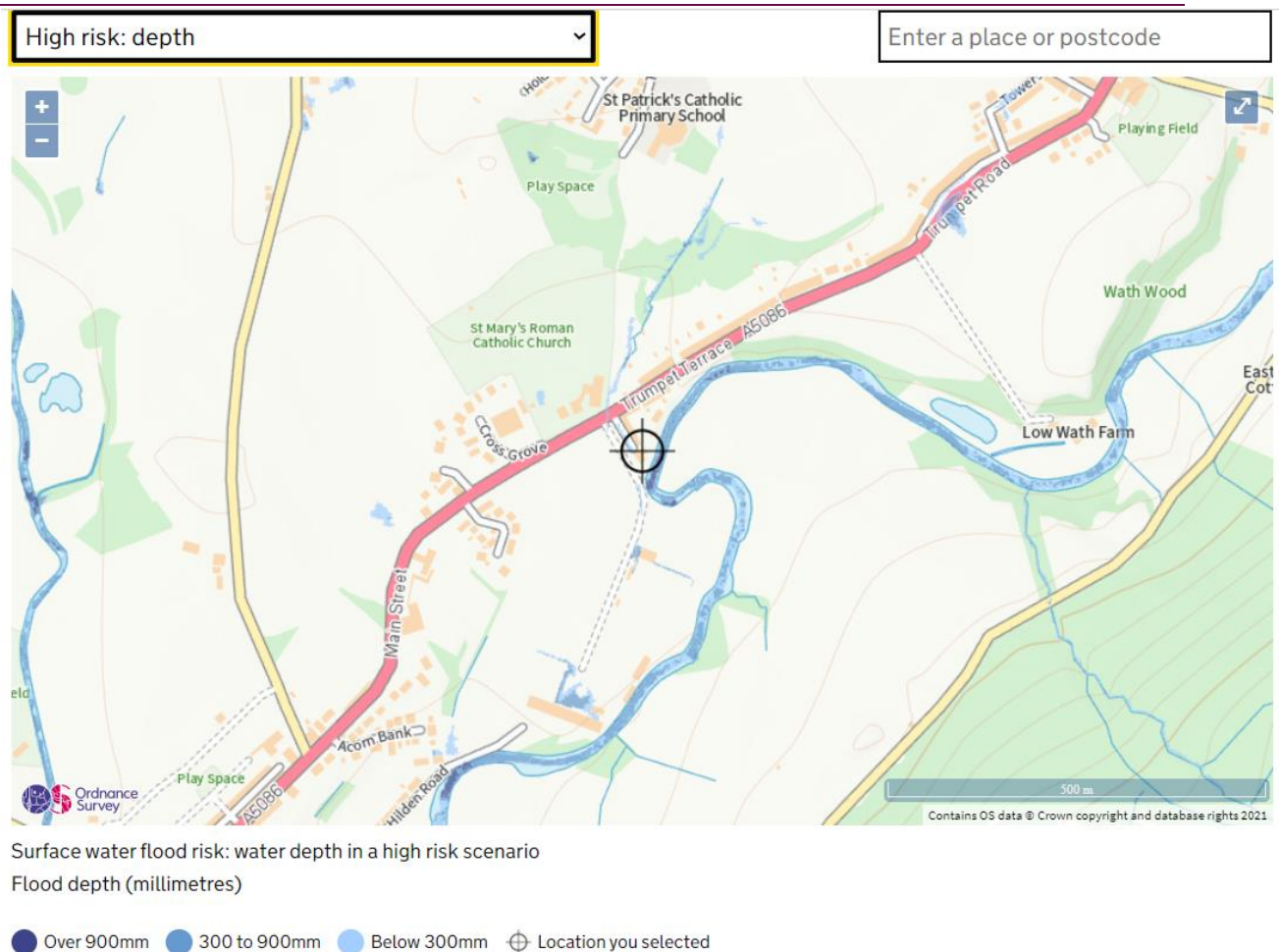


Photo 2 – Raised mound and kerbs along overland flood route



Extract 4 – Environment Agency Medium-Risk Surface Water flood maps (17.07.2021)

The Environment Agency medium flood risk maps demonstrate that no flows are being conveyed over the site and that water appears to be ponding in localised areas.



Extract 5 – Environment Agency High-Risk Surface Water flood maps (17.07.2021)

Extract 5 above highlights that the site is not at a high risk of surface water flooding.

Considering the risk of surface water flows and reviewing the local topography, a topographical survey is included in Appendix H, this demonstrates that flows would most likely follow the existing road rather than overtop the kerb and flow over the site. The data set utilised by the Environment Agency does not appear to take into account the kerbs. RWO has prepared a flow routing plan showing that the flows would follow the road wrapping around the site based on the existing levels and taking into account the kerbs, the drawing is included in Appendix I. As such the surface water flood route for overland, flows could be maintained, and the proposed dwellings afforded protection by raising FFLs over 300mm over the road levels and grading gardens from the higher FFLs to the lower road level. Raising the FFLs would ensure any overland flows which escaped the existing road would not flood properties and afford protection whilst maintaining flow routes.

Based on the Environment Agency surface water flood map surface water runoff enters the River Ehen to the South. South-East of the development site. Ground levels should be maintained to ensure this flood route can be utilised in the event of a surface water flooding incident.

6.0 RECOMMENDED DEVELOPMENT AREA

To afford the development of a level of protection against future flooding, it is recommended that dwellings be located only on the land outside of the 0.1% AEP for flooding from the River Ehen. In addition, dwellings should be located at or above existing ground levels to ensure the risk of flooding is not increased.

The proposed area of development has been reviewed for both defended and undefended scenarios, to ensure both are outside of the area at risk of flooding. Given the modelled scenarios identify an area of land outside of the risk of flooding of the 0.1% AEP / 1000yr return period this places a parcel of the land within flood zone 1.



Extract 6 – Environment Agency undefended 1000 year flood levels (area of development highlighted in Pink)

The overland flows will need to be re-assessed from the unnamed watercourse, subject to agreement in principle of the development area being acceptable, based on the risk of flooding from the River Ehen.

7.0 SAFE ACCESS AND EGRESS

As the proposed development site will be serviced by new access onto the A5086 located to the west of the development site, safe access and egress will always be achievable. In the event of a breach occurring in the northern flood defences, the extents of flooding do not impact upon the proposed access.

It is noted that the Environment Agency does not provide a Flood Warning service for the Cleator community. However, taking into consideration the access/egress location and the proposed FFL's, the risk of access/egress being unachievable is deemed low.

The surface water management plan associated with this development site has been considered utilising the following documentation;

- Building Regulations Part H,
- Sewers for Adoption,
- CIRIA C697

8.0 GROUND CONDITIONS

Elliot Environmental have undertaken the Site Investigation associated with the site with Geo-Environmental Engineering undertaking further soil infiltration tests following BRE365. Elliot Environmental reported ground conditions to have Sand and Gravel, which prompted the further investigation works undertaken by Geo Environment Engineering.

Geo-Environmental Engineering received instruction to undertake six soil infiltration tests across the site following BRE365. Figure 2 below shows the locations of the soil infiltration test results.



Figure 2 – Soil Infiltration Test Locations

SA01 recorded Topsoil from 0.00 – 0.40m with Sand & Gravel recorded from 0.40 – 2.00m, soil infiltration test results for this location have been calculated as $6.04665^{\text{m/s}}$.

SA02 recorded Topsoil from 0.00 – 0.30m, Sand from 0.30 – 0.70m and 0.70 – 2.00m Sand & Gravel, soil infiltration test results for this location have been calculated as $4.97347^{\text{m/s}}$.

SA03 recorded Topsoil from 0.00 – 0.20m with Sand recorded from 0.20 – 0.80m and Sand & Gravel from 0.80 – 2.00m, soil infiltration test results for this location have been calculated as $2.39464^{\text{m/s}}$.

SA04 recorded Topsoil from 0.00 – 0.30m with Sand & Gravel recorded from 0.30 – 1.50m, soil infiltration test results for this location have been calculated as $2.27591^{\text{m/s}}$.

SA05 recorded Topsoil from 0.00 – 0.35m with Sand recorded from 0.35 – 0.60m and Sand & Gravel from 0.60 – 2.00m, soil infiltration test results for this location have been calculated as 2.24551⁻⁵ m/s.

SA06 recorded Topsoil from 0.00 – 0.50m with Sand & Gravel recorded from 0.50 – 0.90m and Sand & Gravel from 0.90 – 1.50m, soil infiltration test results for this location have been calculated as 4.22297⁻⁵ m/s.

All of the recorded soil infiltration rates are well within the acceptable rates and as such the site will be suitable to utilise infiltration. Based upon this in accordance with Building Regulations and the CIRIA SuDS train, surface water should discharge into suitably designed soil infiltration drainage systems.

Geo-Environmental Engineering report is included in Appendix J.

9.0 RECEIVING WATERS

The nearest watercourse is the River Ehen, which generally flows in a south-westerly direction. The Ehen is located on the immediate eastern and southern boundaries of the proposed development site. It has been reported that the water quality within the River Ehen is Quality A in the past.

There is also a small issue located in the western boundary, which discharges into the River Ehen. A further small watercourse is shown flowing southwest before sinking or being culverted approximately 75m from the northern end of the site.

The critical issue relating to the surface water run-off from the proposed development site relates to the River Ehen which is classified as a Site of Special Scientific Interest (SSSI) and a Special Area of Conservation (SAC). It is understood that a direct discharge to the River Ehen has been deemed as unacceptable, based upon this it is proposed to utilise infiltration to dispose of surface water as stated in section 8.0 of this report.

10.0 SURFACE WATER MANAGEMENT PLAN

The surface water management plan associated with this development site has been considered utilising the following documentation;

- Building Regulations Part H,
- Sewers for Adoption,
- CIRIA C697

Soil Infiltration

Section 4.0 Ground Conditions, includes a summary of the soil infiltration test results which have been undertaken by Geo-Environmental Engineering in accordance with BRE 365. A total of six tests have been undertaken, a summary of the results is below in table 1.

Soil Infiltration Test	Results
SA01	6.04665 ⁻⁵ m/s
SA02	4.97347 ⁻⁵ m/s
SA03	2.39464 ⁻⁵ m/s
SA04	2.27591 ⁻⁵ m/s
SA05	2.24551 ⁻⁵ m/s
SA06	4.22297 ⁻⁵ m/s

Table 1 – Soil Infiltration Test Results

The above summary of soil infiltration test results demonstrates that soil infiltration can be utilised across the proposed development site.

Based upon the soil infiltration test results the use of soakaways to accommodate the surface water runoff is deemed as viable. It is recommended that further water monitoring be undertaken to ascertain the water level across the proposed development.

11.0 CONCLUSIONS

This assessment has looked at the implications of the proposed Residential developments in relation to flood risk, including breach analysis as agreed with the Environment Agency during meetings in June 2019.

The proposed development site is shown as being in Flood Zone 1.2 & 3a on the Environment Agency flood maps. When reviewing the defended flood modelling undertaken by the Environment Agency the site is afforded protection for all events up to and including the 1:200 year return period.

The flow rates and water levels for varying events have been considered including the upper central and higher and flow rates are comparable to the 1:1000 year return period, giving a clear indication of potential water levels on the site when looking at the modelled results.

It is proposed to only develop the site outside of the 1:1000yr modelled flood level. This will be subject to further overland flood modelling from the unnamed watercourse to the north east, once agreement on the developable area has been reached.

The Environment Agency surface water flood maps have been reviewed against the topography with flows shown coming over the site in a low-risk event. When reviewing the contours and local topography we believe that surface water flows would follow the road, given the kerb phase and raised levels to the site on the boundary as opposed to run straight across the site. As such surface water overland flow can be managed with the route maintained around the perimeter of the development site.

Safe access and egress have been established via the new proposed access road onto the A5086. The overland flood flow routes do not impede the proposed access/egress for the development's new entrance.

The Environment Agency does not provide a Flood Warning Service for Cleator. It is noted that the site is covered by the River Ehen, Calder, Irt and Esk Flood Alert areas, it would therefore be recommended this be included within the homeowner's packs.

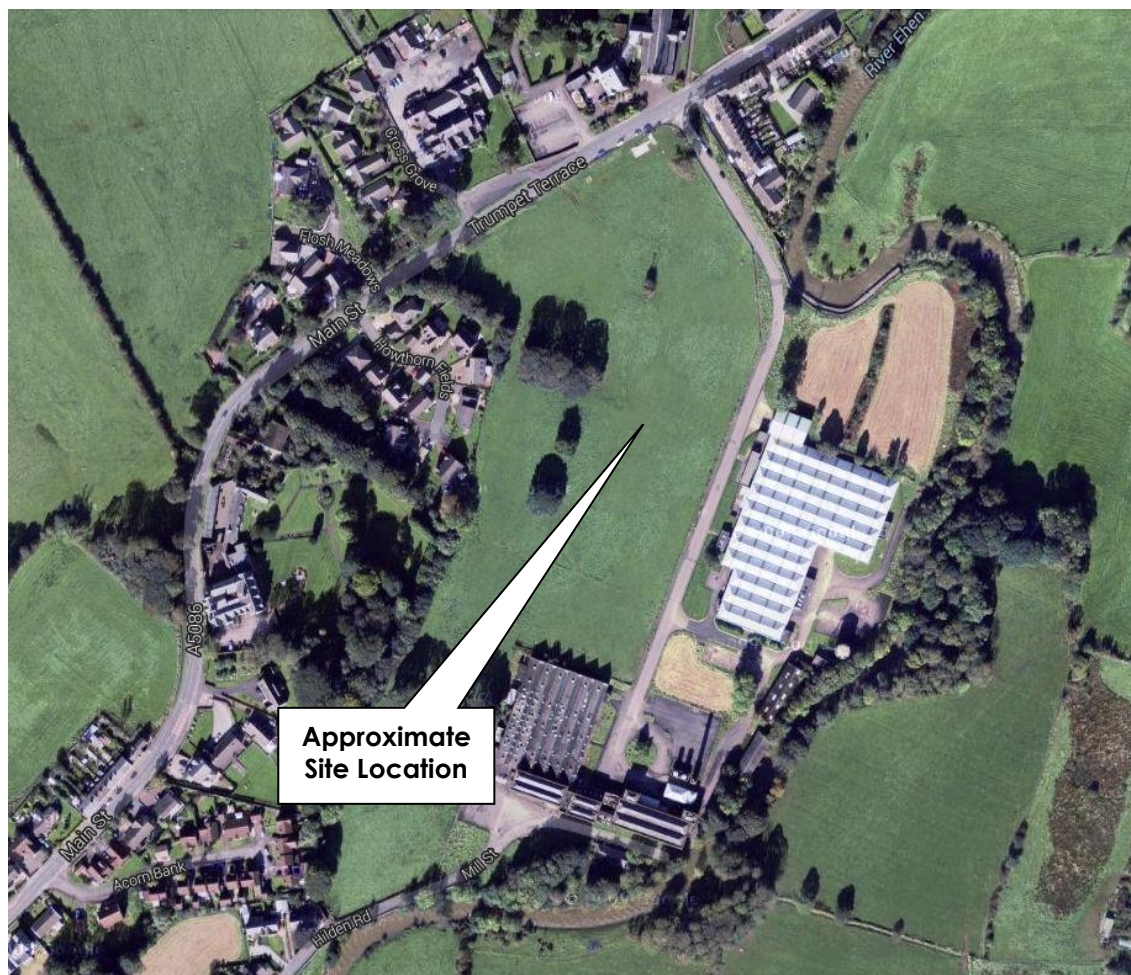
A Surface Water Management Plan (SWMP) has been identified including the levels of treatment required to ensure the River Ehen water quality remains protected.

Any potential impact of the development can be adequately addressed by good drainage design.



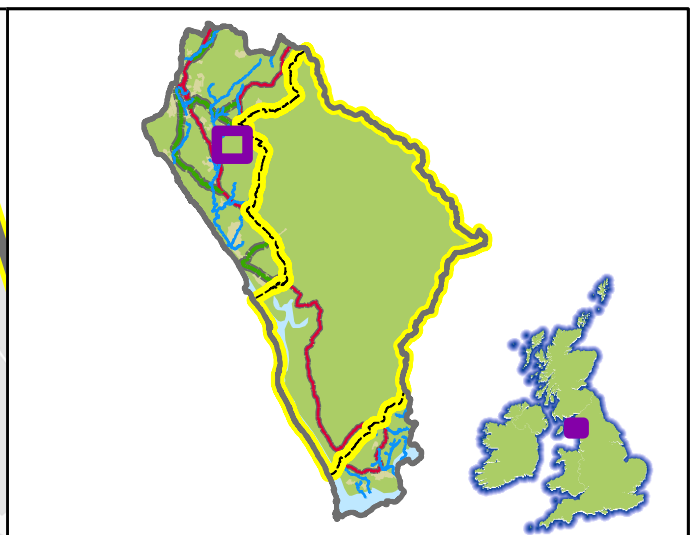
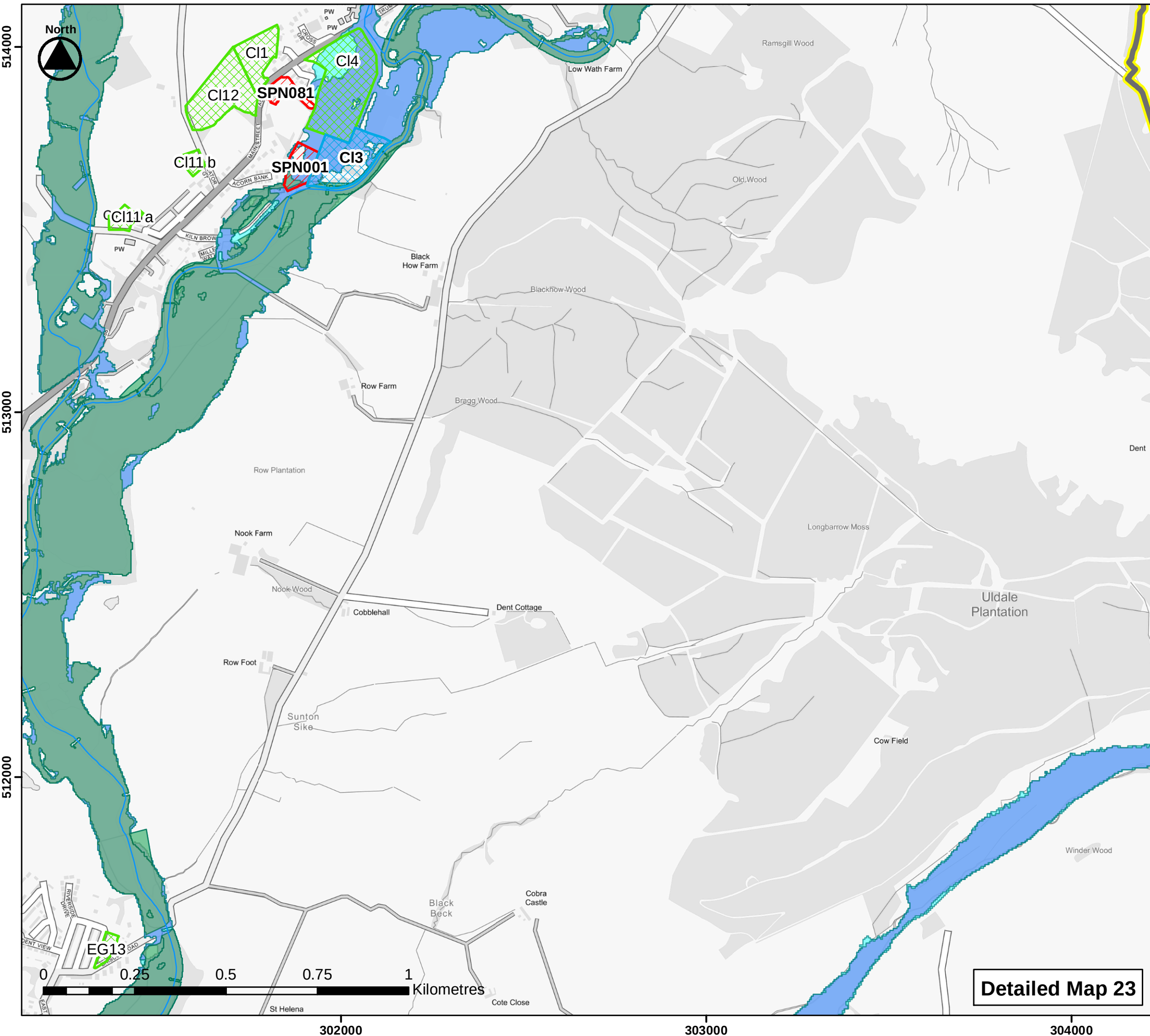
Ross Oakley
For and behalf of RWO Associates Limited
November 2020

Appendix A Site Location Plan



Location Map	
Site	Cleator Mill - Residential
Client	Gleeson Regeneration
Job Number	19002
Scale	NTS

Appendix B Strategic Flood Map



LEVEL 1 STRATEGIC FLOOD RISK ASSESSMENT

For
COPELAND BOROUGH COUNCIL

Please select a data type from the dropdown menu below that you wish to view:

CBC boundary

Detailed River Network

LDNP boundary

Other LPA boundary

Potential Development Sites

Employment Allocations

Employment Opportunity

Possible Housing Allocations

Possible Opportunity Sites

New Sites Submitted 2

Residential

Employment

Mixed Use

Community Garden

Flood Zone 3b

Flood Zone 3a

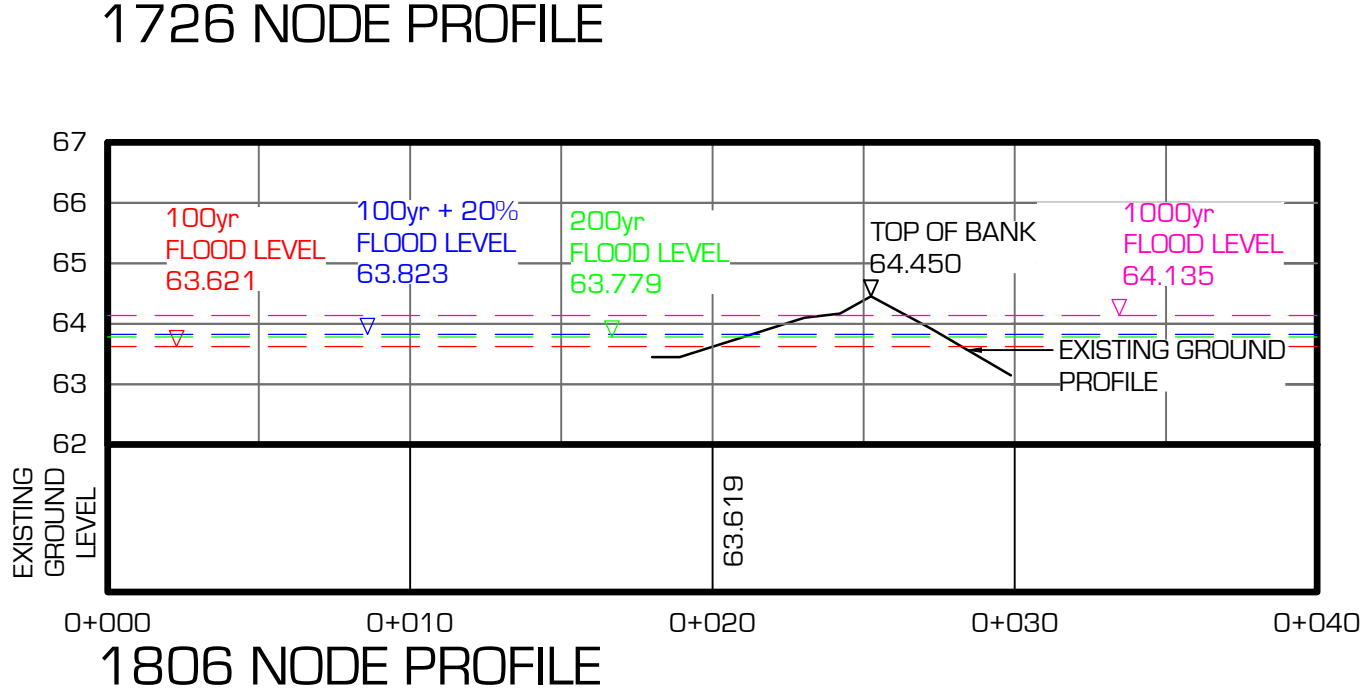
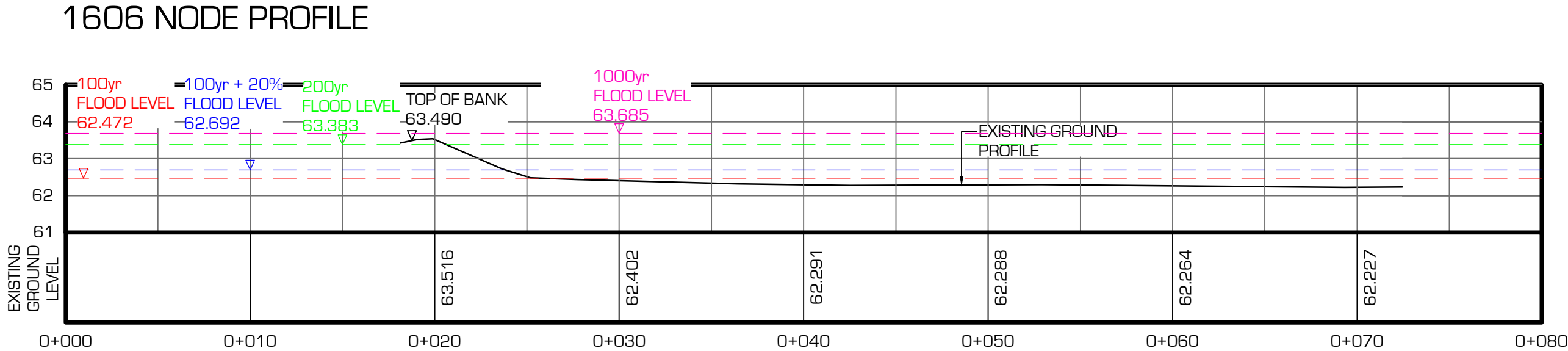
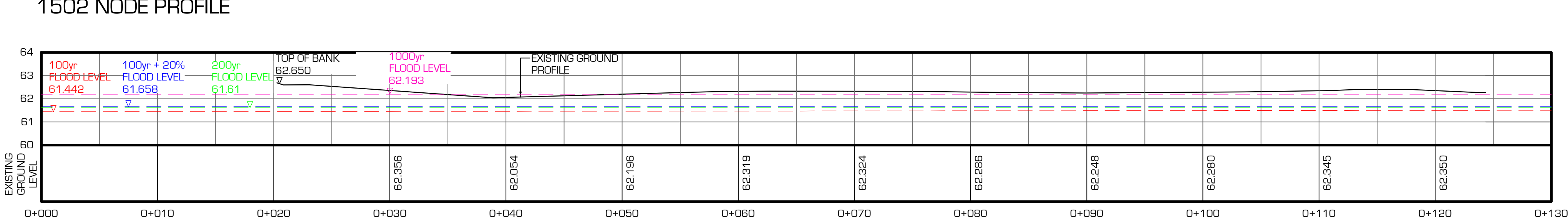
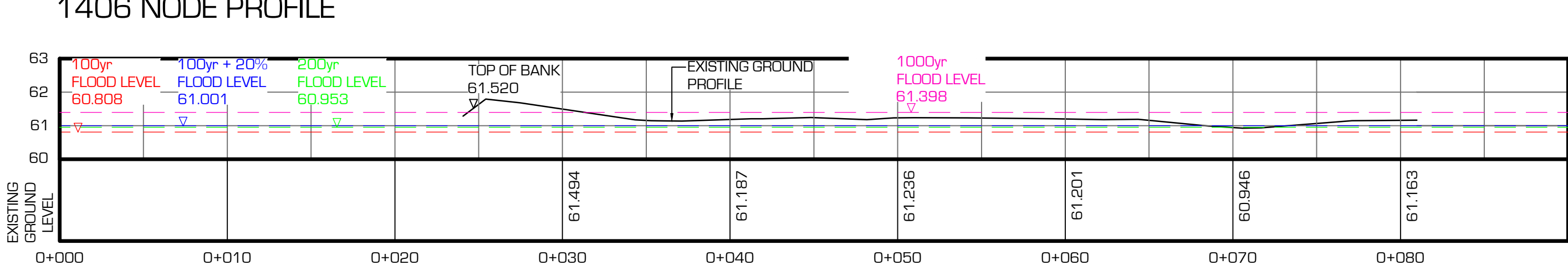
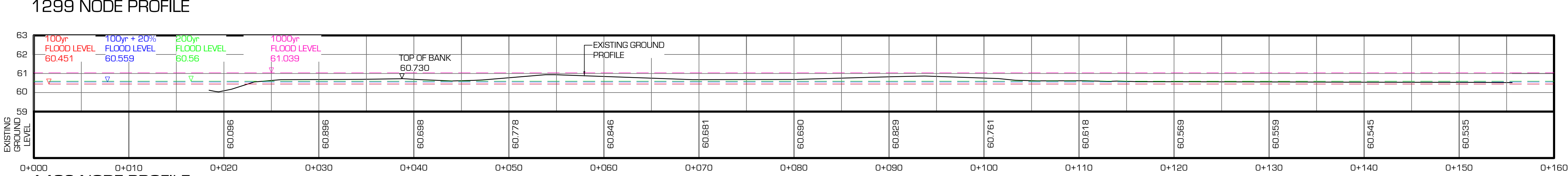
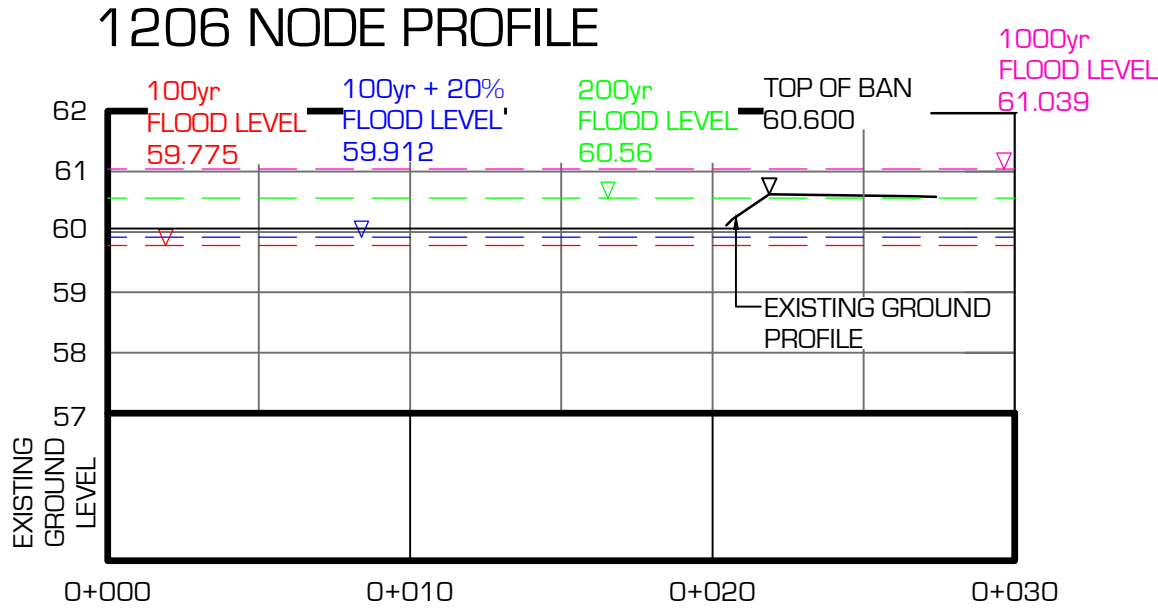
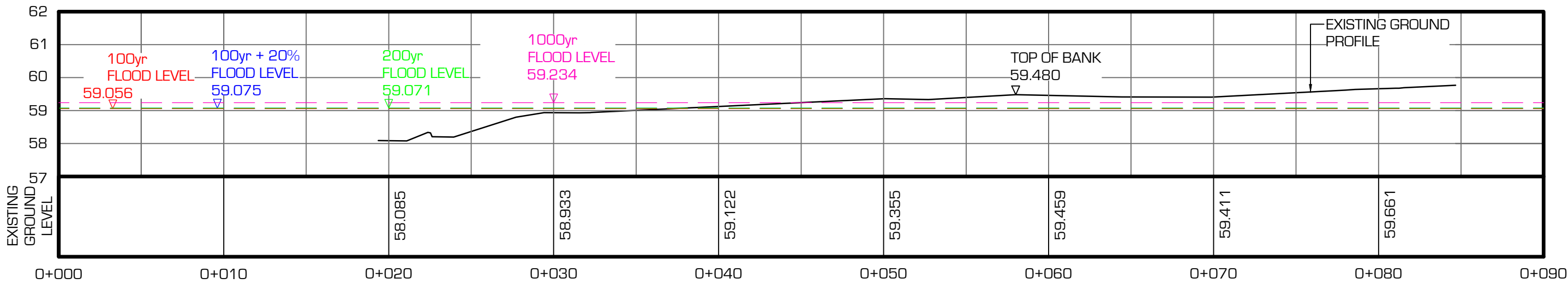
Flood Zone 2

Show Site Reference Labels

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Appendix C Topographical Survey and Site Sections





06.05.2021	AMENDED TO SUIT COMMENTS	NN	2
06.05.2021	AMENDED TO SUIT COMMENTS	NN	1
Date	Revisions	Drawn	Rev.

Dwg Status: PRELIMINARY

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Client: GLEESON HOMES

Project: CLEATOR MILL CUMBRIA

Title: SECTIONS THROUGH NODES

Scale: 250H 500V	Drawn: NN	Checked: RWO	Date: 05.11.20
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Job No. 19002	Drawing No. 951	Revision 2
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Appendix D Flood Defence Survey



Cleator Flood Asset Condition Assessment

23 MAR 2022
Version 1.0
RAB: 2869



Disclaimer

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Quality Control

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Checked	Josh Spittle BSc (Hons) MSc
Approved	Peter Batty BEng (Hons) MSc GMICE

Revision History

Version	Date	Amendments	Issued to
1.0	23/03/2022		Ross Oakley



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Contents

1.0	INTRODUCTION	2
2.0	METHOD	2
3.0	FLOOD ASSETS AND CONDITION ASSESSMENT	3
4.0	FINDINGS AND RECOMMENDATIONS.....	6
	CL1 – Embankment	6
	CL2 – Natural High Ground.....	8
	CL3 – Wall	9
	CL4 – Outfall.....	10
	CL5 – Outfall.....	11
	CL6 – Wall	12
	CL7 – Outfall.....	13
	CL8 – Outfall.....	14
	CL9 – Outfall.....	15
	CL10 – Outfall.....	16
	CL11 – Outfall.....	17
	CL12 – Outfall.....	18
	CL13 – Natural High Ground.....	19
	CL14 – Engineered High Ground	20
	CL15 – Wall	21
	CL16 – Wall	22
	CL17 – Natural High Ground.....	23
	CL18 – Embankment	24
	CL19 – Outfall.....	26
	CL20 – Outfall.....	27
	CL21 – Embankment	28
	CL22 – Embankment	30
	CL23 – Outfall.....	32
	CL24 – Wall	33
5.0	SUMMARY COSTS OF REPAIR AND MAINTENANCE	34
6.0	SUMMARY	35
	APPENDIX A: ASSET INSPECTION LOGS.....	36



**RESILIENCE
& FLOOD RISK**

Cleator Flood Asset Condition Assessment Report

23 MAR 2022

Version 1.0

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1.0 Introduction

Cleator, Cumbria is in the Borough of Copeland in the Northwest of England. The River Ehen is within the catchment of Copeland's Wild Rivers and runs from Ennerdale Water to Sellafield where it enters the Irish Sea. The watercourse passes through Cleator, where there are numerous flood defences and structures around the watercourse including embankments, outfalls, walls, natural high ground and engineered high ground.

Approximately 1km of the River Ehen flood assets were inspected to assess their condition, defects and required maintenance. This report contains details of the findings of these inspections including estimated costs for the preservation of the assets.

2.0 Method

The condition grading and descriptions given below are the standards adopted by the Environment Agency. The five condition grades range from 'very good' to 'very poor', and the descriptions reflect condition according to flood defence performance.

Grade	Rating	Description
1	Very Good	Cosmetic defects that will have no effect on performance
2	Good	Minor defects that will not reduce the overall performance of the asset
3	Fair	Defects that could reduce performance of the asset
4	Poor	Defects that would significantly reduce the performance of the asset. Further investigation needed
5	Very Poor	Severe defects resulting in complete performance failure

The inspection was carried out and recorded in accordance with the Condition Assessment Manual (March 2012) and Version 4 of the Asset Template and Weighting Guidance on 28 January 2022 by Environment Agency accredited Flood Asset Inspectors.

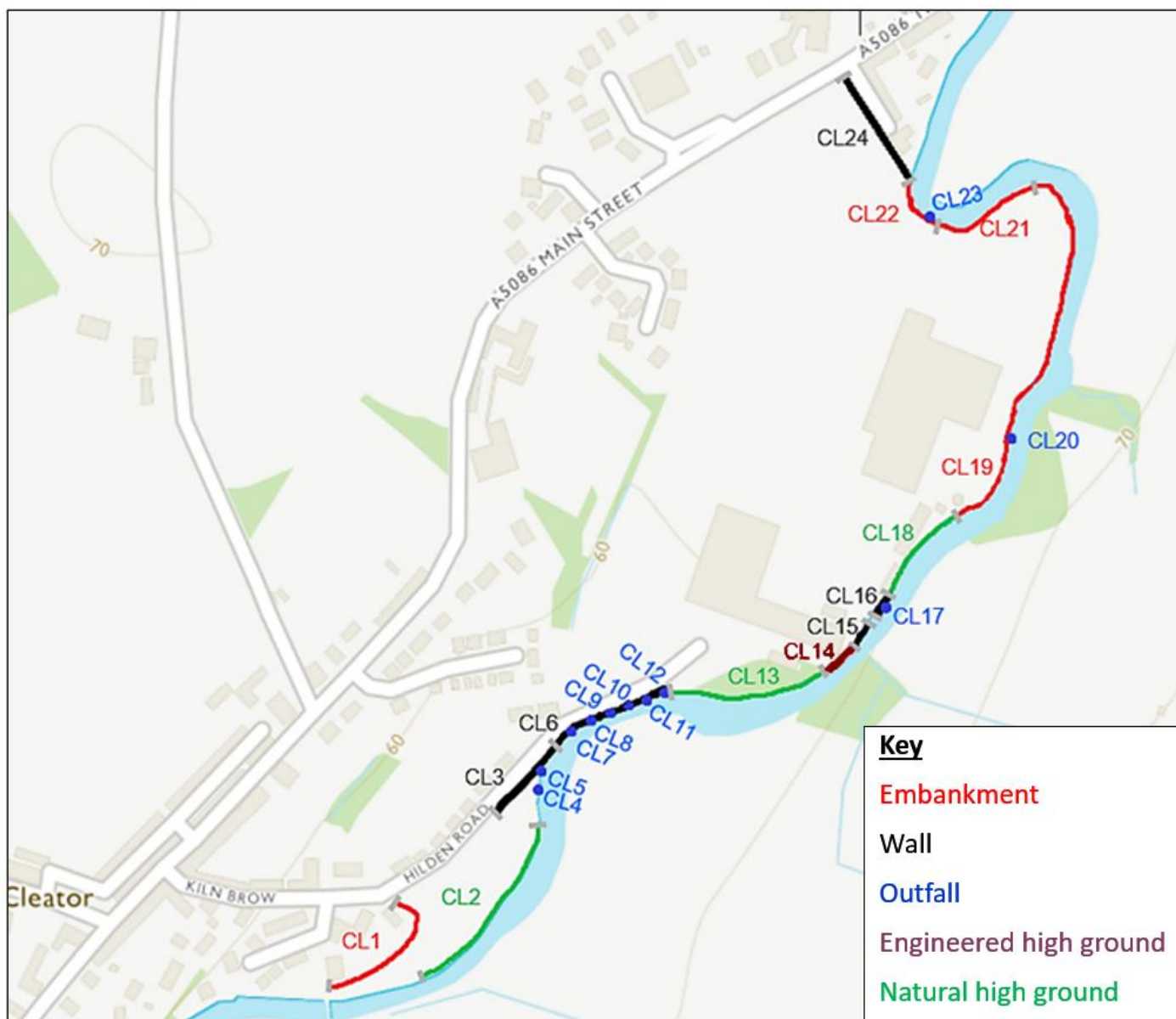
Visual inspection is the simplest form of non-destructive testing, as it does not require any specialist equipment. It is a widely used technique for monitoring assets and their surroundings. However, as only the surface of a structure is visible, this method can only assess the surface details and condition of an asset; changes to interior structure and condition are not easily identifiable until they lead to changes to the surface of the asset. Assessment of an asset's surroundings remains a key indicator to the asset's performance and integrity.

The recommendations arising from the visual inspection include remedial works to address visible defects and bring each element of the asset back to at least "fair" condition, but also actions to overcome access constraints and/or the need for other tests or investigations to assess an assets performance and integrity.



3.0 Flood Assets and Condition Assessment

Figure 1 and Table 1 provide a summary of the location, type and condition grade of flood assets identified and inspected on 28 January 2022.



**TABLE 1: FLOOD ASSET CONDITION SUMMARY.**

Asset ID	Asset type/sub-type	Description	Grade
CL1	Defence - Embankment	Embankment running in front of houses below Hilden Road and Kiln Brow	4
CL2	Defence – Natural High Ground	Natural high ground located below Hilden Road before wall	3
CL3	Defence – Wall	Stone wall on Hilden Road with berm	4
CL4	Structure – Outfall	Outfall located on River Ehen	3
CL5	Structure – Outfall	Outfall located on River Ehen	3
CL6	Defence – Wall	Stone wall on Hilden Road	4
CL7	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
C8	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
CL9	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
CL10	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
CL11	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
CL12	Structure – Outfall	One of six identical outfalls located within wall on Hilden Road	2
CL13	Defence – Natural High Ground	Natural high ground located below Mill Street	3
CL14	Defence – Engineered High Ground	Engineered high ground in front of old mill	3
CL15	Defence – Wall	Stone wall in front of old mill	3
CL16	Defence – Wall	Brick wall with brick channel side located on River Ehen	3
CL17	Defence – Natural High Ground	Natural high ground located on River Ehen	3
CL18	Defence – Embankment	Earth embankment located on River Ehen	3
CL19	Structure – Outfall	Drainage pipe located on River Ehen	3
CL20	Structure – Outfall	Outfall located on River Ehen	3
CL21	Defence - Embankment	Earth embankment with gabions and sheet piling on River Ehen	3



Asset ID	Asset type/sub-type	Description	Grade
CL22	Defence - Embankment	Earth embankment with stone and sheet piling on River Ehen	3
CL23	Structure – Outfall	Outfall located on River Ehen	3
CL24	Defence - Wall	Wall located off Main Street	3

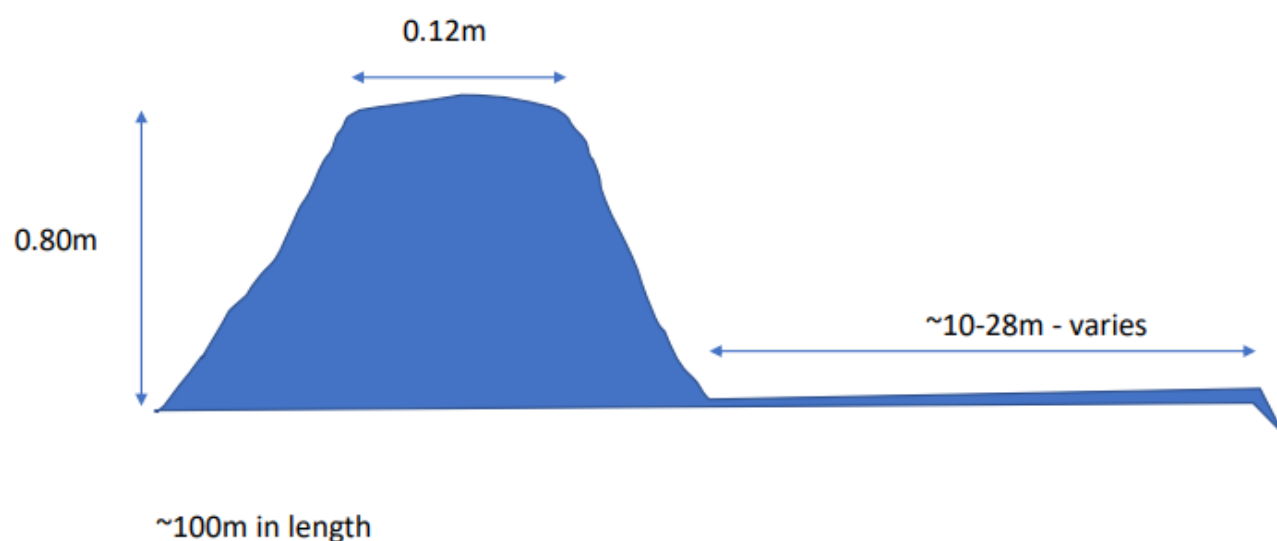


4.0 Findings and Recommendations

The following is a summary of the findings and recommendations to bring all asset elements to at least “fair” condition, grade 3.

CL1 – Embankment

Small earth embankment protecting residential properties behind.



Comments

Variant weighting used for crest as <4m wide. Drainage pipe running through entire width of embankment, low spots, some animal holes and rutting on crest, landward face and exposed face have some holes and uneven slopes but are well vegetated. Undermining, minor erosion and light foreign objects present on channel side but currently stable.

Grade = 4, Poor

Years	Recommendations	Cumulative Cost (£)
Immediate	Install none return valve to drainage pipe	£400.00
1	- Inspect embankment annually and infill any identified low spots on crest with topsoil and lay down grass seed - Manage vegetation to avoid undesirable vegetation growth and maintain grass growth - Consider pest control	£600.00
5	- Continue to inspect the embankment yearly to keep track of and identify potential issues - Continue vegetation management to prevent the growth of undesirable vegetation on embankment	£3,500.00

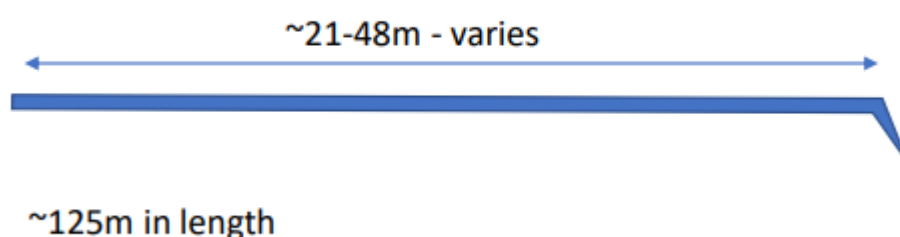


	• Infill identified low spots on crest with topsoil and lay down grass seed • Monitor condition of landward toe to ensure vehicle use does not damage asset – infill low spots and lay down grass seed in areas of vegetation loss	
10	• Continue yearly inspections and vegetation management • If extensive damage has been incurred to the embankment, reprofile the bank and lay down grass seed	£12,500.00
15	• Continue yearly inspections and vegetation management • If extensive damage has been incurred to the embankment, reprofile the bank and lay down grass seed	£16,600.00



CL2 – Natural High Ground

Natural high ground located in a grass field in front of residential properties with a width of 21-48m between the channel side and road.



4.1.1 Comments

Significant undermining, erosion and presence of light foreign objects on channel side. High ground in good condition.

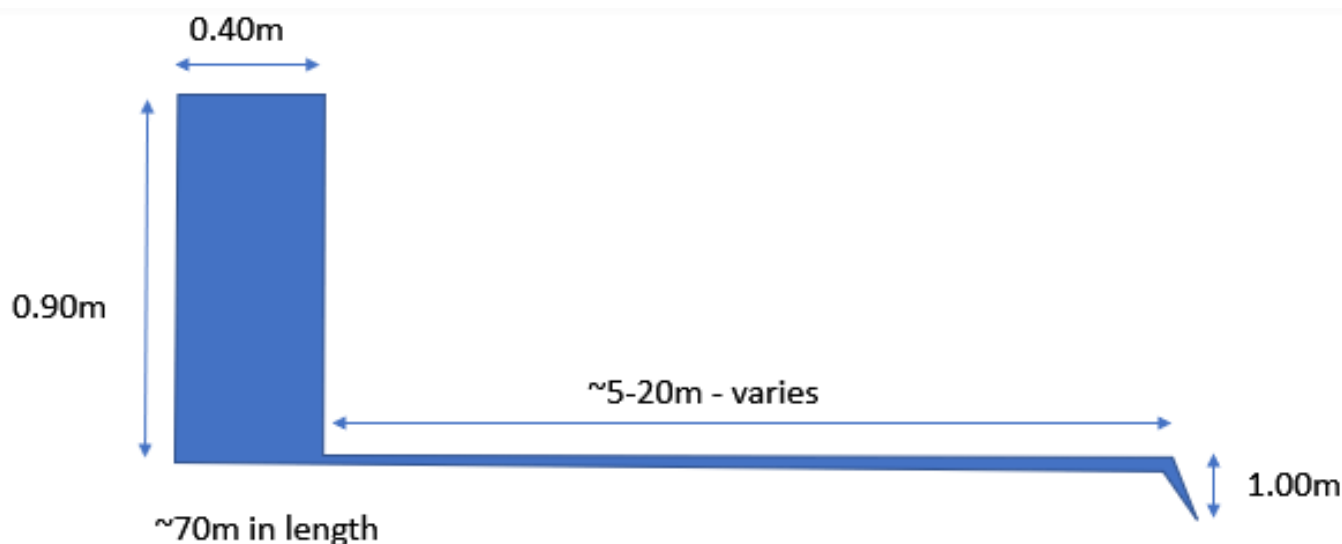
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct visual asset inspections annually, monitor erosion, maintain grass on high ground and ensure vegetation is kept stable and not blocking channel	£600.00
5	- Continue to inspect the high ground yearly to keep track of and identify potential issues - Continue with vegetation management and remove unstable trees	£3,100.00
10	- Continue yearly inspections and vegetation management - If considerable amounts of erosion are being incurred to the channel side, install coir erosion protection matting	£13,200.00
15	- Continue yearly inspections and vegetation management - If extensive erosion has been incurred to the channel side, consider reprofiling bank and installing rock armour	£21,500.00



CL3 – Wall

Stone wall next to road protecting residential properties but not designed as a flood wall.



4.1.2 Comments

Variant weightings used for both faces as no revetments. Significant mortar loss to crest, holes through wall, bulging of wall where light foreign objects are growing in front on wall, distorting its shape and some erosion to channel side.

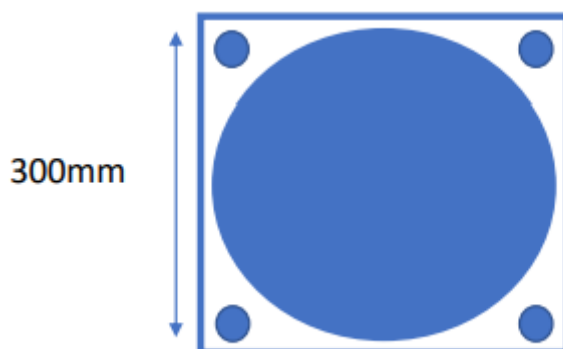
Grade = 4, Poor

Years	Recommendations	Cumulative Cost (£)
Immediate	Rebuild wall and remove trees in front of wall	£1,900.00
1	- Conduct visual asset inspections annually - Carry out minor repairs to bricks and mortar and maintain grass on berm	£200.00
5	- Continue to inspect the wall yearly to keep track of and identify potential issues - Carry out small repairs to brickwork and management of surrounding vegetation	£1,000.00
10	- Carry out repointing of wall - Continue with annual visual asset inspections and management of surrounding vegetation	£2,100.00
15	- If there has been any serious structural damage to the wall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage - If extensive erosion has been incurred to the channel side, consider reprofiling bank and installing rock armour	£10,100.00



CL4 – Outfall

300mm diameter flapped outfall with concrete apron located on channel side in front of wall. Owner and operator unknown.



4.1.3 Comments

Vegetation around headwall. Unable to see through pipe and no CCTV footage available.

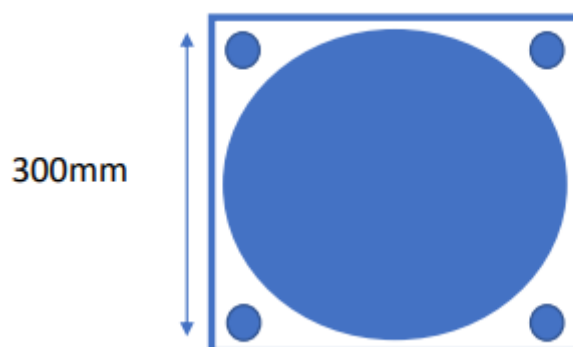
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue to inspect the outfall yearly, including CCTV inspections of the pipe every 5 years - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue yearly inspections of outfall including CCTV inspections of pipe every 5 years - Continue with vegetation management - Carry out small repairs to brick and mortar loss	£6,900.00
15	- Continue yearly inspections of outfall and manage vegetation growth - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ relevant operative to repair damage	£17,400.00



CL5 – Outfall

300mm diameter flapped outfall with no apron located on channel side in front of wall. Owner and operator unknown.



4.1.4 Comments

Outfall in good condition, very minor corrosion present on frame and flap valve. Unable to see through pipe and no CCTV footage available.

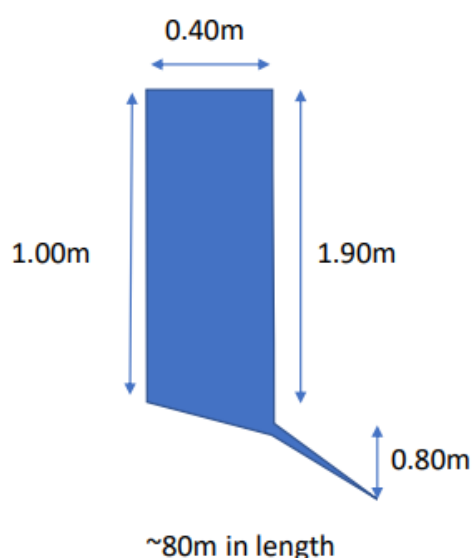
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue to inspect the outfall yearly, including CCTV inspections of the pipe every 5 years - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue yearly inspections of the outfall including CCTV inspections of the pipe every 5 years - Continue with vegetation management	£6,900.00
15	- Continue yearly inspections of the outfall and manage vegetation growth - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£17,400.00



CL6 – Wall

Stone wall with 6 highway outfalls in wall connecting to previous wall, also not a flood wall.



4.1.5 Comments

Heavy foreign objects growing towards channel on berm and channel side and undermining on channel side causing channel side to be unstable. Ivy growth on wall, heavy foreign objects growing close to wall causing bulging to wall and capping stones lost from crest halfway across wall.

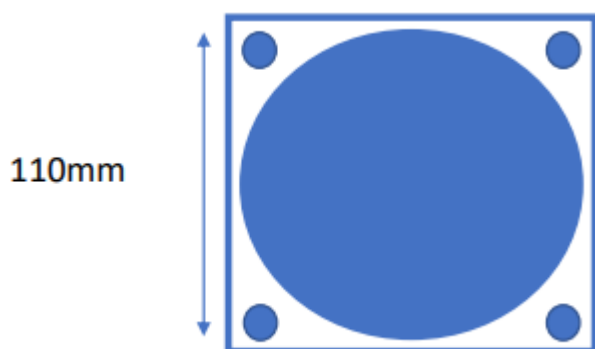
Grade = 4, Poor

Years	Recommendations	Cumulative Cost (£)
Immediate	Rebuild wall, remove unstable trees, and remove trees next to wall	£5,000.00
1	- Conduct visual asset inspections annually - Maintain surrounding vegetation to avoid wall incurring structural damage	£200.00
5	- Continue to inspect the wall yearly to keep track of and identify potential issues - Small repairs to brickwork and management of surrounding vegetation	£1,000.00
10	Carry out repointing of wall and continue with small repairs to brickwork and management of surrounding vegetation	£2,100.00
15	- If there has been any serious structural damage to the wall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage - If extensive erosion has been incurred to the channel side, consider reprofiling bank and installing rock armour	£11,000



CL7 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.6 Comments

No signs of corrosion to flap valve or frame, pipe has minor leaf debris but no blockages or damage. Downstream headwall has some cracks, vegetation growth and mortar loss.

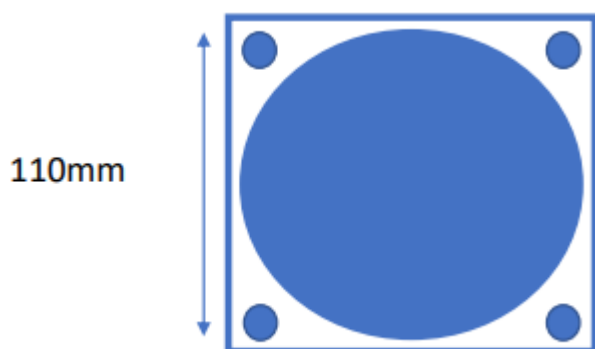
Grade = 2, Good

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL8 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.7 Comments

No signs of corrosion to flap valve or frame, pipe has minor leaf debris but no blockages or damage. Minor crack to downstream headwall, vegetation growth and mortar loss.

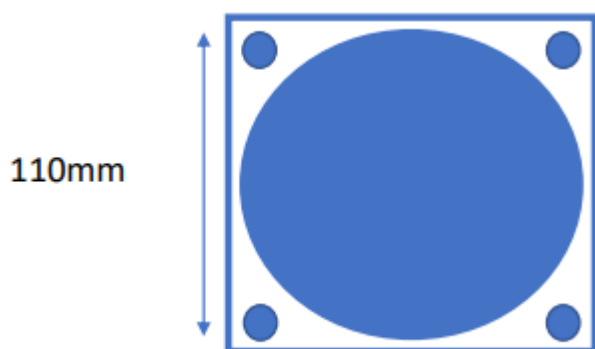
Grade = 2, Good

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL9 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.8 Comments

No corrosion to flap valve or frame. Cracks and mortar loss on headwall. Pipe has minor leaf debris but no blockages or damage.

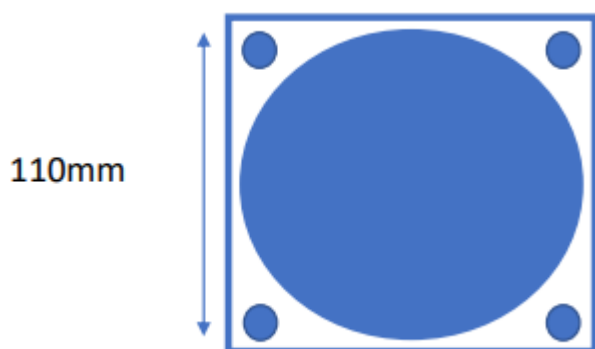
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL10 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.9 Comments

Ivy growth around frame and headwall. No corrosion to flap valve. Minor cracks and vegetation growth on headwall. Pipe has minor leaf debris but no blockages or damage.

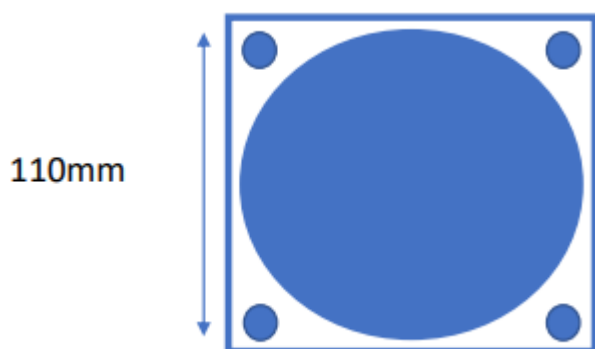
Grade = 2, Good

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL11 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.10 Comments

Ivy growth around frame and headwall. No corrosion to flap valve. Minor cracks and vegetation growth on headwall. Pipe has vegetation debris but no blockages or damage.

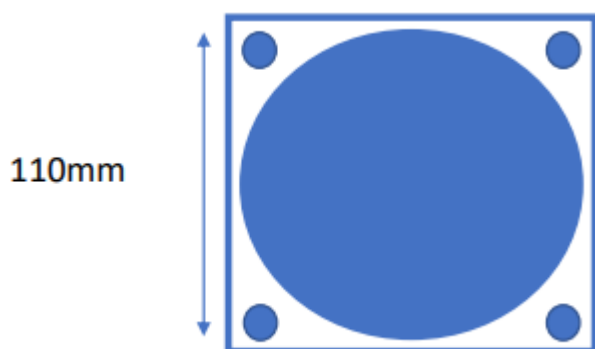
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL12 – Outfall

110mm diameter flapped highway outfall located within stone wall.



4.1.11 Comments

No corrosion to flap valve or frame. Minor cracks, mortar loss and minor vegetation growth on headwall. Pipe has minor leaf debris but no blockages or damage.

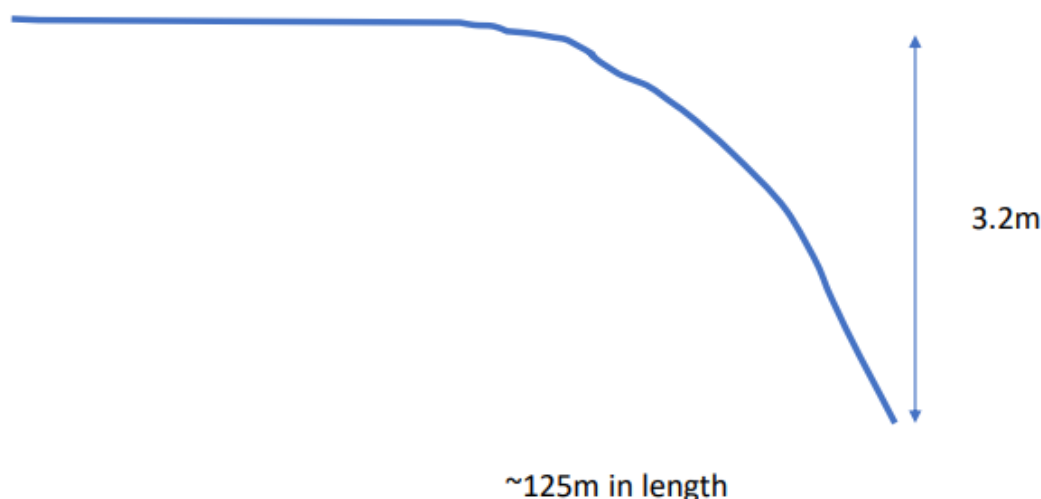
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct annual visual asset inspections and maintain surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue with annual inspections of the outfall - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall	£3,500.00
10	- Continue with annual inspections of the outfall - Continue with vegetation management - Conduct small brick and mortar repairs on headwall	£6,900.00
15	- Continue with annual inspections of the outfall and vegetation management - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£14,800.00



CL13 – Natural High Ground

Stretch of natural high ground with vegetation and trees.



4.1.12 Comments

Significant undermining, erosion, and presence of light foreign objects on channel side. High ground in good condition.

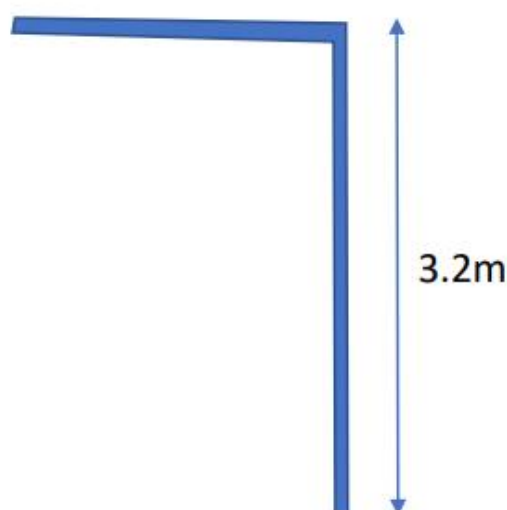
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct visual asset inspections annually, monitor erosion and ensure vegetation is kept stable and not blocking channel	£700.00
5	- Continue to inspect high ground yearly to keep track of and identify potential issues - Continue with vegetation management and remove unstable trees	£5,500.00
10	- Continue yearly inspections and vegetation management - If considerable amounts of erosion are being incurred to the channel side, install erosion protection matting	£17,900.00
15	- Continue yearly inspections and vegetation management - If extensive erosion has been incurred to the channel side, consider reprofiling bank and installing further erosion protection measures such as rock armour	£34,200.00



CL14 – Engineered High Ground

Masonry retaining wall at edge of road with metal fencing above.



~20m in length

4.1.13 Comments

Light foreign objects and ivy growing in front of and on top of channel side wall. High ground is road in good condition. Heavy foreign object upstream with roots growing into channel side brickwork.

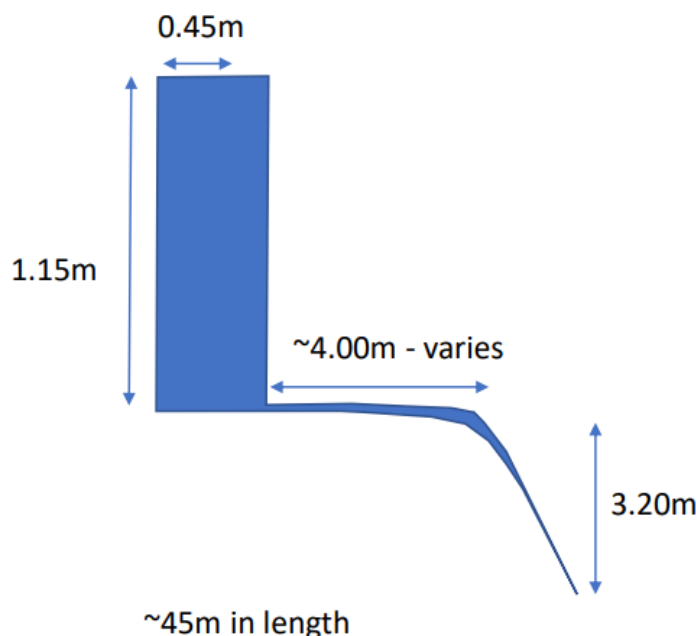
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	Conduct visual asset inspections annually and cut back surrounding vegetation to avoid damaging asset	£600.00
5	- Continue with annual visual asset inspections and vegetation management - Conduct small brick and mortar repairs	£1,100.00
10	- Continue with annual visual asset inspections and vegetation management - Consider repointing brickwork	£2,200.00
15	- Continue with annual visual asset inspections and vegetation management - If there has been any serious structural damage to the engineered high ground such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£12,000.00



CL15 – Wall

Masonry wall with capping stones with berm and channel side heavily vegetated with tree growth through wall.



4.1.14 Comments

Several heavy foreign objects on berm and channel side. Severe mortar loss in landward face, exposed face difficult to inspect but wall covered in ivy and some tree roots and growing through it. Crest is uneven where ivy has grown around it.

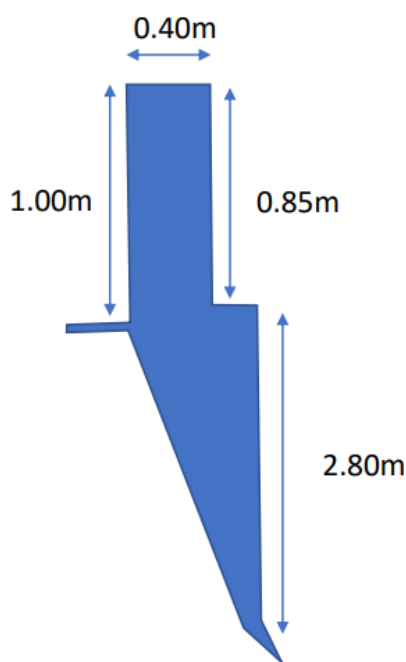
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Conduct visual asset inspections annually - Maintain surrounding vegetation including ivy removal to avoid wall incurring structural damage	£200.00
5	- Continue to inspect the wall yearly to keep track of and identify potential issues - Small repairs to brickwork and management of surrounding vegetation	£1,200.00
10	Carry out repointing of wall and continue with small repairs to brickwork and management of surrounding vegetation	£2,400.00
15	If there has been any serious structural damage to the wall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£7,700.00



CL16 – Wall

Brick wall with concrete landward face connecting to channel side brick retaining wall.



~30m in length

4.1.15 Comments

Extensive ivy growth, channel side wall is walling down with severe brick loss and root penetration. Heavy foreign objects growing on channel side causing brick displacement and loss. Crest is uneven due to brick loss but landward face is made from concrete slabs in good condition.

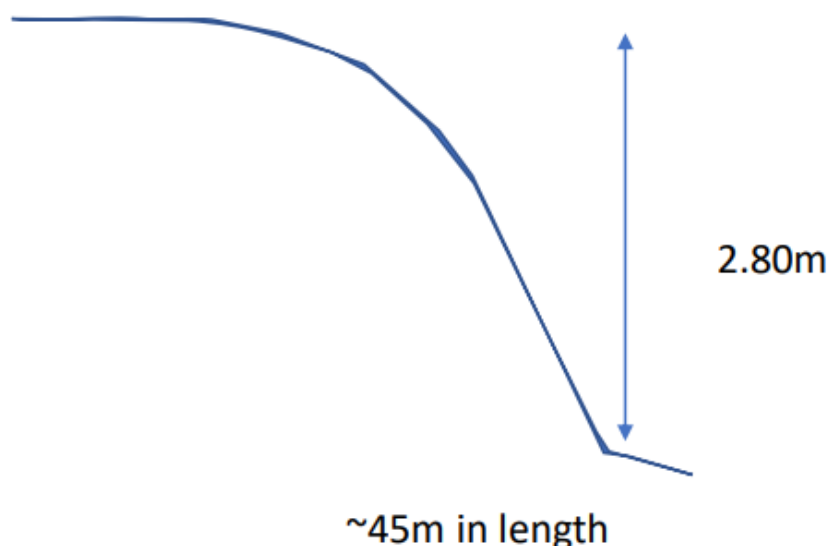
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Conduct visual asset inspections annually - Maintain surrounding vegetation to avoid wall incurring structural damage	£200.00
5	- Continue to inspect the wall yearly to keep track of and identify potential issues - Small repairs to brickwork and management of surrounding vegetation	£1,200.00
10	Carry out repointing of wall and continue with small repairs to brickwork and management of surrounding vegetation	£4,800.00
15	If there has been any serious structural damage to the wall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£8,200.00



CL17 – Natural High Ground

Natural high ground heavily vegetated with tree growth with brick building directly behind.



4.1.16 Comments

Heavy foreign objects on channel side leaning towards channel. Building <3m from channel on high ground.

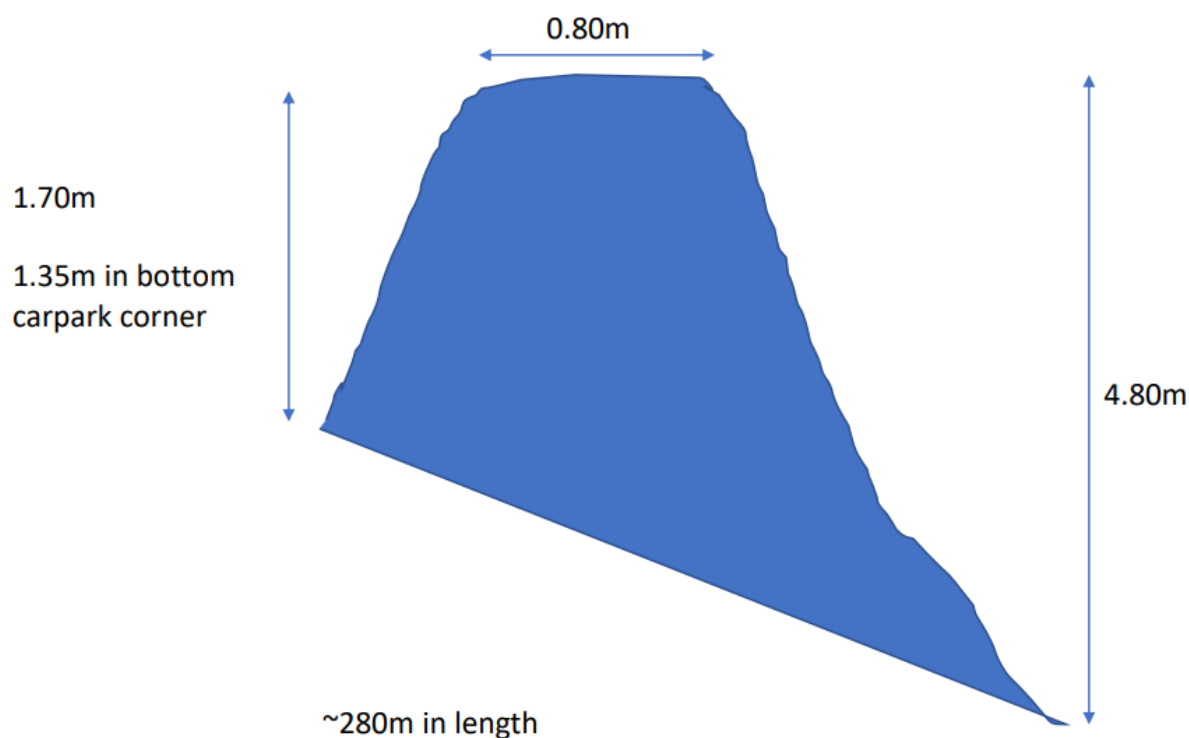
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Remove unstable trees - Conduct visual asset inspections annually, monitor erosion and movement which could affect nearby building - Ensure vegetation is kept stable and not blocking channel	£200.00
5	- Continue to inspect high ground yearly to keep track of and identify potential issues - Continue with vegetation management and remove unstable trees	£1,200.00
10	- Continue yearly inspections and vegetation management - If considerable amounts of erosion are being incurred to the channel side, install coir erosion protection matting	£4,800.00
15	- Continue yearly inspections and vegetation management - If extensive erosion has been incurred to the channel side, consider reprofiling bank and installing further erosion protection measures such as rock armour	£8,200.00



CL18 – Embankment

Earth embankment with unknown construction materials and unstable tree-ridden channel side, reducing stability of embankment. Unlikely to have clay core and may be comprised of waste material.



4.1.17 Comments

Low points and rutting in crest but well vegetated. Variant used for exposed face due to steepness. Exposed and landward faces have isolated bare patches. Telegraph pole behind embankment but embankment build around it. Severe undermining of channel side around heavy foreign objects with extensive root exposure.

Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Consider installing erosion protection to channel side such as rock armour - Inspect embankment annually and infill any identified low spots on crest with topsoil and lay down grass seed - Manage vegetation to avoid undesirable vegetation growth	£7,200.00
5	Continue to inspect the embankment yearly to keep track of, identify potential issues and monitor stability of telegraph pole within embankment	£33,400.00

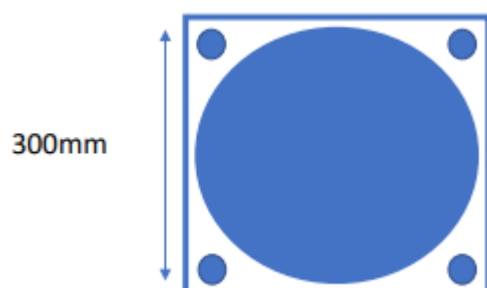


	• Continue vegetation management to prevent the growth of undesirable vegetation on embankment • Infill identified low spots on crest with topsoil and lay down grass seed	
10	• Continue yearly inspections and vegetation management • Infill any identified low spots on crest with topsoil and lay down grass seed • If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed	£90,100.00
15	• Continue yearly inspections and vegetation management • Infill any identified low spots on crest with topsoil and lay down grass seed • If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed • Consider employing engineer to assess asset condition in detail to identify potential structural issues with embankment, employ relevant operative to repair damage	£166,600.00



CL19 – Outfall

300mm outfall on channel side of embankment with damaged concrete headwall.



4.1.18 Comments

Drainage pipe halfway between wall and building on high ground. Unable to see through pipe and no CCTV footage available. Vegetation around headwall and at base of pipe.

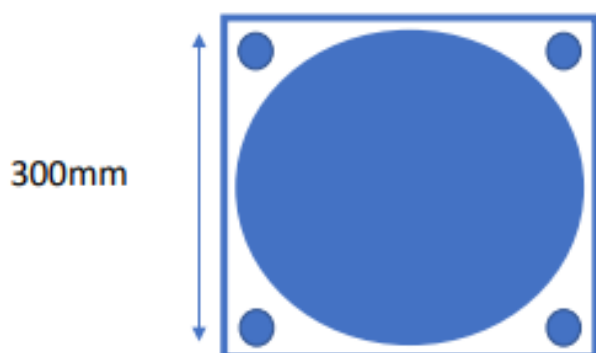
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Investigate stability of headwall, rebuild if necessary - Conduct CCTV inspection of pipe to assess condition - Conduct annual visual asset inspections and provide ongoing management of surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue to inspect the outfall yearly, including CCTV inspections of the pipe every 5 years - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall - Carry out small repairs to any brick and mortar loss on headwall	£3,500.00
10	- Continue yearly inspections of outfall including CCTV inspections of pipe every 5 years - Continue with vegetation management - Carry out small repairs to any brick and mortar loss on headwall	£6,900.00
15	- Continue yearly inspections of outfall and manage vegetation growth - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ relevant operative to repair damage	£17,400.00



CL20 – Outfall

150mm clay drainage pipe located on channel side of embankment surrounded by rocks providing unstable headwall.



4.1.19 Comments

Downstream headwall in pieces. Unable to see through pipe and no CCTV footage available.

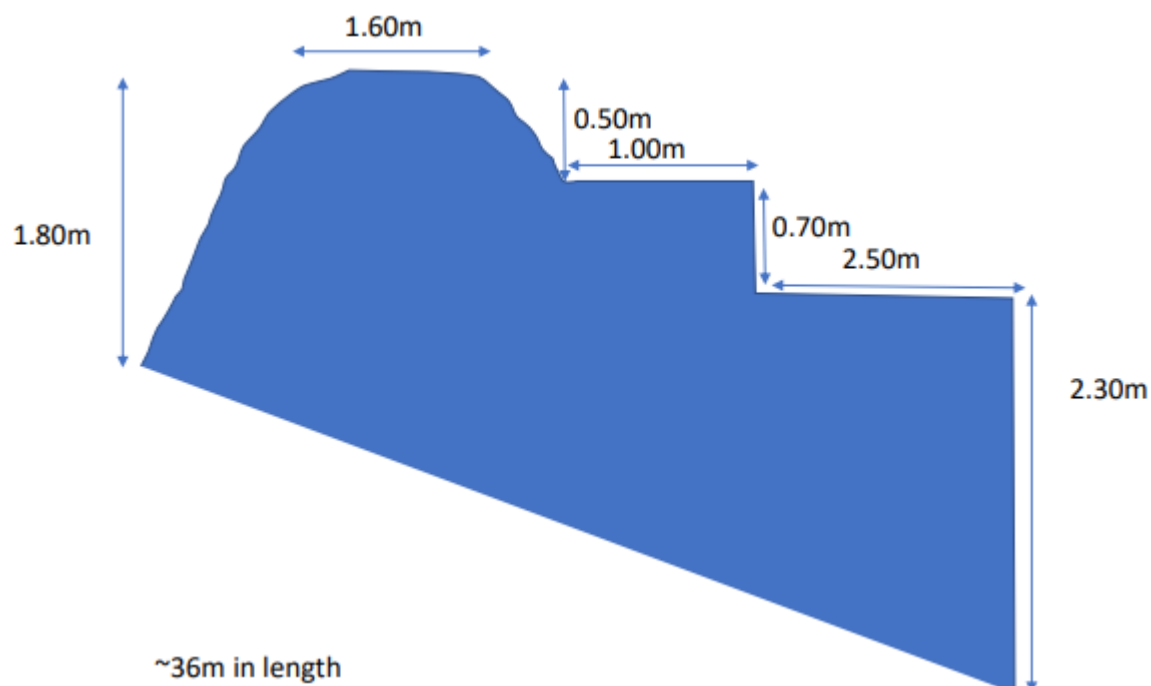
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Rebuild headwall - Conduct CCTV inspection of pipe to assess condition - Conduct annual visual asset inspections and provide ongoing management of surrounding vegetation to avoid damage incurring to outfall	£600.00
5	- Continue to inspect the outfall yearly, including CCTV inspections of the pipe every 5 years - Monitor and remove moss growth and vegetation growth on headwall to reduce damage to the headwall - Carry out small repairs to any brick and mortar loss on headwall	£3,500.00
10	- Continue yearly inspections of outfall including CCTV inspections of pipe every 5 years - Continue with vegetation management - Carry out small repairs to any brick and mortar loss on headwall	£6,900.00
15	- Continue yearly inspections of outfall and manage vegetation growth - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ relevant operative to repair damage	£17,400.00



CL21 – Embankment

Earth embankment with gabion basket and sheet piling exposed faces and concrete berm.



4.1.20 Comments

Berm 2 and channel side in good condition with minor cosmetic defects to sheet piles. Vegetation growth through gabion baskets with a few broken wires but no gabion displacement. Uneven ground on exposed face 1 and landward face but well vegetated. Rutting and low spots in isolated places on crest. Variants used on crest as less than 4m wide and landward face due to steepness.

Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Repair gabion baskets and remove vegetation growing through - Inspect embankment annually and infill any identified low spots on crest with topsoil and lay down grass seed - Manage vegetation to avoid undesirable vegetation growth	£200.00
5	- Continue to inspect embankment yearly to keep track of, identify potential issues - Continue vegetation management to prevent growth of undesirable vegetation on embankment - Infill identified low spots on crest with topsoil and lay down grass seed	£1,100.00
10	Continue yearly inspections and vegetation management	£2,500.00

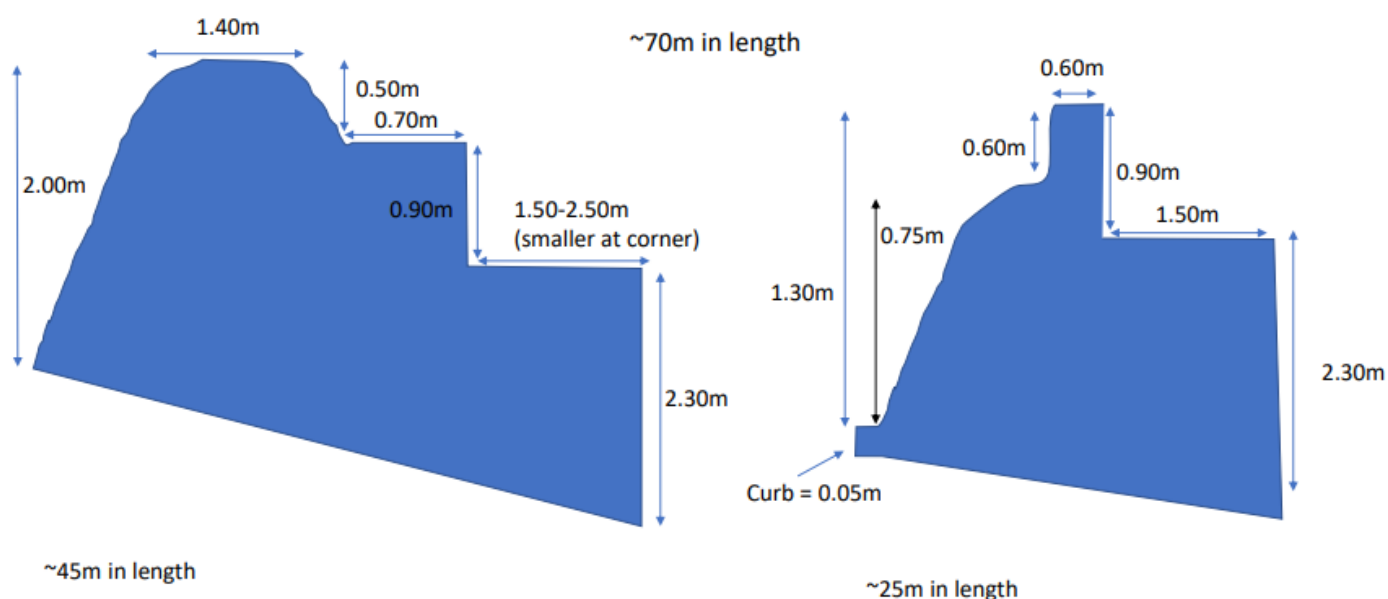


	• If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed • Repaint sheet piling • Repair any damage to gabion baskets	
15	• Continue yearly inspections and vegetation management • If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed • Repair any damage to concrete apron and gabion baskets • Consider employing engineer to assess asset condition in detail to identify potential structural issues with embankment, employ relevant operative to repair damage	£9,600.00



CL22 – Embankment

Earth embankment with stone wall and sheet piling exposed faces and concrete berm. Crest height and embankment width reduce as earth landward face diminishes and crest changes to stone crest.



4.1.21 Comments

Minor vegetation growth within berm 1 and exposed face 2 with minor mortar loss. Uneven crest with some low spots but well vegetated. Berm 2 and channel side in good condition with minor cosmetic defects to sheet piling. Landward face and exposed face 1 are well vegetated but uneven. Landward face 2 around corner and has minor vegetation growing through stone and minor mortar loss.

Grade = 3, Fair

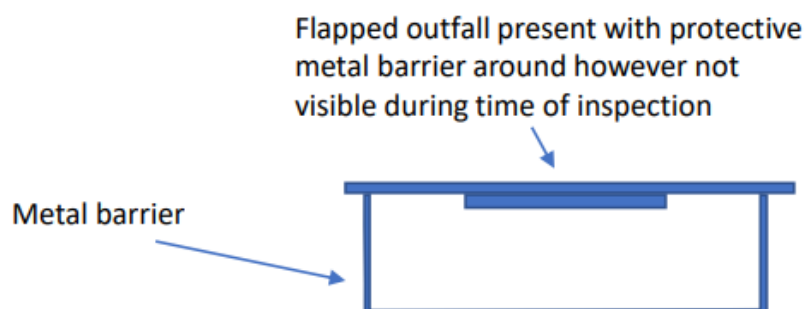
Years	Recommendations	Cumulative Cost (£)
1	- Inspect embankment annually and infill any identified low spots on crest with topsoil and lay down grass seed - Repair mortar loss and remove vegetation growing through - Manage vegetation to avoid undesirable vegetation growth	£200.00
5	- Continue to inspect embankment yearly to keep track of, identify potential issues - Continue vegetation management to prevent the growth of undesirable vegetation on embankment - Conduct small repairs on brick and mortar loss - Infill identified low spots on crest with topsoil and lay down grass seed	£1,600.00
10	Continue yearly inspections and vegetation management	£3,400.00



	• If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed • Continue with small repairs of brick and mortar loss • Repaint sheet piling • If extensive damage has been incurred to wall, rebuild wall	
15	• Continue yearly inspections and vegetation management • If extensive damage has been incurred to embankment, reprofile bank and lay down grass seed • Repair any damage to concrete apron and wall • Consider employing engineer to assess asset condition in detail to identify potential structural issues with embankment, employ relevant operative to repair damage	£9,600.00

CL23 – Outfall

Flapped outfall with unknown diameter located behind metal barrier which obstructs view of outfall.



4.1.22 Comments

Minor corrosion to barrier. Unable to see headwall and pipe due to high water level and barrier around.

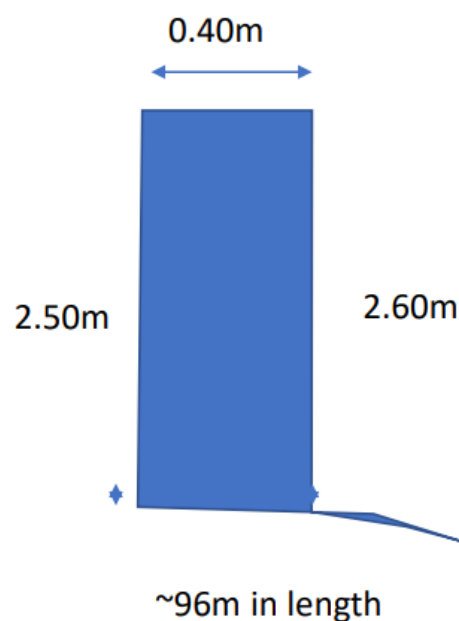
Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Investigate dimensions and condition of outfall - Carry out CCTV inspection to assess pipe condition - Conduct annual visual asset inspections to assess the condition of the asset	£600.00
5	- Continue to inspect outfall yearly, including CCTV inspections of pipe every 5 years - Monitor stability of metal barrier and replace if necessary	£3,500.00
10	- Continue yearly inspections of the outfall - Manage any vegetation growth which could damage asset	£6,900.00
15	- Continue yearly inspections of the outfall and manage vegetation growth - If there has been any serious structural damage to the outfall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£23,700.00



CL24 – Wall

High stone wall with capping stones located off right bank and going away from main channel towards village.



4.1.23 Comments

Minor vegetation growth through crest. Minor mortar loss on exposed face and a couple of holes on both faces, not whole way though. Few bricks missing for drainage

Grade = 3, Fair

Years	Recommendations	Cumulative Cost (£)
1	- Repair holes in wall and remove vegetation - Conduct visual asset inspections annually - Maintain surrounding vegetation to avoid wall incurring structural damage	£200.00
5	- Continue to inspect the wall yearly to keep track of and identify potential issues - Conduct small repairs to brick and mortar loss and manage surrounding vegetation	£1,100.00
10	Carry out repointing of wall and continue with small repairs to brickwork and management of surrounding vegetation	£2,200.00
15	If there has been any serious structural damage to the wall over time such as cracking or movement, employ an engineer to investigate. If investigations have found structural damage, employ the relevant operative to repair the damage	£9,200.00



5.0 Summary Costs of Repair and Maintenance

TABLE 2: TOTAL COST

Asset	Immediate	1 Year	5 Years	10 Years	15 Years
CL1	£400.00	£600.00	£3,500.00	£12,500.00	£16,600.00
CL2		£600.00	£3,100.00	£13,200.00	£21,500.00
CL3	£1,900.00	£200.00	£1,000.00	£2,100.00	£10,100.00
CL4		£600.00	£3,500.00	£6,900.00	£17,400.00
CL5		£600.00	£3,500.00	£6,900.00	£17,400.00
CL6	£5,000.00	£200.00	£1,000.00	£2,100.00	£11,000.00
CL7		£600.00	£3,500.00	£6,900.00	£14,800.00
CL8		£600.00	£3,500.00	£6,900.00	£14,800.00
CL9		£600.00	£3,500.00	£6,900.00	£14,800.00
CL10		£600.00	£3,500.00	£6,900.00	£14,800.00
CL11		£600.00	£3,500.00	£6,900.00	£14,800.00
CL12		£600.00	£3,500.00	£6,900.00	£14,800.00
CL13		£700.00	£5,500.00	£17,900.00	£34,200.00
CL14		£600.00	£1,100.00	£2,200.00	£12,000.00
CL15		£200.00	£1,200.00	£2,400.00	£7,700.00
CL16		£200.00	£1,000.00	£2,000.00	£5,900.00
CL17		£200.00	£1,200.00	£4,800.00	£8,200.00
CL18		£7,200.00	£33,400.00	£90,100.00	£166,600.00
CL19		£600.00	£3,500.00	£6,900.00	£17,400.00
CL20		£600.00	£3,500.00	£6,900.00	£17,400.00
CL21		£200.00	£1,100.00	£2,500.00	£9,600.00
CL22		£200.00	£1,600.00	£3,400.00	£9,600.00
CL23		£600.00	£3,500.00	£6,900.00	£23,700.00
CL24		£200.00	£1,100.00	£2,200.00	£9,200.00
Total	£7,300.00	£18,000.00	£94,000.00	£233,700.00	£504,300.00



6.0 Summary

Overall, three of the flood assets are in poor condition, two are walls which will require reconstruction, and the first of the embankments requires the installation of a none return valve to retain its flood defence function. There are six outfalls in good condition and the remaining fourteen flood assets are in fair condition. All assets are no longer inspected by the Environment Agency and have a limited flood protection function, the capacity of the channel itself and the lower land on the opposite bank provides some protection to the site.

The associated costs from immediate action to 15 years ahead involve visual asset inspections which will allow the condition of each asset to be assessed in order to ensure the assets remain in good working order. Vegetation management is also a very consistent cost for almost all assets since root penetration and undesirable vegetation can destabilise assets which could cause them to fail. Mortar repair is a minor but regular maintenance requirement for all defences and structures containing brickwork to ensure internal degradation to brick structures is reduced.

Larger costs which may be required after a longer period of time include the replacement of sheet piling, bank reprofiling and repointing of walls. These costs would be necessary to ensure the assets remain stable.

The recommendations made in Section 4 emphasise monitoring and management to maintain assets to allow them to reach or maintain a condition grade of 3 - 'Fair'. Monitoring and management makes up most of the 5 and 10 year costings outlined in Table 2, including yearly inspections, vegetation management, and minor repair work where required.

For the 15-year period, more intrusive, structural recommendations have been made to maintain assets to achieve condition grade 3 - 'Fair'. These recommendations make assumptions that the assets will degrade over time, and that erosion of the channel side will continue. Investigations by engineers will be required to determine any further work required at the time.



Appendix A: Asset inspection logs

Asset inspection logs including photos are available to download as PDF documents.



Asset ID	CL1	Frequency		 RESILIENCE & FLOOD RISK			
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Embankment				
Asset Location	Cleator						
Description	Near to Millers Walk, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Earth				9	3
2	Landward Face	Earth				7	3
3	Exposed Face	Earth				7	3
4	Channel Side	Earth				5	3
5	Berm	Earth				5	2
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Variant weighting used for crest as <4m wide. Drainage pipe running through entire width of embankment, low spots, some animal holes and rutting on crest, Landward face and exposed face have some holes and uneven slopes but are well vegetated. Undermining, minor erosion and light foreign objects present on channel side but currently stable.						
Recommendations	Infill low spots on crest, remove drainage pipe from embankment and consider pest control.						



Asset ID		Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Channel	Asset Type - Subtype		Natural High Ground			
Asset Location	Cleator						
Description	Near to Millers Walk, Cleator						
Current Asset Condition	CL2	Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	High ground	Earth				2	2
2	Channel Side	Earth				5	3
3							
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Significant undermining, erosion and presence of light foreign objects on channel side. High ground in good condition.						
Recommendations	Monitor erosion, consider installing erosion protection layer to channel side.						



Asset ID	CL3	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Wall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Stone				7	3
2	Landward Face	Stone				9	4
3	Exposed Face	Stone				9	4
4	Channel Side	Earth				5	3
5	Berm	Earth				5	2
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override	4		
Override Reason	Critical element has lower grading						
Comments	Variant weightings used for both faces as no revetments. Significant mortar loss to crest, holes through wall, bulging of wall where light foreign objects are growing in front on wall, distorting its shape and minor erosion to channel side.						
Recommendations	Rebuild wall and remove trees in front of wall.						



Asset ID	CL4	Frequency		 RESILIENCE & FLOOD RISK			
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	2
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	3
4	Apron	Concrete				5	2
5	Downstream headwall	Stone and concrete				8	3
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override	3		
Override Reason	Critical element has lower grading						
Comments	Vegetation around headwall. Unable to see through pipe and no CCTV footage available.						
Recommendations	Conduct a CCTV survey to inspect pipe and remove vegetation around headwall.						



Asset ID	CL5	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	2
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	3
4	Downstream headwall	Stone and concrete				8	2
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override	3		
Override Reason	Critical element has lower grading						
Comments	Outfall in good condition, very minor corrosion present on frame and flap valve. Unable to see through pipe and no CCTV footage available.						
Recommendations	Conduct a CCTV survey to inspect pipe.						



Asset ID	CL6	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype		Wall			
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Stone				7	4
2	Landward Face	Stone				9	4
3	Exposed Face	Stone				9	4
4	Channel Side	Earth				5	3
5	Berm	Earth				5	3
6							
7							
8							
9							
10							
11							
Calculated	4	Worst		Override			
Override Reason							
Comments	Heavy foreign objects growing towards channel on berm and channel side and undermining on channel side causing channel side to be unstable. Ivy growth on wall, heavy foreign objects growing close to wall causing bulging to wall and capping stones lost from crest halfway across wall.						
Recommendations	Rebuild wall, remove unstable trees and remove trees next to wall.						



Asset ID	CL7	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	2
2	Flap valve	Metal				9	2
3	Pipe	Unknown				9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	No signs of corrosion to flap valve or frame, pipe has minor leaf debris but no blockages or damage. Downstream headwall has some cracks, vegetation growth and mortar loss.						
Recommendations	Continue with ongoing vegetation maintenance.						



Asset ID	CL8	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	2
2	Flap valve	Metal				9	2
3	Pipe	Unknown				9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	No signs of corrosion to flap valve or frame, pipe has minor leaf debris but no blockages or damage. Minor crack to downstream headwall, vegetation growth and mortar loss.						
Recommendations	Continue with ongoing vegetation maintenance.						



Asset ID	CL9	Frequency		 RESILIENCE & FLOOD RISK			
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype		Outfall			
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	3
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	No corrosion to flap valve or frame. Cracks and mortar loss on headwall. Pipe has minor leaf debris but no blockages or damage.						
Recommendations	Remove vegetation and continue with vegetation maintenance.						



Asset ID	CL10	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype		Outfall			
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	3
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	Ivy growth around frame and headwall. No corrosion to flap valve. Cracks and vegetation growth on headwall. Pipe has minor leaf debris but no blockages or damage.						
Recommendations	Remove vegetation and continue with vegetation maintenance.						



Asset ID	CL11	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	3
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	Ivy growth around frame and headwall. No corrosion to flap valve. Minor cracks and vegetation growth on headwall. Pipe has vegetation debris but no blockages or damage.						
Recommendations	Remove vegetation and continue with vegetation maintenance.						



Asset ID	CL12	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype		Outfall			
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Frame	Metal				7	3
2	Flap valve	Metal				9	2
3	Pipe	Unknown			X	9	2
4	Downstream headwall	Stone and concrete				8	3
5							
6							
7							
8							
9							
10							
11							
Calculated	2	Worst		Override			
Override Reason							
Comments	No corrosion to flap valve or frame. Minor cracks, mortar loss and minor vegetation growth on headwall. Pipe has minor leaf debris but no blockages or damage.						
Recommendations	Remove vegetation and continue with vegetation maintenance.						



Asset ID	CL13	Frequency						
Latest Assessment Date	28/01/2022	Due Date						
Asset Inspector	Alexandra Mackaness							
Asset Name	Channel	Asset Type - Subtype		Natural High Ground				
Asset Location	Cleator							
Description	Near to Millers Walk, Cleator							
Current Asset Condition		Target condition	3					
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition	
1	High ground	Tarmac				2	2	
2	Channel Side	Earth				5	3	
3								
4								
5								
6								
7								
8								
9								
10								
11								
Calculated	3	Worst		Override				
Override Reason								
Comments	Significant undermining, erosion and presence of light foreign objects on channel side. High ground in good condition.							
Recommendations	Monitor erosion, consider installing erosion protection layer to channel side.							



Asset ID	CL14	Frequency						
Latest Assessment Date	28/01/2022	Due Date						
Asset Inspector	Alexandra Mackaness							
Asset Name	Channel	Asset Type - Subtype	Natural High Ground					
Asset Location	Cleator							
Description	Near to Millers Walk, Cleator							
Current Asset Condition		Target condition	3					
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition	
1	High ground	Tarmac				2	2	
2	Channel Side	Earth				5	3	
3								
4								
5								
6								
7								
8								
9								
10								
11								
Calculated	3	Worst		Override				
Override Reason								
Comments	Light foreign objects and ivy growing in front of and on top of channel side wall. High ground is road in good condition. Heavy foreign object upstream with roots growing into channel side brickwork.							
Recommendations	Remove trees on top of and in front of channel side brickwork. Remove ivy.							



Asset ID	CL15	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Wall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Stone				7	3
2	Landward Face	Stone				9	3
3	Exposed Face	Stone				9	3
4	Channel Side	Earth				5	3
5	Berm	Earth				5	3
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Several heavy foreign objects on berm and channel side. Severe mortar loss in landward face, exposed face difficult to inspect but wall covered in ivy and some tree roots and growing through it. Crest is uneven where ivy has grown around it.						
Recommendations	Rebuild wall, remove ivy and remove trees growing into wall.						



Asset ID	CL16	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Wall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Stone				7	4
2	Landward Face	Stone				9	2
3	Exposed Face	Stone				9	3
4	Channel Side	Earth				5	4
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Extensive ivy growth, channel side wall is walling down with severe brick loss and root penetration. Heavy foreign objects growing on channel side causing brick displacement and loss. Crest is uneven due to brick loss but landward face is made from concrete slabs in good condition.						
Recommendations	Rebuild wall and remove heavy foreign objects.						



Asset ID	CL17	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Channel	Asset Type - Subtype	Natural High Ground				
Asset Location	Cleator						
Description	Near to Millers Walk, Cleator						
Current Asset Condition	3	Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	High ground	Tarmac				2	2
2	Channel Side	Earth				5	3
3							
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Heavy foreign objects on channel side leaning towards channel. Building <3m from channel on high ground.						
Recommendations	Continue with vegetation maintenance and monitor tree growth.						



Asset ID	CL18	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Embankment				
Asset Location	Cleator						
Description	Near to Millers Walk, Cleator						
Current Asset Condition	4	Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Earth				9	3
2	Landward Face	Earth				9	3
3	Exposed Face	Earth				9	3
4	Channel Side	Earth				7	4
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Low points and rutting in crest but well vegetated. Variant used for exposed face due to steepness. Exposed and landward faces have isolated bare patches. Telegraph pole behind embankment but embankment build around it. Severe undermining of channel side around heavy foreign objects with extensive root exposure.						
Recommendations	Remove unstable trees on channel side, infill low spots on crest and seed bare patches.						



Asset ID	CL19	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Pipe	Unknown			X	9	3
2	Apron	Concrete				5	3
3	Downstream headwall	Stone and concrete				8	3
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Drainage pipe halfway between wall and building on high ground. Unable to see through pipe and no CCTV footage available. Vegetation around headwall and at base of pipe.						
Recommendations	Remove vegetation and provide ongoing vegetation maintenance. Conduct CCTV inspection of pipe.						



Asset ID	CL20	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Hilden Road, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Pipe	Unknown			X	9	3
2	Downstream headwall	Stone and concrete				8	4
3							
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Downstream headwall in pieces. Unable to see through pipe and no CCTV footage available.						
Recommendations	Rebuild headwall and conduct CCTV inspection of pipe.						



Asset ID	CL21	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Embankment				
Asset Location	Cleator						
Description	Near to Millers Walk, Cleator						
Current Asset Condition	3	Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Earth				9	3
2	Landward Face	Earth				7	2
3	Exposed Face 1	Earth				7	2
4	Berm 1	Gabions				5	3
5	Exposed Face 2	Gabions				7	3
6	Berm 2	Concrete				5	2
7	Channel Side	Sheet piling				5	2
8							
9							
10							
11							
Calculated	2	Worst		Override	3		
Override Reason	Critical element has worse condition grade						
Comments	Berm 2 and channel side in good condition with minor cosmetic defects to sheet piles. Vegetation growth through gabion baskets with a few broken wires but no gabion displacement. Uneven ground on exposed face 1 and landward face but well vegetated. Rutting and low spots in isolated places on crest. Variants used on crest as less than 4m wide and landward face due to steepness.						
Recommendations	Remove vegetation in gabions and repair wires. Infill low spots on crest.						



Asset ID	CL22	Frequency							
Latest Assessment Date	28/01/2022	Due Date							
									
Asset Inspector	Alexandra Mackaness								
Asset Name	Defence	Asset Type - Subtype						Embankment	
Asset Location	Cleator								
Description	Between Mill Street and Brookside, Cleator								
Current Asset Condition	3	Target condition	3						
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition		
1	Crest	Earth				9	3		
2	Landward Face	Earth				7	2		
3	Exposed Face 1	Earth				7	2		
4	Berm 1	Stone				5	3		
5	Exposed Face 2	Stone				7	2		
6	Berm 2	Concrete				5	2		
7	Channel Side	Sheet piling				5	2		
8	Landward face 2	Stone				7	2		
9									
10									
11									
Calculated	2	Worst		Override	3				
Override Reason	Critical element has worse condition grade								
Comments	Minor vegetation growth within berm 1 and exposed face 2 with minor mortar loss. Uneven crest with some low spots but well vegetated. Berm 2 and channel side in good condition with minor cosmetic defects to sheet piling. Landward face and exposed face 1 are well vegetated but uneven. Landward face 2 around corner and has minor vegetation growing through stone and minor mortar loss.								
Recommendations	Monitor vegetation growth in wall and infill low spots in crest.								



Asset ID	CL23	Frequency					
Latest Assessment Date	28/01/2022	Due Date					
							
Asset Inspector	Alexandra Mackaness						
Asset Name	Structure	Asset Type - Subtype	Outfall				
Asset Location	Cleator						
Description	Between Mill Street and Brookside, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Downstream headwall	Stone and concrete			X	8	3
2	Pipe	Unknown			X	9	3
3	Barrier	Metal				2	3
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Minor corrosion to barrier. Unable to see headwall and pipe due to high water level and barrier around.						
Recommendations	Conduct CCTV inspection for pipe and headwall.						



Asset ID	CL24	Frequency		 RESILIENCE & FLOOD RISK			
Latest Assessment Date	28/01/2022	Due Date					
Asset Inspector	Alexandra Mackaness						
Asset Name	Defence	Asset Type - Subtype	Wall				
Asset Location	Cleator						
Description	Brookside, Cleator						
Current Asset Condition		Target condition	3				
Element Sequence	Element Type	Material	Photo ref	Notes	ENI	Weighting	Condition
1	Crest	Stone				7	3
2	Landward Face	Stone				9	3
3	Exposed Face	Stone				9	3
4							
5							
6							
7							
8							
9							
10							
11							
Calculated	3	Worst		Override			
Override Reason							
Comments	Minor vegetation growth through crest. Minor mortar loss on exposed face and a couple of holes on both faces, not whole way though. Few bricks missing for drainage.						
Recommendations	Repair holes in wall and remove vegetation.						



Appendix E

Envireau Water Breach Analysis

UPDATED FLOOD RISK MODELLING REPORT

CLEATOR MILLS



For

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TABLE OF CONTENTS

1	INTRODUCTION.....	1
1.1	Background.....	1
1.2	Location and Setting.....	1
1.3	Scope of Breach Analysis.....	1
2	BREACH ANALYSIS.....	2
2.1	Breach Scenarios	2
2.2	Breach Methodology	2
3	2D HYDRODYNAMIC MODELLING.....	3
3.1	Approach	3
3.2	Model Build	3
3.2.1	Digital Terrain Model.....	4
3.2.2	Boundary Conditions	4
3.2.3	Manning's n	4
3.3	Flood Hazard Classification.....	5
4	RESULTS	6
4.1	Breach 1.....	6
4.2	Breach 2.....	6
5	FLOOD MAPPING	7
6	ASSUMPTIONS AND LIMITATIONS.....	7
7	CONCLUSIONS.....	8
	REFERENCES	9

FIGURES

Figure 1	Site Setting
Figure 2	Flood Defence Breach Locations
Figure 3	Flood Defence Breach Hydrographs
Figure 4	Breach 1 Flood Wave Progression
Figure 5	Breach 2 Flood Wave Progression

TABLES

Table 1	Breach Location and Details
Table 2	Flood Defence and Floodplain Elevations
Table 3	2D Model Grid Details
Table 4	Manning's n Values for Land Use Classifications
Table 5	Debris Factor for Land Use and Flood Depth (Table 4.1, FD2331/TR2)
Table 6	Hazard to People as a Function of Depth and Velocity (Table 4.2, FD2331/TR2)
Table 7	Summary of Flood Maps

APPENDICES

Appendix A	Previous Model Report
Appendix B	RWO Associates Topographical Survey
Appendix C	Breach 1 Flood Maps – Figures 6a, 6b, 6c and 6d
Appendix D	Breach 2 Flood Maps - Figures 7a, 7b, 7c and 7d

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Revision	Details	Completed by	Date	Checked by	Date
REV01	Final	RH	27/02/2020	LC	02/03/2020
REV02	Revision 1	RH	01/06/2022	LC	06/06/2022
REV03					
REV04					

UPDATED FLOOD RISK MODELLING REPORT

CLEATOR MILLS

1 INTRODUCTION

1.1 Background

Envireau Water has been commissioned to provide an updated flood defence breach analysis at Cleator Mills, Cleator, Cumbria, CA23 3DU. Envireau Water have previously submitted an updated to the flood defence breach analysis in February 2020. Since completing this work a factory has been removed from the site. Therefore this assessment has been updated further (Revision 1) to reflect this topographical change.

The work follows on from a previous flood defence breach analysis undertaken by Mott MacDonald based on the Environment Agency hydraulic model produced in 2010. The previous modelling report is provided in Appendix A.

This report describes the methodology and results of the two-dimensional modelling and mapping of the flood defence breach scenarios.

1.2 Location and Setting

Cleator Mills (the "Site") is located to the south-east of Cleator Moor Village (Figure 1). The Site is centred on National Grid Reference NY 02067 13818. The River Ehen located adjacent to the north and eastern boundaries of the Site. The Site is split into three areas, the Kangol factory which has been removed (Removed Factory), a disused Kangol factory (Disused Factory) and a car park area. The flood defences are located between the river and Site.

1.3 Scope of Breach Analysis

The scope of the flood defence breach analysis is summarised below:

- Build a 2D model of the Site to replace the previous model developed by Mott MacDonald in 2013 which is not available.
- Obtain and apply new topographic survey information provided by RWO Associates (Appendix B) and LiDAR 1m Digital Terrain Model (DTM) from the Environment Agency dated 2013 (Ref. 1).
- Develop breach hydrographs using the updated 2016 Environment Agency hydraulic model for the River Ehen. The model was built and run using linked Flood modeller TUFLOW simulations.
- Prediction of flood extent, depth, velocities and hazard ratings for the 1 in 100 year plus climate change flood defence breach at two locations.

2 BREACH ANALYSIS

2.1 Breach Scenarios

Two breach scenarios have been analysed in the updated assessment. The locations for the flood defence breaches were agreed with the Environment Agency in March 2010 and remain unchanged. Details of the two scenarios are provided in Table 1 below and shown on Figure 2.

Table 1 Breach Location and Details

Breach Scenario	Location	Defence Type	Breach Width (m)	Point X	Point Y	Elevation (mAOD)	Bank
Breach 1	North of Site	Combination of gabion lined baskets and earth embankment	40	302196	513947	64.52	Right Bank
Breach 2	East of Site	Earth Embankment	40	302202	513840	62.49	Right Bank

The following criteria was agreed with the Environment Agency for the previous assessment and maintained for this update:

- One design event to be assessed – 1 in 100 year plus climate change.
- As both breach locations are on a fluvial river, the following breach width and time apply:
 - Combination of hard defence and earth bank: 40m width, 36 hours to closure.
 - Earth banks: 40m width, 36 hours to closure.
- The start of the breach is the bank-full condition or at the peak water level if lower.

2.2 Breach Methodology

The method used to assess the flood defence breach has been maintained from the previous assessment to ensure consistency between the two results. The method applied is summarised below.

- Review the updated Environment Agency hydraulic model which covers the entire River Ehen, including the two breach locations.
- Spill units representing the breach locations within the Environment Agency model were identified. Where necessary an interpolated channel cross section was added 40m downstream of the breach to ensure a breach width of 40m was achieved. Spill units that represent the breaches floodplains within the Environment Agency model are represented by 1D reservoir units with water exchanged between the river and floodplain via spill units.
- Where an interpolation was required a spill unit to connect it to the 1D reservoir unit was added to ensure all flood water from the main channel was captured.

- The breach was assumed to develop within a single one second timestep in the model run across the full 40m width. This represents a worst case scenario for the breach assessment.
- The breach was assumed to occur through the full embankment height to the surrounding ground level. This was represented within the Environment Agency model by lowering the elevation of the right bank spill at the breach location from the embankment level to the level of the surrounding floodplain.
- The level of the surrounding flood plain was obtained from the topographical survey provided by RWO Associates and 2013 Environment Agency LiDAR data. Table 2 identifies the embankment and floodplain elevation used within the model for each Breach. The floodplain elevations are above those used in the previous model due to the updated topographical survey and Environment Agency LiDAR data differing from that used in the previous model.

Table 2 Flood Defence and Floodplain Elevations

Breach Number	Flood Defence Elevation (mAOD)	Floodplain Elevation (mAOD)
Breach 1	64.52	62.6
Breach 2	62.49	61.5

- The hydrographs for the spill units representing the breach locations were used as an input to a 2D model of the Site to establish the flood depth, extent, velocity and hazard rating from each breach event.

3 2D HYDRODYNAMIC MODELLING

3.1 Approach

The 2D modelling approach is outlined below for assessing the two flood defence breaches for the 1 in 100 year plus climate change event:

1. Construct a 2D hydraulic model incorporating topographic data provided by RWO Associates and Environment Agency 1m LiDAR data dated 2013;
2. Insert the breach hydrographs for each scenario extracted from the updated Environment Agency River Ehen model;
3. Predict flood extents at the site for the specified return period of 1 in 100 year plus climate change;
4. Produce flood extent, depth, velocity and hazard maps.

The model was built and run within Flood Modeller v4.6.

3.2 Model Build

The model extent has been iteratively adjusted to cover a sufficient length of the River Ehen and the maximum flood plain extent which is flooded during the breach assessments. The same model extent was used for both breach scenario.

3.2.1 Digital Terrain Model

The DTM for the Site was produced using the topographical survey and 1m resolution LiDAR dated 2013. To make sure flood water from the breach was not underestimated the DTM was edited to raise the channel elevation to the bank elevation. This ensured the watercourse channel was not available for storage or conveyance of the 'breached flows'. This is in accordance with the breach occurring at the same time as bank full conditions with the River Ehen.

Details of the grid used within the model is summarised in Table 3, each cell within the grid is assigned a z value, which is the elevation in mAOD. The previous assessment used a grid size of 7m, for this assessment a grid size of 5m was determined to provide sufficient detail for flood mapping, whilst not creating onerous model run times.

Table 3 2D Model Grid Details

Grid Information	
Grid Size (spacing)	5 m
Origin	301,135N 512,883E (British National Grid)
Orientation	0 degrees
Width of grid (in the east direction)	1260 m
Height of grid (in the north direction)	1051 m

3.2.2 Boundary Conditions

The inflow (upstream) boundary is a flow-time boundary assigned to the breach location via a polyline shapefile. The breach hydrograph extracted from the updated Environment Agency model was assigned to the polyline to simulate the flood defence breach. The breach hydrographs are shown in Figure 3.

The peak flow for Breach 2 is greater than the peak flow for Breach 1. We have assumed this is different from the previous model due to the inclusion of flow re-entering the River Ehen from the floodplain between Breach 1 and Breach 2 in the updated Environment Agency model. However, we would naturally expect to see a higher flow at Breach 2 than at Breach 1.

3.2.3 Manning's n

A roughness grid was applied to the 2D grid based on land classification. The roughness values (Table 4) allows the model to calculate the resistance provided by the land to the flood water.

Table 4 Manning's n Values for Land Use Classification.

Land Classification	Manning's n (Roughness)
Water	0.035
Grassed floodplain	0.055
Buildings	0.300
Woodland	0.120
Roads and railways	0.020

3.3 Flood Hazard Classification

The hazard rating has been defined using the method outlined in Defra's Flood Risks to People report (FD2321/TRA) (Ref 2). The hazard rating is calculated from depth, velocity and debris factor at each time step in the model. The equations governing this calculation are provided below:

$$HR = d (v + 0.5) + DF$$

Where, HR = (flood) hazard rating;

D = depth of flooding (m);

V = velocity of floodwaters (m/s); and

DF = debris factor

The debris factor varies with depth and velocity for each land use classification as shown in Table 5. The debris factor used within the flood mapping is Urban as the Site is occupied as a factory and used for car parking with no extensive woodland coverage.

Table 5 Debris Factor for Land Use and Flood Depths (Table 4.1, FD2321/TRA)

Depths	Debris Factor		
	Pasture/Arable	Woodland	Urban
0 to 0.25 m	0	0	0
0.25 to 0.75 m	0	0.5	1
d>0.75m and/or v>2	0.5	1	1

Hazard rating (HR) has been classified into four categories as defined within FD2321/TRA, the categories are listed in Table 6.

Table 6 Hazard to People as a Function of Depth and Velocity (Table 4.2, FD2321/TRA)

Hazard Rating	Degree of Flood Hazard	Description
<0.75	Low	Caution <i>"Flood zone with shallow flowing water or deep standing water"</i>
0.75 – 1.25	Moderate	Dangerous for some (e.g. children) <i>"Danger: Flood zone with deep or fast flowing water"</i>
1.25 – 2.0	Significant	Dangerous for most people <i>"Danger: flood zone with deep fast flowing water"</i>
> 2.5	Extreme	Dangerous to all <i>"Extreme danger: flood zone with deep fast flowing water"</i>

4 RESULTS

4.1 Breach 1

During a 1 in 100 year plus climate change event flood defence breach at location 1 flood water flows onto the floodplain progressing south flooding the Removed Factory. Water then flows across the Removed Factory and car park area. Water flows around the disused factory downstream. Flood water re-enters the River Ehen near the Removed Factory at the eastern car parking area. Figure 4 shows the progression of the flood wave across the Site from the initial time at which the flood breaches fail ($t = 0$ hour) to the maximum flood extent ($t = 4.5$ hour).

Flood depths in the vicinity of the Removed Factory is up to 0.54m near with depths up to 0.62m around the Disused Factory. Water depths in the car parking area range from 0.4m to 0.15m. The remainder of the floodplain flood depth typically reaching 0.15m.

The velocity reaches a maximum of 3.2m/s at the Site. The highest velocities are located close to the breach location and along the eastern edge of the Site adjacent to the River Ehen. Velocities slowly dissipate as water travels across the Removed Factory reducing to 0.25m/s to 0.55m/s around the Disused Factory.

The hazard rating for the Site is typically Low (<0.75), however the hazard increased in areas with deeper flooding or higher velocities. These areas are located along the breach flow pathway adjacent to the right bank of the River Ehen and around the Removed Factory and on the northern extent of the Disused Factory. The hazard level of these areas are Moderate to Significant indicating that it would be dangerous to people during a flood defence breach.

Compared to the previous assessment the maximum flood depth has increased from 0.9m to 1.46m where flood water re-enters the River Ehen, this in turn has increased the hazard rating in these areas of the Site. However the maximum flood extent at the Site remains the same. The velocities experienced on site are slightly increased from those predicted in the previous breach due to the higher peak in the breach hydrograph.

4.2 Breach 2

During a 1 in 100 year plus climate change event flood defence breach at location 2, flood water flow onto the floodplain and flows across the site of the Removed Factory. As the breach progresses water flows towards the disused factory with some water re-entering the River Ehen downstream of the breach location. Figure 5 shows the progression of the flood wave across the Site from the initial time at which the flood defence fails ($t = 0$ hour) to the maximum flood extent ($t = 5.5$ hour).

Flood depths in the vicinity of the Removed Factory are generally below 0.5m with an isolated area at the breach location experiencing depths up to 0.7m. Flood depths at the car park reach 0.55m. Flood depths at the Disused factory reach 0.9m with the remainder of the floodplain typically reaching 0.27m.

The velocity reaches a maximum of 2.18m/s at the Site, high velocities are experienced at the breach location and to the west of the Disused Factory.

The hazard rating for the Site during Breach 2 is typically Low (<0.75), however like Breach 1 there are areas of higher hazards associated with deeper flooding or higher velocities. These areas are located at the breach location, at locations of higher flood depths around the Disused Factory and along the bank of the River Ehen. The hazard level of these areas are moderate to significant indicating that it would be dangerous to people during a flood defence breach.

In comparison to the previous assessment the maximum flood extent has increased due to the updated Environment Agency hydraulic model incorporating flow back into the River Ehen from the floodplain upstream. This has resulted in a higher peak in Breach 2's hydrograph compared to Breach 1's.

The flood depth has also increased under Breach 2 scenario from 0.5m to 0.7m in the vicinity of the existing factory. This has increased velocities and hazard ratings at the site as a result of the increased volume and peak in the flood defence breach hydrograph. Therefore, although the hazard rating for the Site is typically Low, the area small areas with a hazard rating rising to moderate or significant.

5 FLOOD MAPPING

Flood maps have been produced from the outputs of the 2D model. The maps show the maximum depth, velocity, water level and hazard rating for each Breach individually. Flood maps figures for Breach 1 (Figure 6a – 6d) are provided in Appendix C and flood maps figures for Breach 2 (Figure 7a – 7d) are provided in Appendix D. Table 7 summarise the flood maps.

Table 7 Summary of Flood Maps

Figure Number	Parameter Shown	Breach Location	Return Perion
6a	Depth	Breach 1	100 year + Climate Change
6b	Velocity	Breach 1	100 year + Climate Change
6c	Water Level	Breach 1	100 year + Climate Change
6d	Hazard Rating	Breach 1	100 year + Climate Change
7a	Depth	Breach 2	100 year + Climate Change
7b	Velocity	Breach 2	100 year + Climate Change
7c	Water Level	Breach 2	100 year + Climate Change
7d	Hazard Rating	Breach 2	100 year + Climate Change

6 ASSUMPTIONS AND LIMITATIONS

The following assumptions were made within the model:

- The River Ehen is at bank-full levels downstream of the breach.
- Flood defence and embankment levels within the updated Environment Agency model are correctly representing the modelled area.
- The updated Environment Agency model accounts for surface runoff within the modelled area.
- The Site is an urban environment with no extensive woodland or pastureland.

The following limitations apply to the hydraulic model:

- LiDAR data has a verified vertical accuracy of +/- 15cm.
- Models are not calibrated or verified for flood extent due to breaches due to the lack of observed historic data.
- The updated Environment Agency model was only run to peak producing results for 25 hours. To run the dam breaches for 36 hours to closure, the rising limb has been used as a proxy for the falling limb.

7 CONCLUSIONS

An updated flood defence breach analysis has been undertaken for two breach locations adjacent to Cleator Mills. The breach assessment methodology has been maintained from previous assessment to ensure consistency between assessments. The breach hydrographs have been updated applying the updated Environment Agency 2016 River Ehen hydraulic model results.

A new 2D hydraulic model was constructed using a grid assigned levels from a DTM and flow-time boundary conditions representing the inflow from the flood defence breach. The 2D model grid covered an area representing the potential for flooding from the breach with a grid size of 5m.

A flood defence breach at location 1 would result in extensive flooding of the Site. The main areas affected are the Removed Factory and car park area and the Disused Factory downstream of the Site. The hazard rating for the majority of the Site was Low, however there were areas that had a Moderate to Significant hazard rating where the flood depth was greater. In these areas the breach poses a significant risk to people.

A flood defence breach at location 2 would result in less extensive flooding with flood water covering the Removed Factory, car parking area and area around the Disused factory. Similar to Breach, 1 the hazard rating for the majority of the Site was Low, with areas experiencing greater flood depths having a Moderate to Significant hazard rating. These areas pose a significant risk to people during a flood defence breach at location 2.

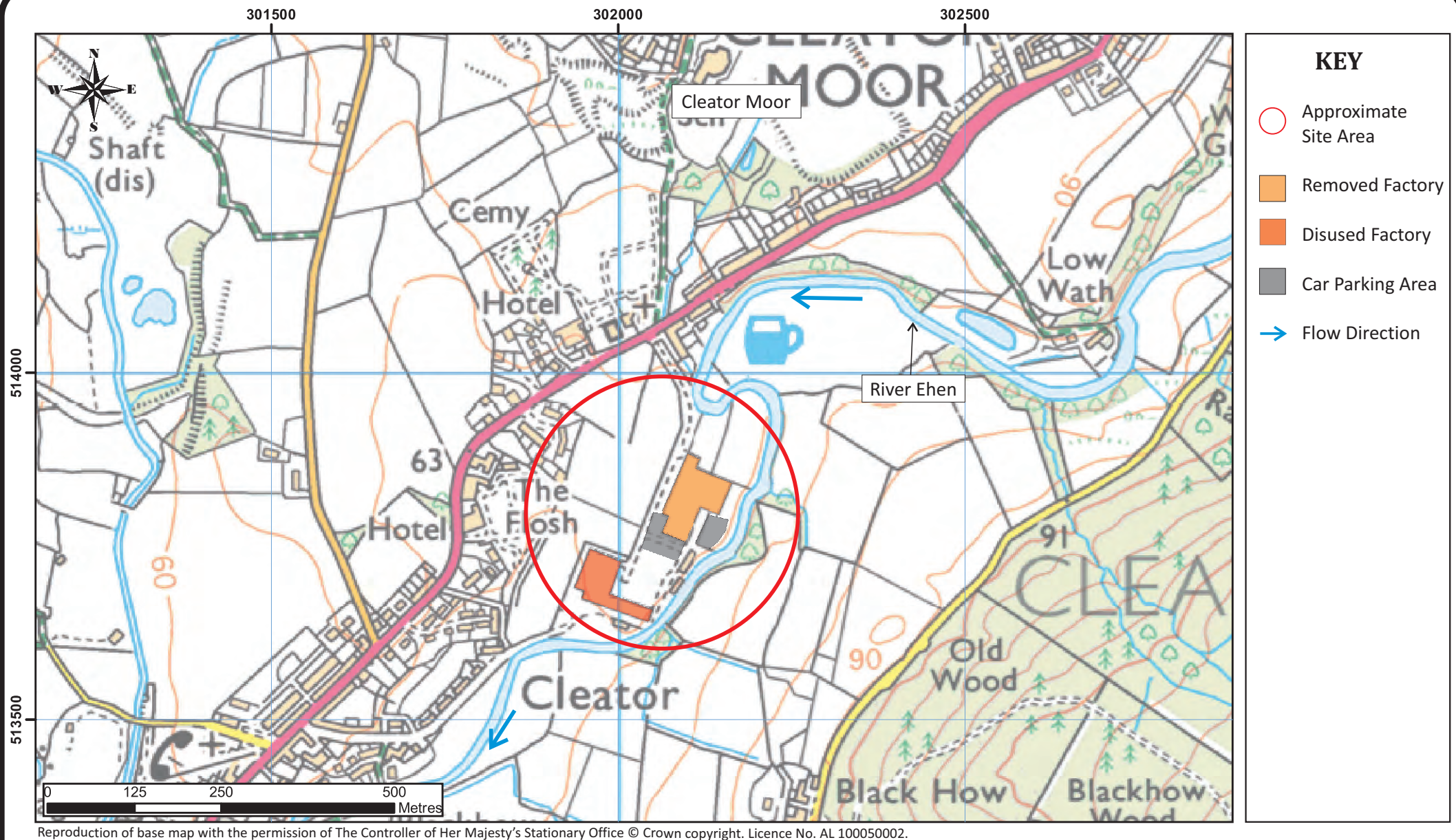
The extent of flooding experienced in Breach 1 remains similar to that experienced in the previous assessment however the flood extent in Breach 2 is increased from that identified in the previous assessment. The flood depths for both assessments are increased. The increased depths on Site have resulted in an increase in hazard ratings in these areas, however the majority of the Site remains within the Low hazard category.

Envireau Water
06/06/2022

REFERENCES

- Ref.1 Environment Agency (2013). LIDAR Tiles DTM: 2013 DTM 1M.
<https://environment.data.gov.uk/DefraDataDownload/?Mode=survey>
- Ref.2 DEFRA (2006). Flood Risks to People – Phaser 2, FD2321/TR2 Guidance Document.

FIGURES





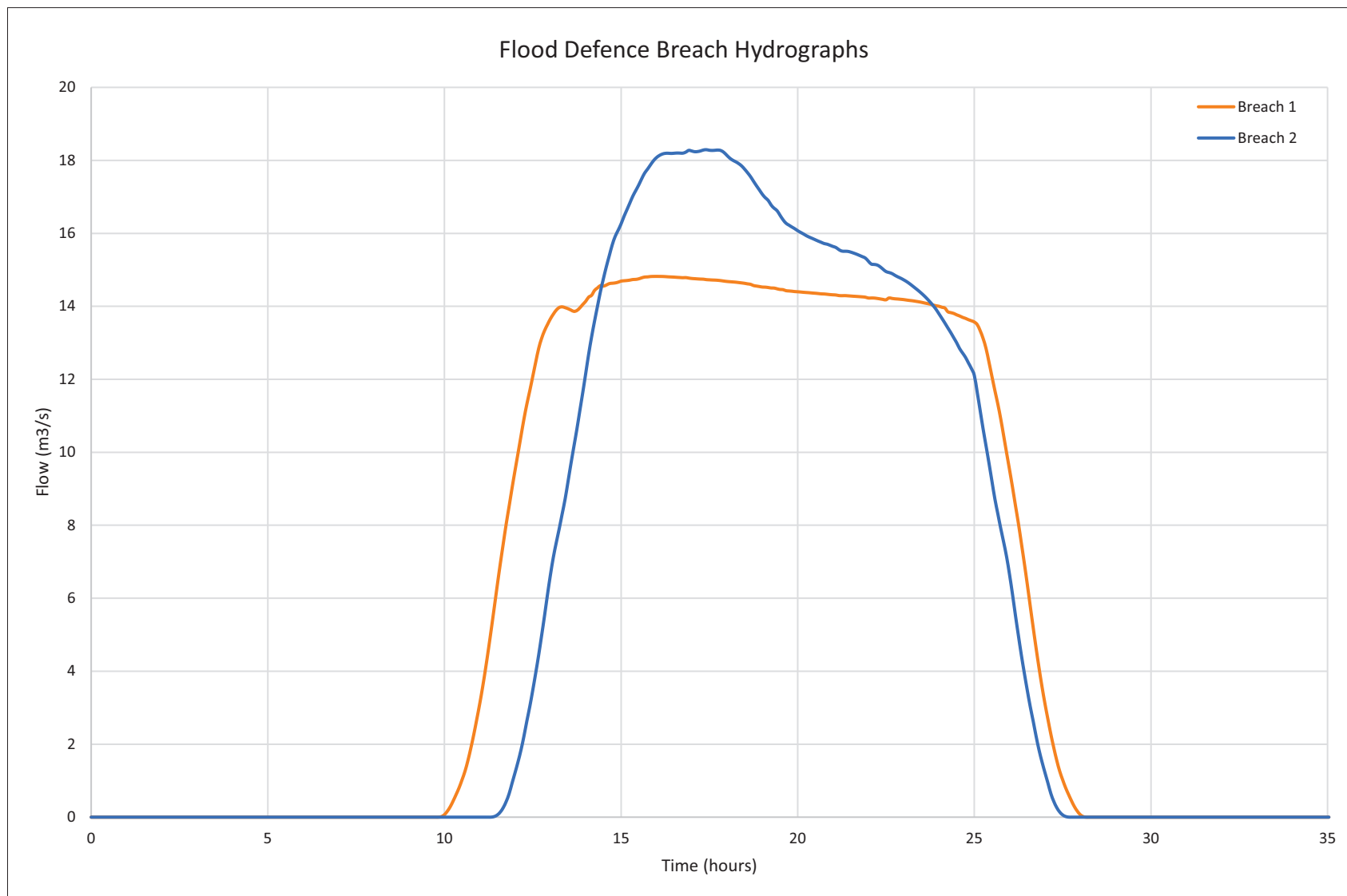
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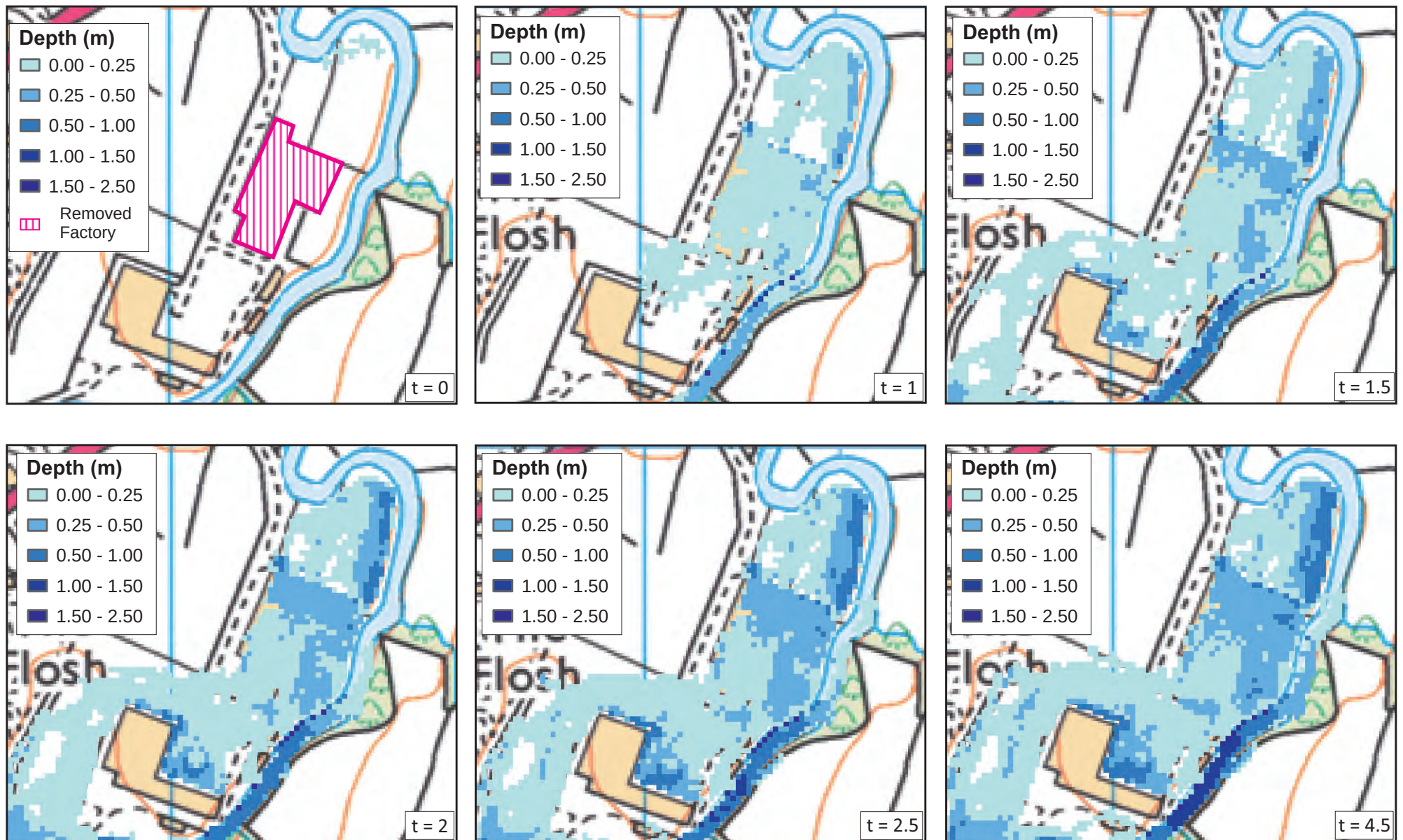


Breach 1 Location

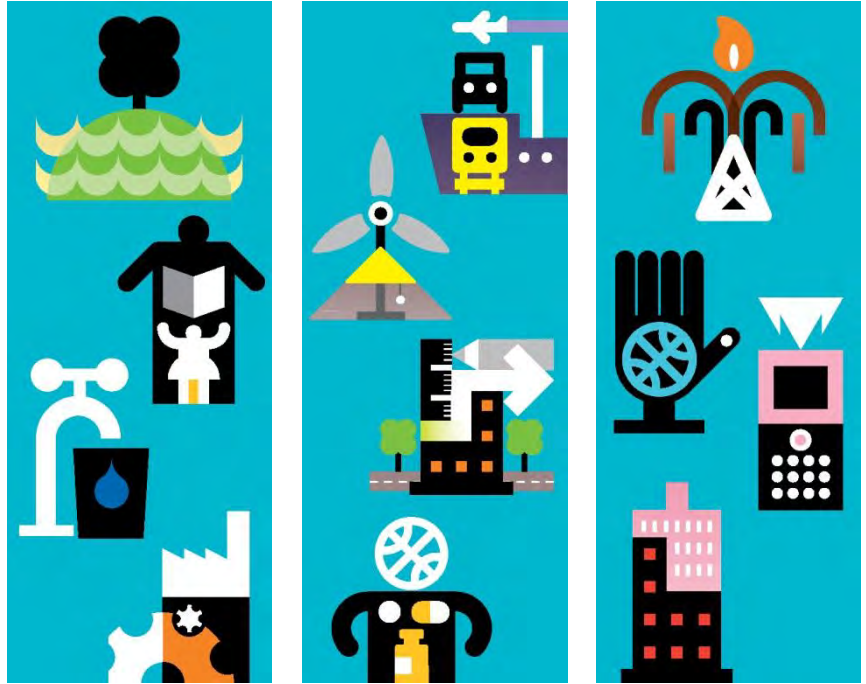


Breach 2 Location





**APPENDIX A
PREVIOUS MODEL REPORT**



Updated Flood Risk Modelling - Cleator Mills Site

Modelling Report

October 2013

RWO Associates



Updated Flood Risk Modelling - Cleator Mills Site

Modelling Report

October 2013

RWO Associates

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Issue and revision record

Revision	Date	Originator	Checker	Approver	Description	Standard
A	23/10/2013	Istvan Galambos	Richard Gamble	Richard Gamble	First Issue	

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Contents

1	Introduction	1
1.1	Background and Objectives	1
1.2	Study Area and Model Extent	1
1.3	Scope of Work	1
2	Breach Analysis	2
2.1	Breach Constraints and Inputs	2
2.2	Breach Methodology	2
3	2D Hydrodynamic Modelling	4
3.1	Introduction	4
3.2	Model Build	4
3.2.1	Digital Terrain Model	4
3.2.2	Boundary Conditions	5
3.2.3	Manning's n	5
3.3	Flood Hazard Classification	6
3.4	Scenarios Modelled	7
4	Results	8
4.1	Breach 1	8
4.2	Breach 2	8
5	Flood Mapping	10
6	Assumptions and Limitations	11
7	Conclusions	12
	Appendices	14
	Appendix A. Study Area	15
	Appendix B. Flood Maps	16

1 Introduction

1.1 Background and Objectives

Mott MacDonald has been commissioned by RWO Associates to undertake a flood defence breach analysis in the River Ehen catchment, near the Cleator Mills site at Cleator in Cumbria. This work follows on from the previous breach analysis work, which Mott MacDonald carried out for a proposed redevelopment of land on the Cleator Mills site in 2010.

The main objectives of the new study are:

- Set up and run a two-dimensional TUFLOW model with new ground survey now available;
- To map the spatial variation of depth, velocity and hazard rating across the floodplain resulting from failure of defences in two alternative locations for a fluvial flood with a return period of 100 year plus climate change.

This report describes the methodology and results of two-dimensional modelling and mapping of the River Ehen breach scenarios.

1.2 Study Area and Model Extent

The breach analyses cover an area situated to the south-east of Cleator Village, adjacent to the River Ehen. The location is shown on the map included in Appendix A. The River Ehen is located to the north and east of the Cleator Mills site. The site is divided into three sections, including the existing Kangol premises, a disused Kangol factory and a car park area.

1.3 Scope of Work

The scope of work for this study is summarised below:

- Use of the existing 2D model of the Cleator Mills site which was developed by Mott MacDonald in 2010;
- Update the model with new topographic survey information provided by RWO Associates;
- Use breach hydrographs as developed for the 2010 modelling and apply these at the same locations as for the 2010 modelling;
- Prediction of the flooding extent, flood depth, velocities and hazard ratings for the 1 in 100 year plus climate change fluvial event;
- Reporting.

2 Breach Analysis

The initial locations of defence breaches to be assessed were agreed with the Environment Agency in March 2010. Output from the existing ISIS model, developed by JBA in 2004, was used by Mott MacDonald in the 2010 study to generate breach scenario hydrographs. Hydrology and boundary inputs that form the basis of this assessment are based on the 2010 study.

2.1 Breach Constraints and Inputs

The following breach locations were used in the 2010 study:

Table 2.1: Breach Locations and Details

Breach	Location	Defence Type	Breach Width (m)	Point X	Point Y	Elevation (mAOD)	Bank
Breach 1	North of the site	Combination of gabion lined baskets and earth embankment	40	302196	513947	64.52	Right bank
Breach 2	East of the site	Earth embankment	40	302202	513840	62.49	Right bank

The following additional requirements were also agreed with the Environment Agency at the time:

- One design event to be considered: 1 in 100 year plus climate change return period;
- All of the breach locations are on a fluvial river, and therefore the following breach width and time to closure details were to be used:

Earth bank: 40m width; 36 hours to closure.

Combination of hard defence and earth bank: 40m width; 36 hours to closure.

- The start of the breach is the bank-full condition or at the peak water level if lower.

2.2 Breach Methodology

The following gives details of the method used in 2010 to model the breach hydrographs in the 1D ISIS model.

- The existing hydraulic model covers the entire reach of River Ehen, including the breaches identified in Table 2.1. The objective of the assessment was to determine a flow hydrograph through each of the breach locations. These hydrographs identified the flows leaving the main channel at these points and was then used as an input to a 2D model of the surrounding area to establish a flood extent and rate of inundation from the breach event.
- In the existing ISIS model of River Ehen, floodplains were represented by ISIS RESERVOIR units which model the rate of water accumulation in a storage pond/lake and made the assumption of a water level surface in the storage. Exchange of flow between river channel and flood cells was characterised by SPILL units representing side weir flow over the river banks.

- The breach locations were identified on the model network. Where necessary an interpolated channel cross-section was added 40m downstream to ensure the breach width of 40m was maintained. The interpolated channel cross-sections were also connected to the RESERVOIR units to ensure any excess water was spilled from the main channel onto the flood cells. This prevented any downstream water level increase, any backwater effect through the breach and also stabilised free flow conditions.
- The breaches were assumed to be formed over a single one second time step in the model runs. The breaches were assumed to form to the full extent of 40m width, thereby providing a 'worst-case' assessment for the development of the breach. The breach was taken as occurring through the full height of the embankment to the level of the surrounding land. This was represented by lowering the elevation of the right bank spill from embankment level to the elevation of the surrounding floodplain. This lower level was obtained from the LiDAR data available for the catchment (See Table 2.2).

Table 2.2: Embankment and Floodplain Levels

Breach Nr.	Embankment Elevation (mAOD)	Floodplain Elevation (mAOD)
Breach 1	64.52	62.5
Breach 2	62.49	61.0

3 2D Hydrodynamic Modelling

3.1 Introduction

The main purpose of this study was to assess the flood extent in the event of flood defence breach for the 100 year plus climate change fluvial event.

The approach to hydraulic modelling has comprised the following stages:

Step 1: constructing a two-dimensional hydraulic model incorporating the new topographic data made available by RWO Associates;

Step 2: breach analysis using the breach hydrographs generated in 2010 study;

Step 3: predicting flood extent for the specified fluvial return period (1 in 100 year plus climate change);

Step 4: producing flood extent, depth, velocity and hazard maps.

3.2 Model Build

The proposed development site is located to the south-east of the village of Cleator adjacent to the River Ehen. The extent of the model was estimated so that the model would include a sufficient length of the River Ehen within the model, whilst also including the Cleator Mills site that has a theoretical chance of flooding. Two breach locations are identified in the study area, as described in Table 2.1.

3.2.1 Digital Terrain Model

The Digital Terrain Model (DTM) for the Cleator Mills area was produced using 1m resolution LiDAR and ground based topographic survey data. In order to ensure that channel volume was not available to flood waters (since during a breach scenario channels are assumed to be full to bank-top) the DTM along channel lengths was raised to bank-top levels.

The topographic survey (North Associates - Kangol Factory, Cleator_topo.dwg) was provided by RWO Associates. The survey data was recorded in local coordinate system, therefore the first step was to transform it to the national coordinate system. After the transformation the 2d_zsh feature of TUFLOW was used to incorporate the survey into the DTM.

The TUFLOW model comprises of a grid of the Cleator Mills area, with grid points (z points) assigned elevations from the above mentioned sources. Details of the grid used for modelling the River Ehen at Cleator Mills are summarised in Table 3.1 below.

Table 3.1: Cleator Mills TUFLOW Model Grid Details

Grid Information	
Grid size (spacing)	7m
Origin	301,135N, 512,883E (British National Grid)
Orientation	0 degrees
Width of grid (in the east direction)	2.16km
Height of grid (in the north direction)	2.15km

A grid size of 7m was used as this is of sufficient detail for flood mapping, whilst not being so small as to result in unacceptably long model run times.

3.2.2 Boundary Conditions

The upstream boundary of the model is a flow-time boundary condition. Breach hydrographs were extracted at SPILL units connected to the model river cross-sections at each breach location for the 100 year plus climate change fluvial event. The breach hydrographs were developed in the 2010 modelling study and have been used in this updated study without modification. The breach hydrographs are shown on Figure 3.1

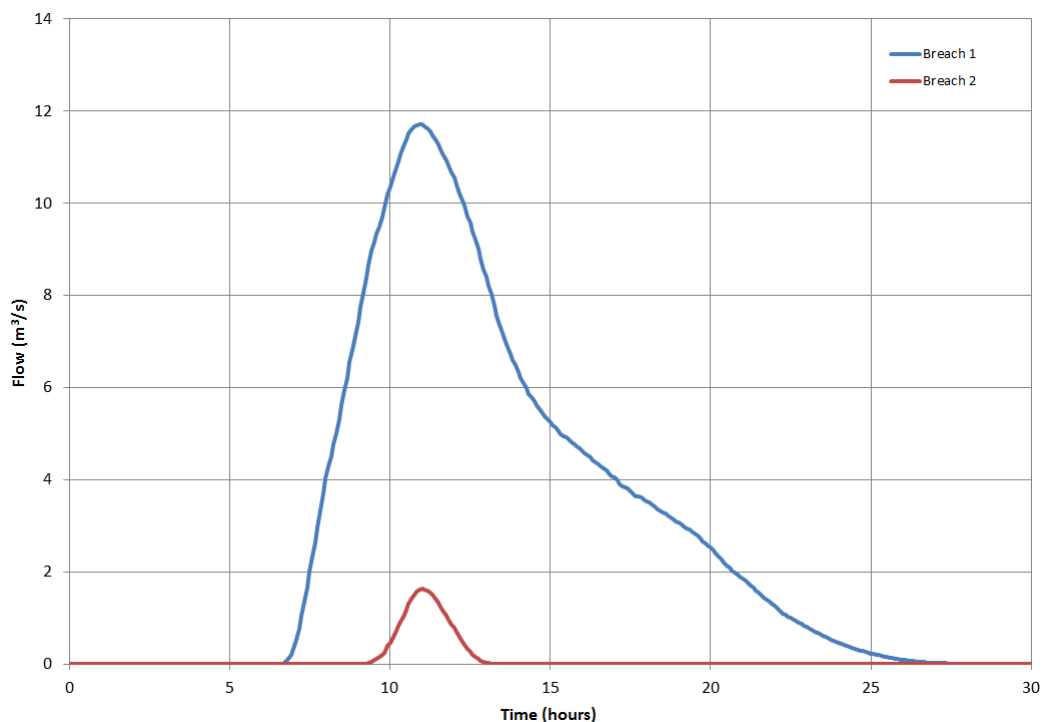


Figure 3.1 – Breach hydrographs

3.2.3 Manning's n

Land classification within the TUFLOW model determines the roughness values (Manning's n) of each land type, and therefore the resistance that is provided by the land to the flood water. For this study, a detailed land classification was used, as outlined in Table 3.2.

Table 3.2: Summary of Manning's n Values Used in the Model

Terrain Type	Roughness
Water	0.035
Grassed floodplain	0.055
Buildings	0.300
Woodland	0.120
Roads and railways	0.020

3.3 Flood Hazard Classification

Hazard rating has been defined in the *Supplementary Note on Flood Hazard ratings and Thresholds for Development Planning and Control Purpose – Classification of the Table 13.1 of FD2320/TR2 and Figure 3.2 of FD2321/TR1* (Defra 2008). Hazard rating is calculated from depth, velocity and a debris factor at each time step in the model using the following equation:

$$HR = d (v + 0.5) + DF$$

where, HR = (flood) hazard rating;

d = depth of flooding (m);

v = velocity of floodwaters (m/s); and

DF = debris factor (0, 0.5, 1 depending on probability that debris will lead to a hazard).

The debris factor was based on the conservative land use classification. It varies with depth and velocity of flooding as shown in Table 3.3.

Table 3.3: Guidance on debris factors for different flood depths, velocities and dominant land use (from Table 4.2 in Flood Risks to People)

Depth (d)/Velocity (v)	Debris Factor based on Conservative Land Use
d = 0 to 0.25m	0.5
d = 0.25 to 0.75m	1.0
d > 0.75 and/or v > 2m/s	1.0

Hazard rating has been classified into four categories in the *Supplementary Note on Flood Hazard ratings and Thresholds for Development Planning and Control Purpose – Clarification of the Table 13.1 of FD2320/TR2 and Figure 3.2 of FD2321/TR1* (Defra, 2008) for emergency planning purposes.

Table 3.4 summarises the four categories. This classification has been used in the description of the results.

Table 3.4: Hazard to People as a Function of Velocity and Depth

Hazard Rating	Degree of Flood Hazard	Elevation (m AOD) Bank
<0.75	Low	Caution "Flood zone with shallow flowing water or deep standing water"
0.75 – 1.25	Moderate	Dangerous for some (e.g. children) "Danger: Flood zone with deep or fast flowing water"
1.25 – 2.0	Significant	Dangerous for most people "Danger: flood zone with deep fast flowing water"
>2.0	Extreme	Dangerous for all "Extreme danger: flood zone with deep fast flowing water"

3.4 Scenarios Modelled

Two scenarios using the above methodology have been modelled for the 1 in 100 year plus climate change event. These scenarios are listed in Table 3.5 below:

Table 3.5: Scenarios Modelled

Breach Nr.	Design Event
Breach 1	100 year plus climate change
Breach 2	100 year plus climate change

Appendix A shows the location of breaches.

4 Results

4.1 Breach 1

A breach in the gabion lined baskets north of the site has been considered for the 1 in 100 year plus climate change event. The approximate location of the breached defence is indicated on the Appendix A. A breach of the flood defence was assumed to occur when the river was at bank-full downstream. During a breach for the 100 year plus climate change event, floodwaters flow onto the floodplain (see Figure 4.1), flooding the existing premises, car park area and the disused factory building downstream of the site. Some of the floodwaters flow back into the River Ehen near the downstream end of the existing Kangol premises. Flood depths in the vicinity of the breach are fairly significant reaching up to 0.90 m near this building.

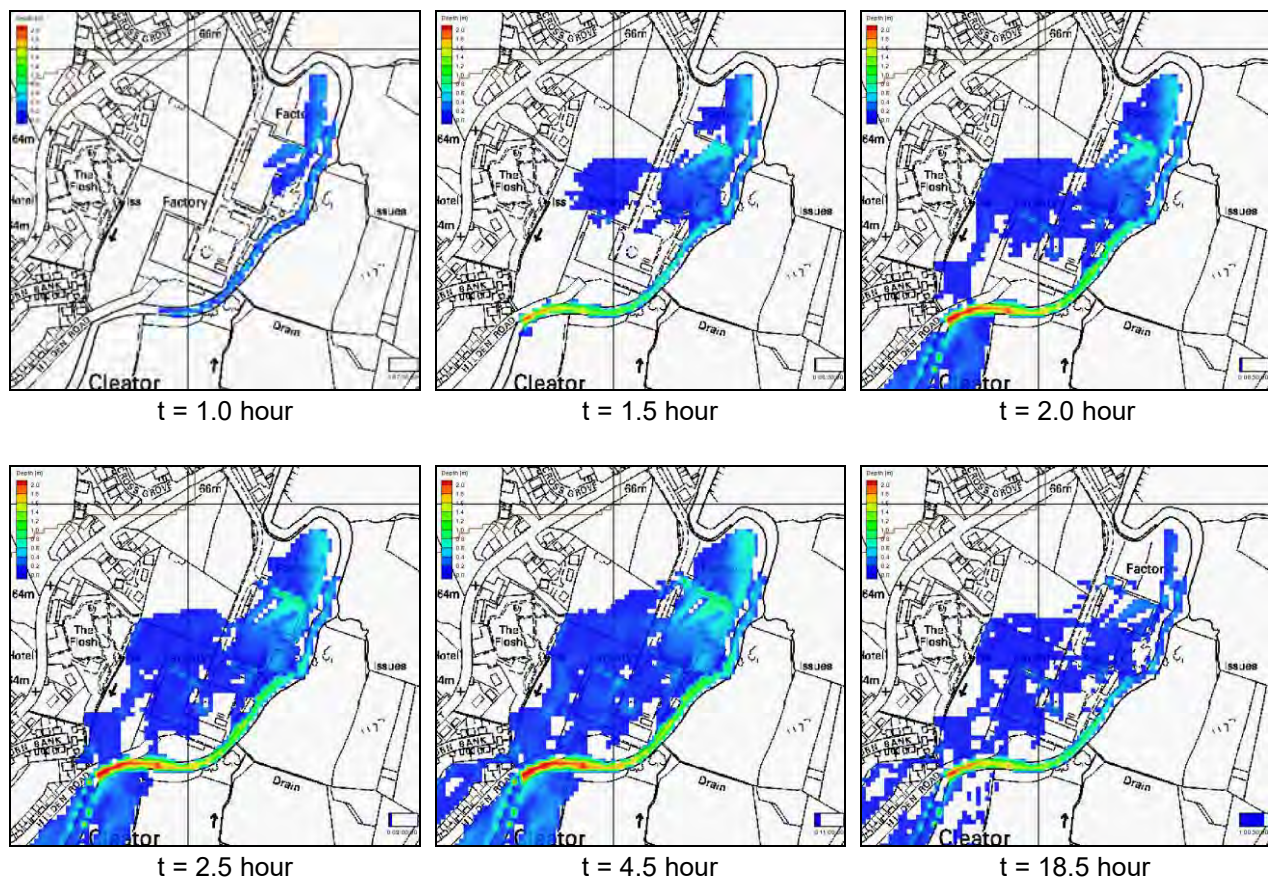


Figure 4.1 – Progress of flood wave from Breach 1

The hazard rating was generally low (0 to 0.75) throughout the site, although this was observed to be greater in the areas of deeper waters. There are areas, in the vicinity of the Kangol Building where the hazard rating is significant (1.25 to 2) implying that it is dangerous for most people.

4.2 Breach 2

A breach in the earth flood embankment east of the site was considered for the 100 year plus climate change event. The approximate location of the breached flood embankment is shown on Appendix A. For this analysis it has been assumed that the River Ehen was bank-full downstream of the breached

embankment. During a breach, floodwaters spread onto the floodplain (see Figure 4.2), inundating the Kangol premises, and then flow through parts of the car park area and the disused factory building. Flood depths generally remain low (0 to 0.25m) through the site, although there are small areas in the vicinity of the Kangol building where there is deeper flooding of up to 0.5m. The flood hazard rating of the breach floodwaters is low (0 to 0.75) as the depth of flooding is shallow (less than 0.25m) and the velocities are low (less than 0.3m/s) with the exception of a few areas in the vicinity of the existing building (0.8m/s).

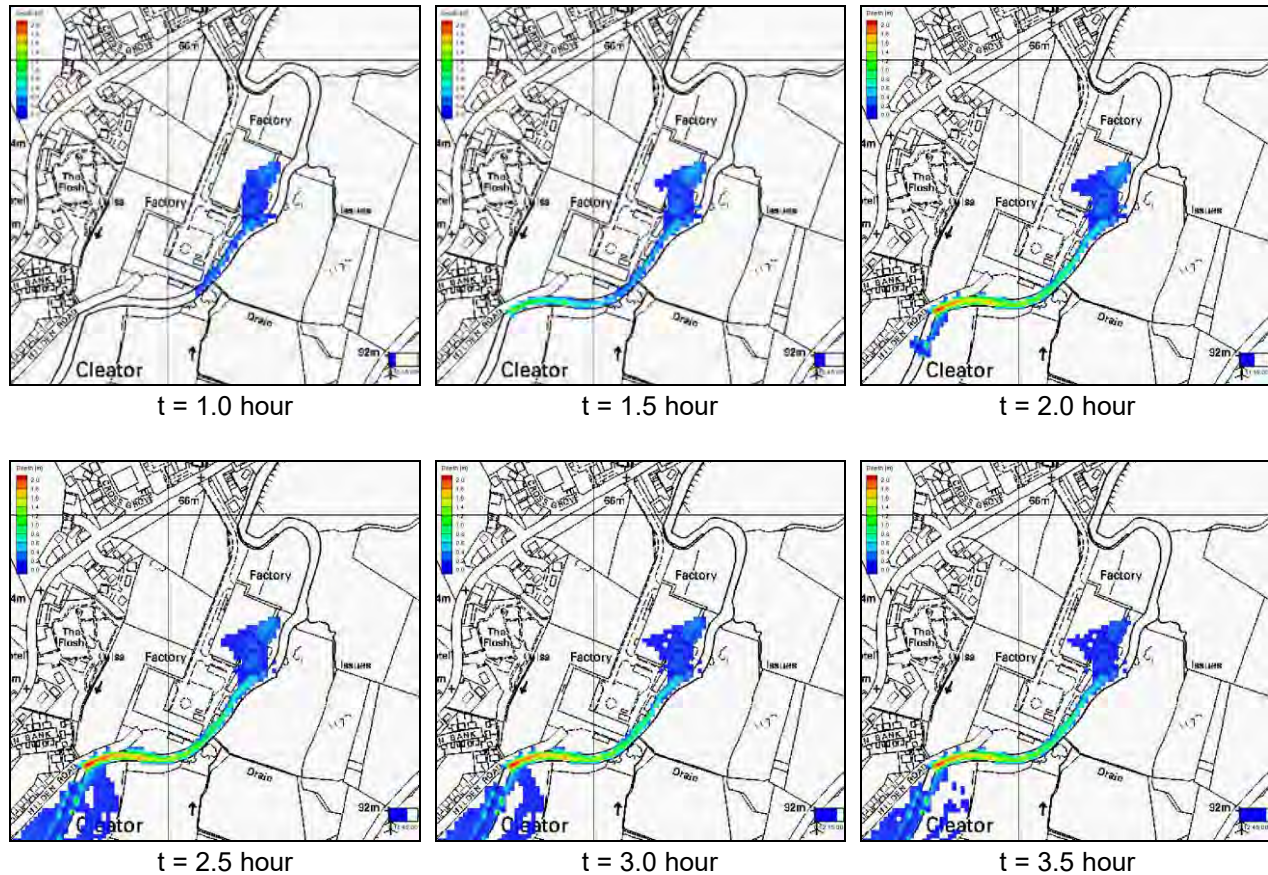


Figure 4.2 – Progress of flood wave from Breach 2

5 Flood Mapping

Flood maps have been produced from the outputs of the 2D modelling. The maps show maximum water level, flood depth, velocities and hazard rating for all of the scenarios which have been modelled. Table 5.1 summarises the flood maps located in Appendix B and discussed in Section 4.

Table 5.1: Summary of Flood Maps

Drawing No.	Parameter Shown	Breach Location	Return Period
1.01	Depth	Breach 1	100 year + 20%
2.01	Velocity	Breach 1	100 year + 20%
3.01	Water Level	Breach 1	100 year + 20%
4.01	Hazard Rating	Breach 1	100 year + 20%
1.03	Depth	Breach 2	100 year + 20%
2.03	Velocity	Breach 2	100 year + 20%
3.03	Water Level	Breach 2	100 year + 20%
4.03	Hazard Rating	Breach 2	100 year + 20%

6 Assumptions and Limitations

The model and input data are based on the following assumptions:

- River channel is bank-full downstream of breach locations.
- Flood defences and embankment levels used in the existing ISIS model are correctly representing the study area.
- The ISIS model accounts for surface runoff in the study area.

The model has several limitations which should be understood before applying the findings of this report:

- Models are not calibrated or verified, owing to lack of observed historic data.
- LiDAR data has verified accuracy of +/- 150mm.

7 Conclusions

The outputs from the updated Cleator Mills FRA Breach Analysis facilitate the assessment of extent and severity of flooding in the event of breaches in the fluvial defences. The breach hydrographs used were those produced in the previous breach analysis (2010) and are for the 100 year plus climate change event, based on best available data at the time.

Breach hydrographs were input as flow-time boundary conditions into the 2D TUFLOW model. The 2D model covered areas adequate to model the full extent of flood waters, using a grid size of 7m.

It was observed that the extent of flooding south of the breached gabion lined baskets (Breach 1) was significant. Areas affected were mainly near the existing Kangol premises, car park area and the disused factory building downstream of the site. Hazard rating was generally low through the site, with the exception of a few areas in the vicinity of the existing building. Flood waters were observed to be deeper in these areas (up to 0.9 m), and the hazard rating was identified to be significant (1.25 to 2) implying that it is dangerous for most people.

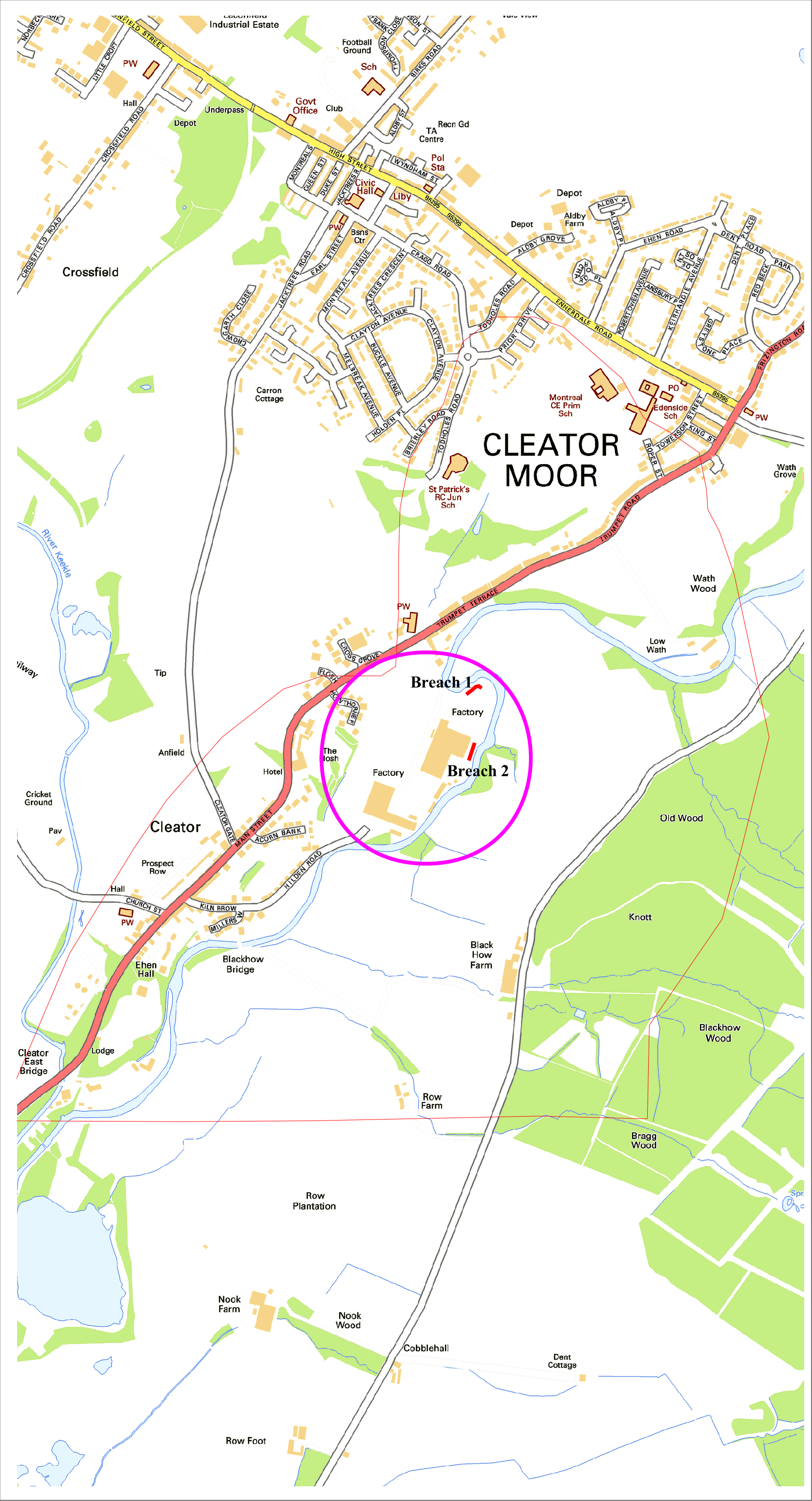
During a breach in the earth embankment east of the site (Breach 2), floodwaters covered the existing building and parts of the car park area. Flood depths generally remained low (0 to 0.25m) through the site, although there were small areas in the vicinity of the factory building where there was deeper flooding of up to 0.5m. The flood hazard rating of the breach floodwaters was low (0 to 0.75) as the depth of flooding was shallow (less than 0.25m) and the velocities were low (less than 0.3m/s) with the exception of a few areas in the vicinity of the existing building (0.8m/s).

The extent and severity of flooding predicted for both breaches is very similar to that predicted in the 2010 study. The additional ground based topographic data now available indicates that the area to north-west of the existing factory are lower than given by LiDAR data used in 2010. This results in greater flood extent in this area. However maximum values of flood depth, velocity and hazard around the site has not significantly changed.

Appendices

Appendix A. Study Area	15
Appendix B. Flood Maps	16

Appendix A. Study Area



KEY PLAN



LEGEND

Extent of 2D Domain

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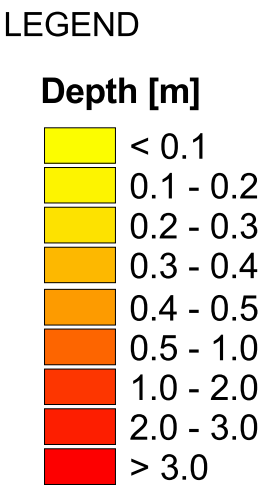
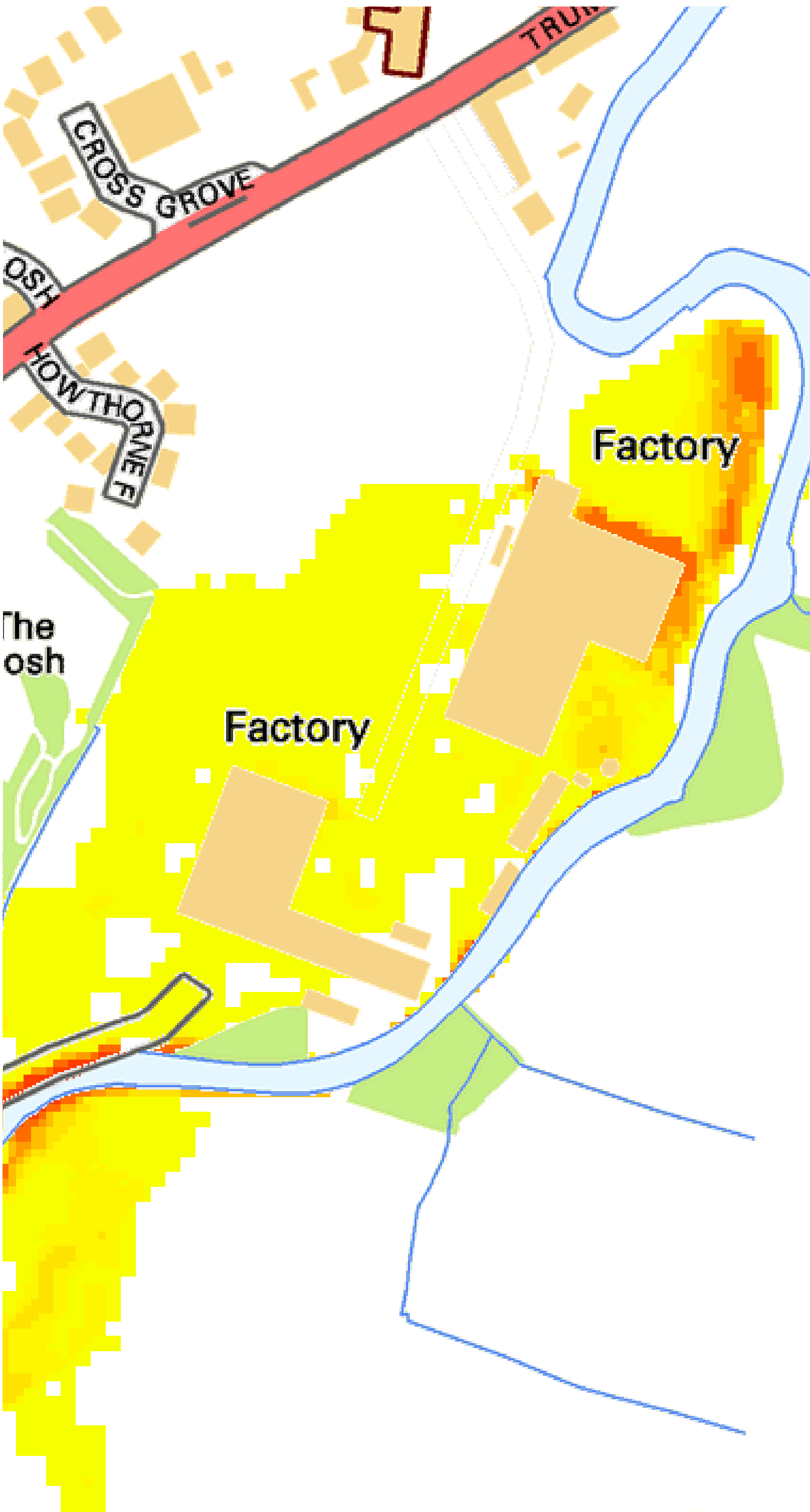
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www.mottmac.com

Project Title
Flood Risk Modelling - Cleator Mill Site

Map Title
2D Model Extent

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	0.01
Drawing Scale at A3	1:5000

Appendix B. Flood Maps



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www.rwoassociatesuk.com

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www.mottmac.com

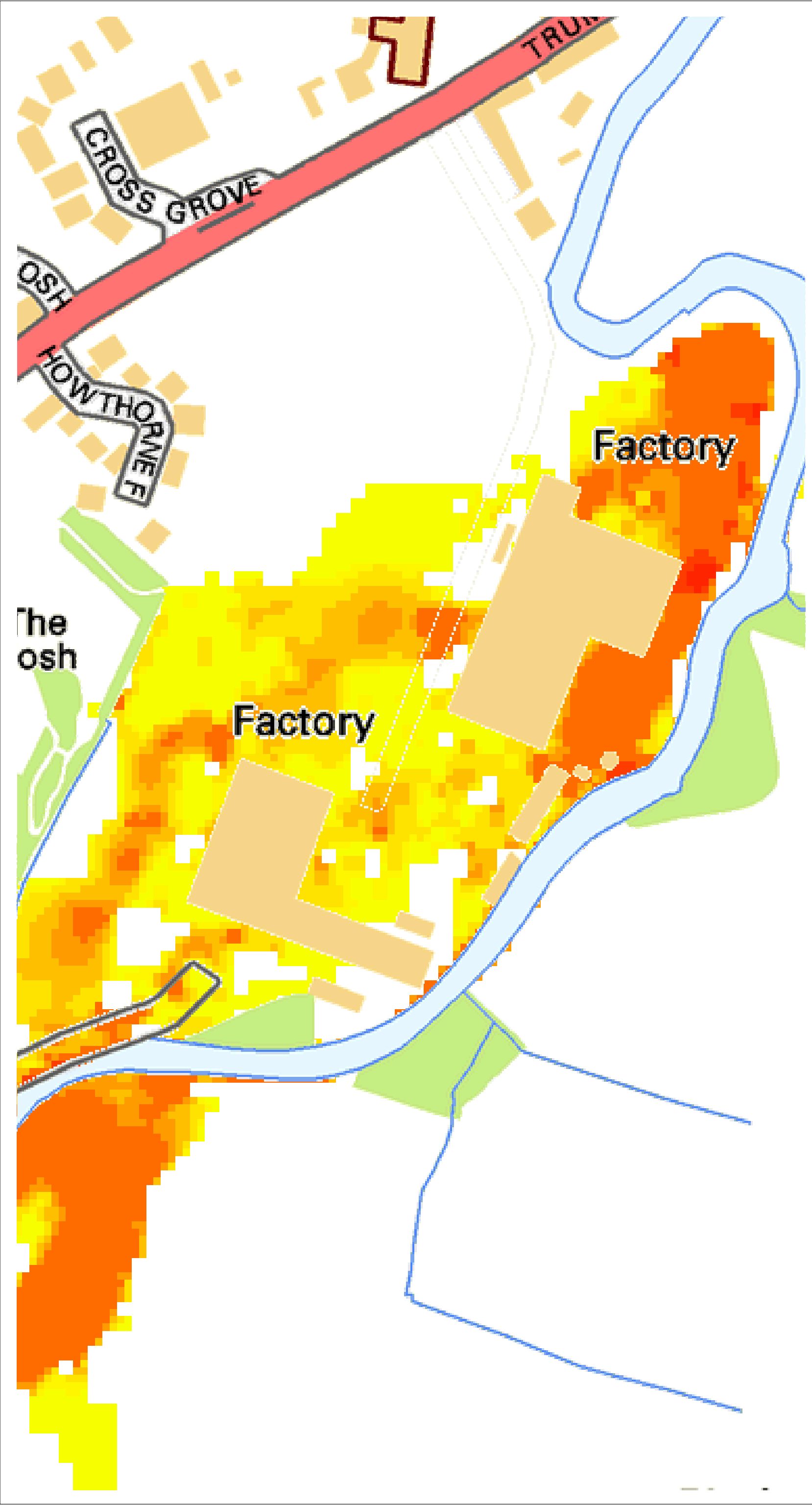
Project Title

Flood Risk Modelling - Cleator Mill Site

Map Title

Maximum flood depth for breach 1 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	1.01
Drawing Scale at A3	1:1100

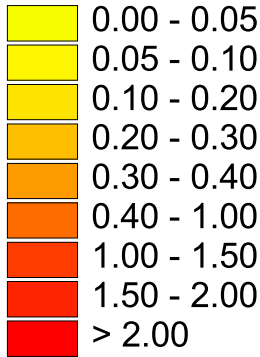


KEY PLAN



LEGEND

Velocity [m/s]



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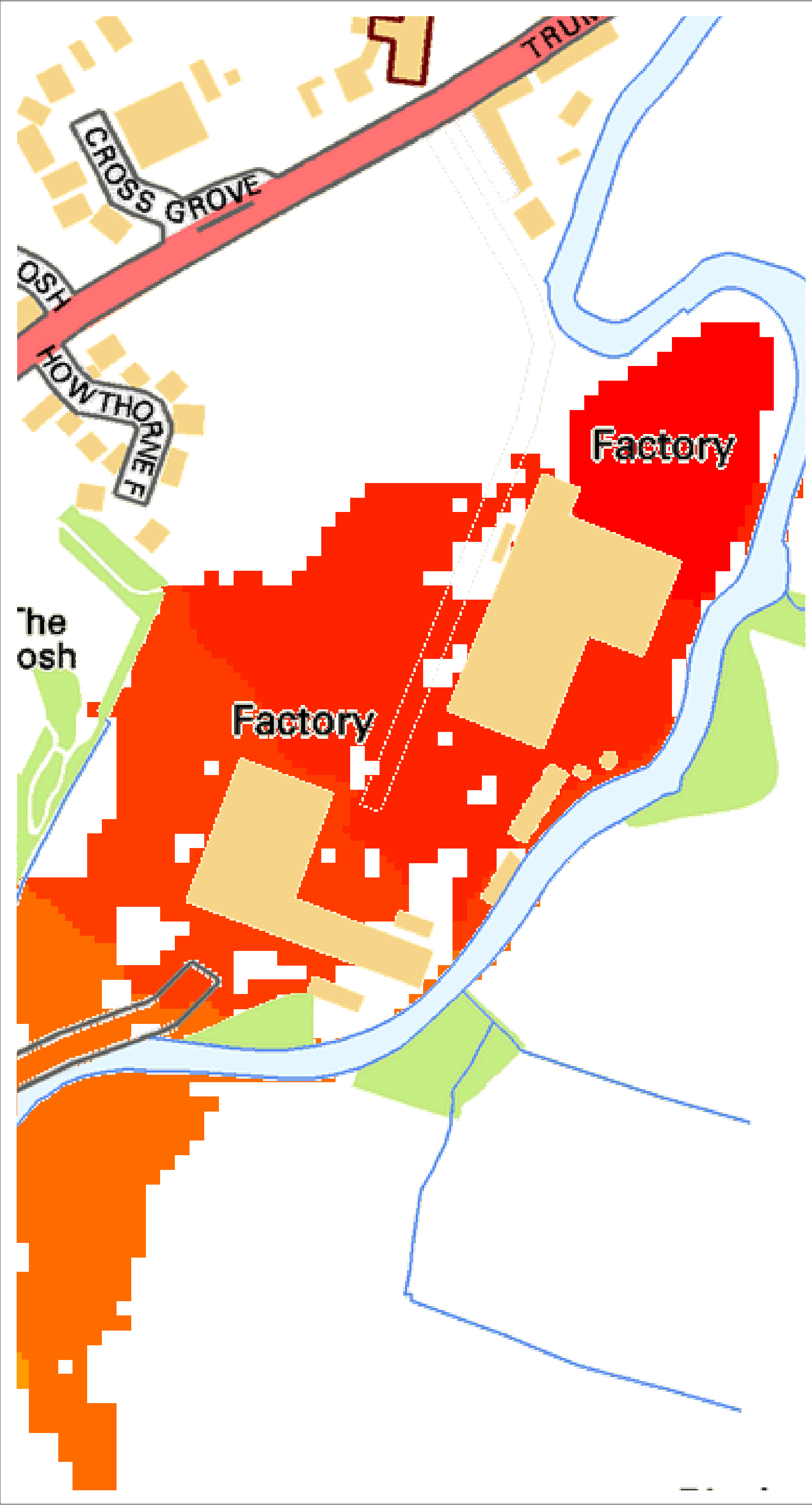


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Project Title
Flood Risk Modelling - Cleator Mill Site

Map Title
Maximum flow velocity for breach 1 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	2.01
Drawing Scale at A3	1:1100

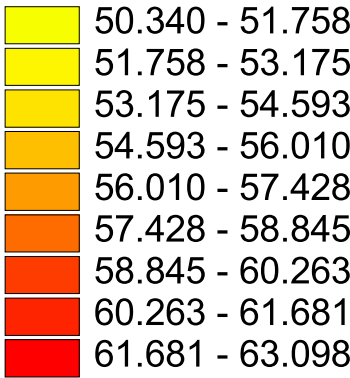


KEY PLAN



LEGEND

Water Level [mAOD]



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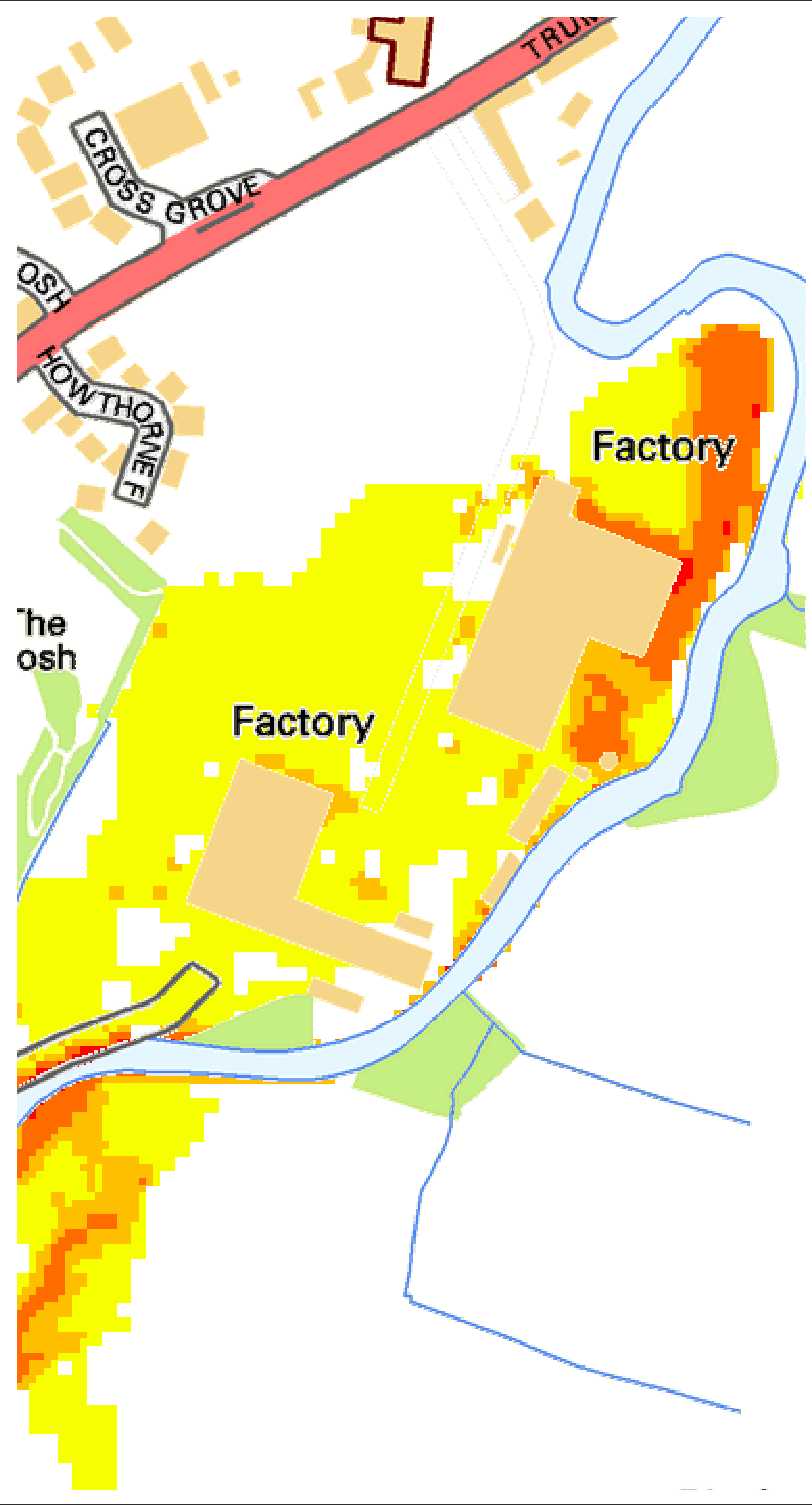


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Project Title
Flood Risk Modelling - Cleator Mill Site

Map Title
Maximum water level for breach 1 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	3.01
Drawing Scale at A3	1:1100



KEY PLAN



LEGEND

- Flood Hazard Category**
- Low
 - Moderate
 - Significant
 - Extreme

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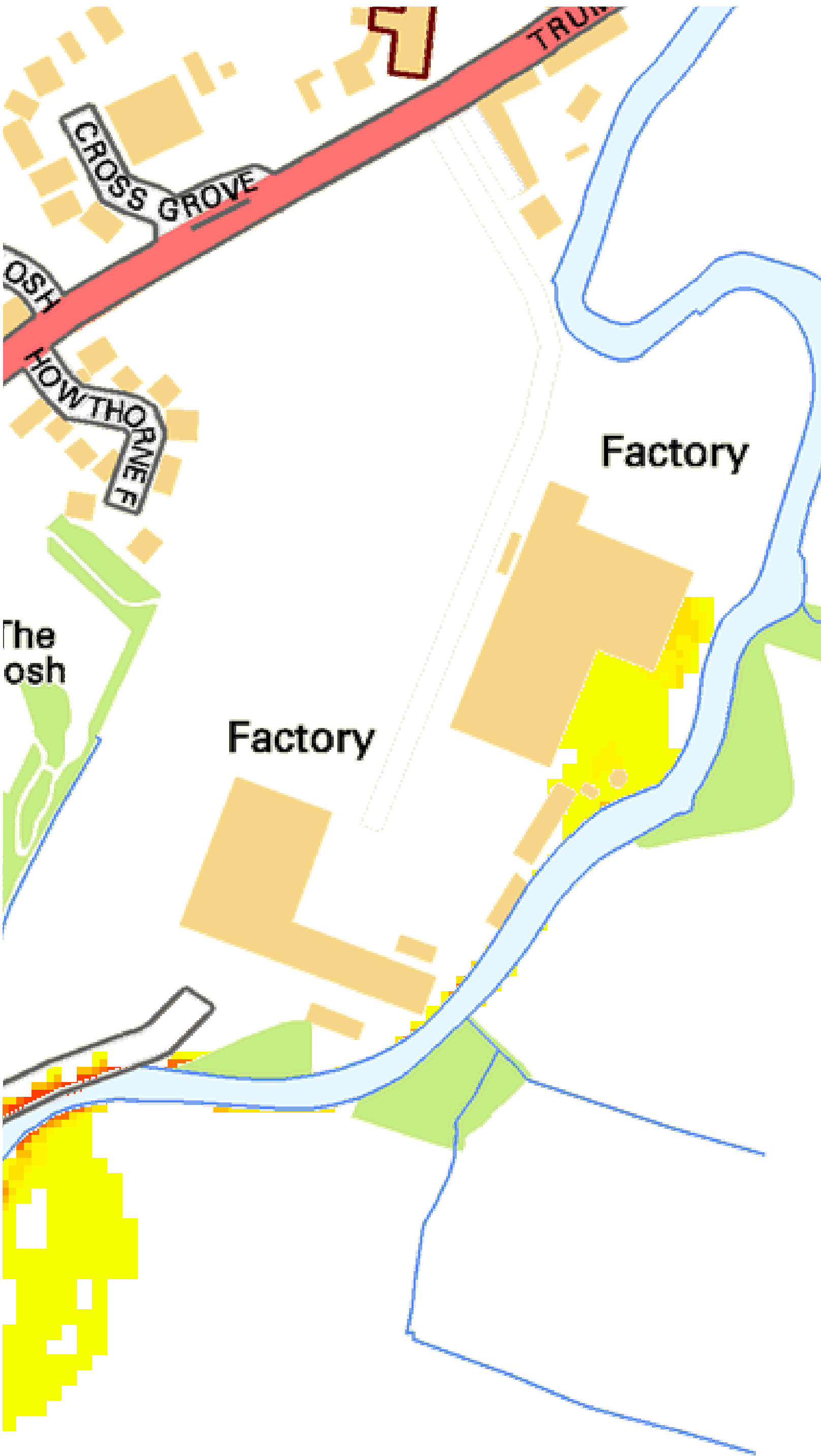


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Project Title
Flood Risk Modelling - Cleator Mill Site

Map Title
Hazard categories for breach 1 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	4.01
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Project Title

Flood Risk Modelling - Cleator Mill Site

Map Title

Maximum flood depth for breach 2 (DTM 2013)

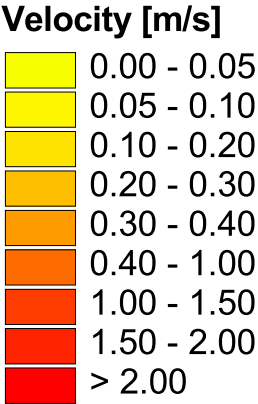
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Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	1.03
Drawing Scale at A3	1:1100



KEY PLAN



LEGEND



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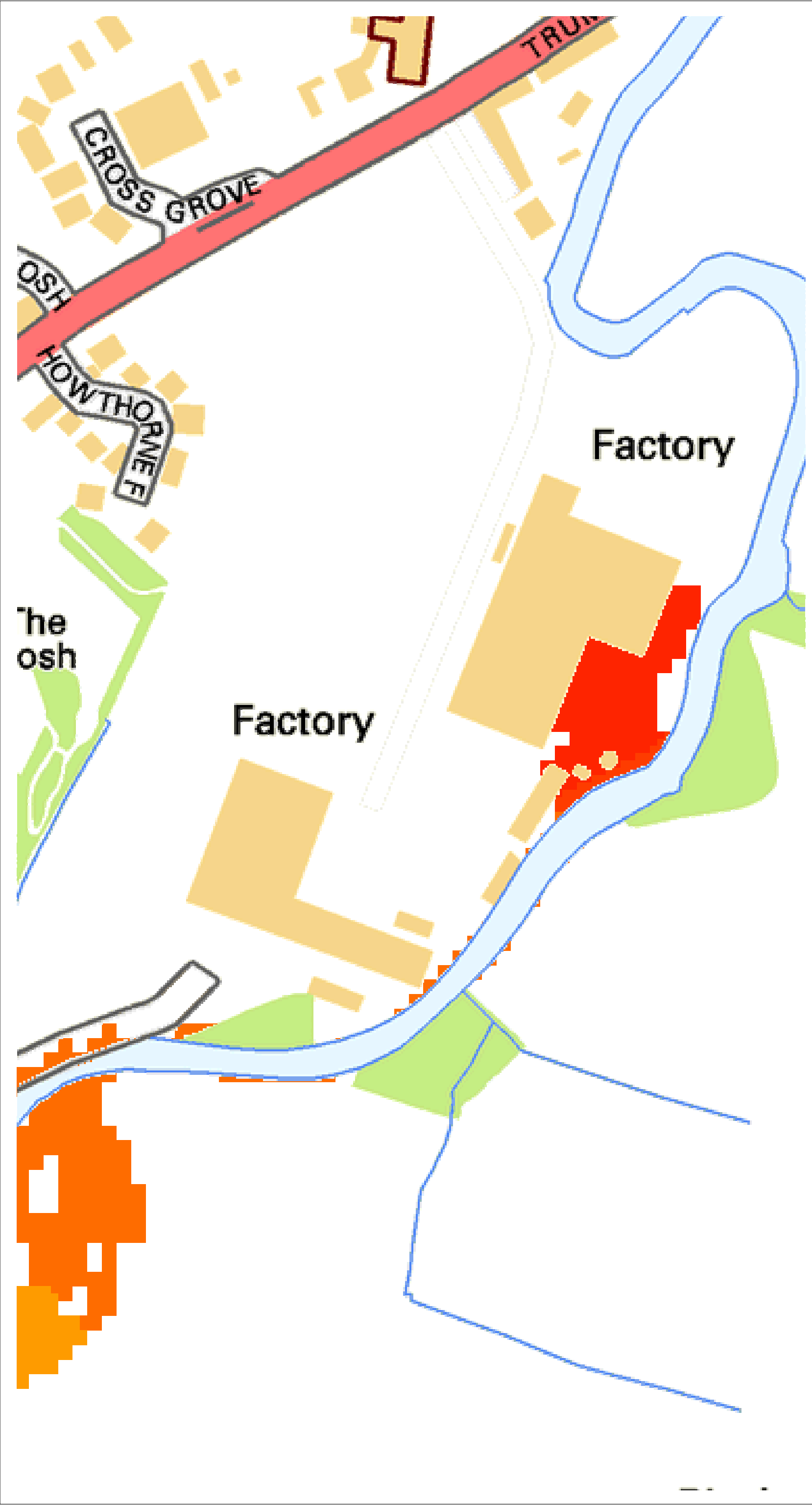
Project Title

Flood Risk Modelling - Cleator Mill Site

Map Title

Maximum flow velocity for breach 2 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	2.03
Drawing Scale at A3	1:1100

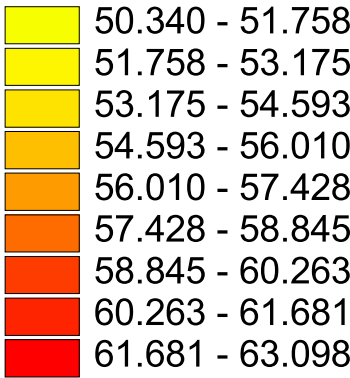


KEY PLAN



LEGEND

Water Level [mAOD]



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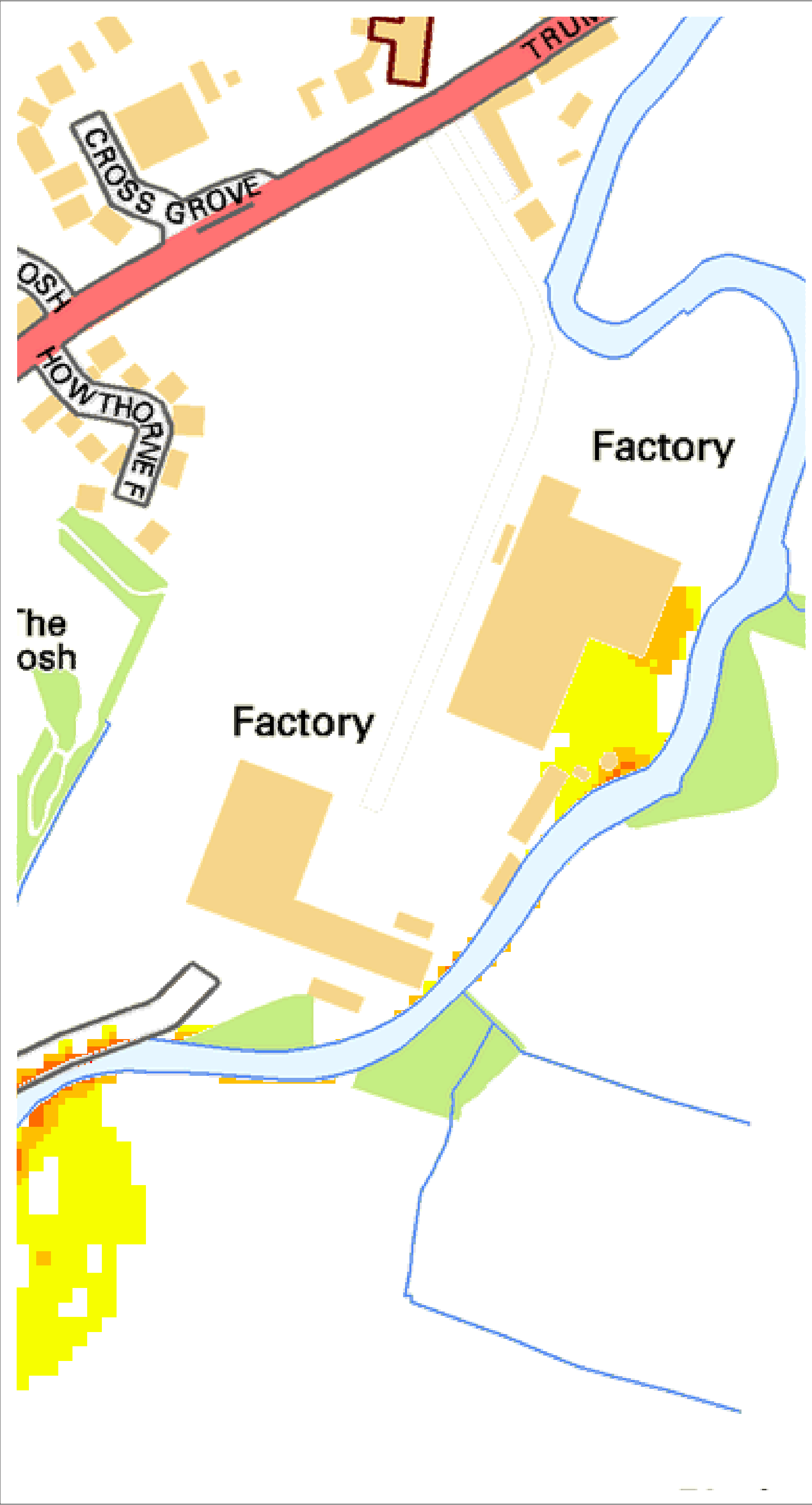


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Project Title
Flood Risk Modelling - Cleator Mill Site

Map Title
Maximum water level for breach 2 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	3.03
Drawing Scale at A3	1:1100



KEY PLAN



LEGEND

- Flood Hazard Category**
- Low
 - Moderate
 - Significant
 - Extreme

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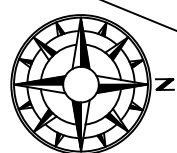
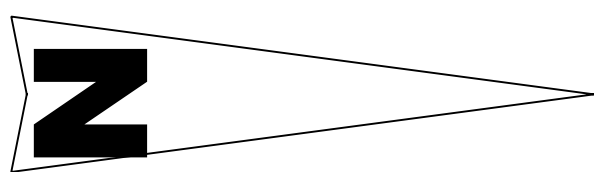
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Project Title
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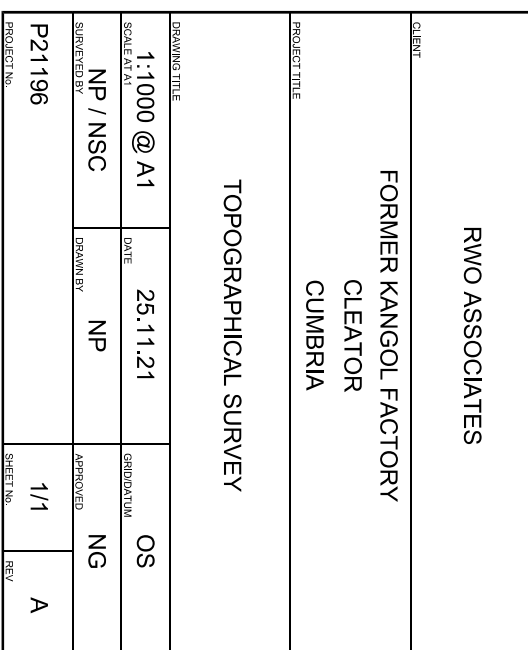
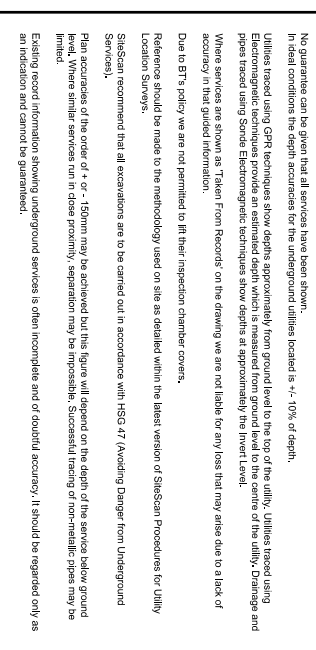
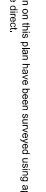
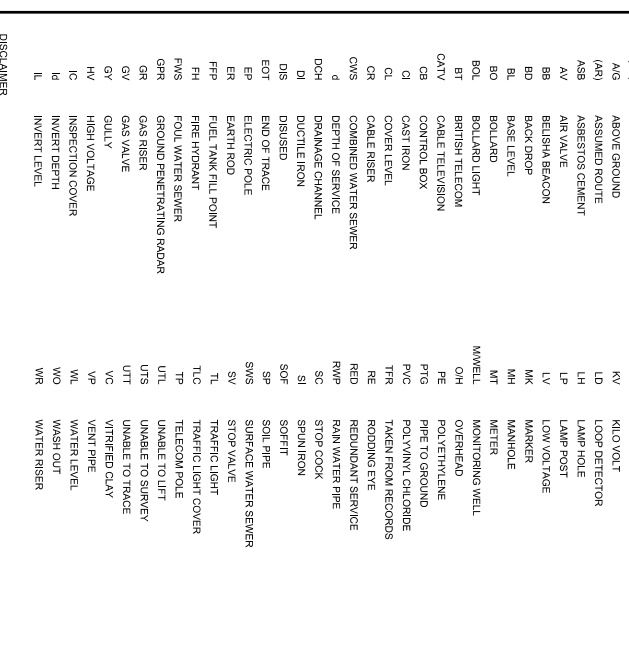
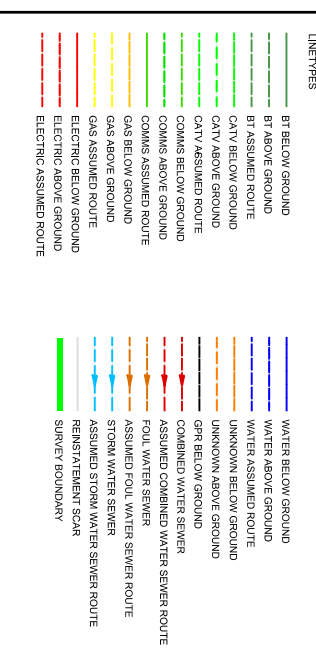
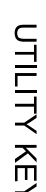
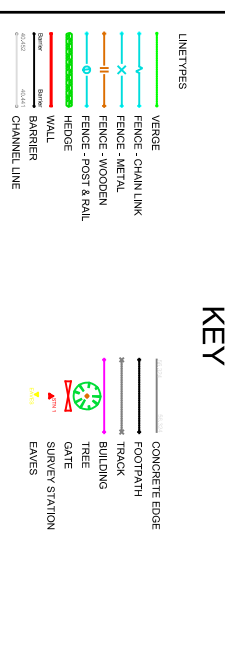
Map Title
Hazard categories for breach 2 (DTM 2013)

Date / Revision	14/10/2013
Modelled	IG
Checked	RJG
Approved	RJG
Drawing No.	4.03
Drawing Scale at A3	1:1100

APPENDIX B
RWO ASSOCIATES TOPOGRAPHICAL SURVEY



- | Key | Monhale | Telemont | Monhale |
|-----|----------------------|----------|---------|
| MH | Monhale | | |
| BT | Brish | | |
| LP | Inspection | | |
| CP | Lens Post | | |
| SV | Stop Post | | |
| TP | Stop Vine | | |
| PH | Gale | | |
| WM | Telegraph Pole | | |
| | Fire Hydrant | | |
| | Water Meter | | |
| | Wall | | |
| | Fence | | |
| | Fence | | |
| | Fence | | |
| | Kerbline | | |
| | Edge of Path/Track | | |
| | Top of Bank | | |
| | Bottom of Bank | | |
| | Gate | | |
| | Face of Hedge/Bushes | | |



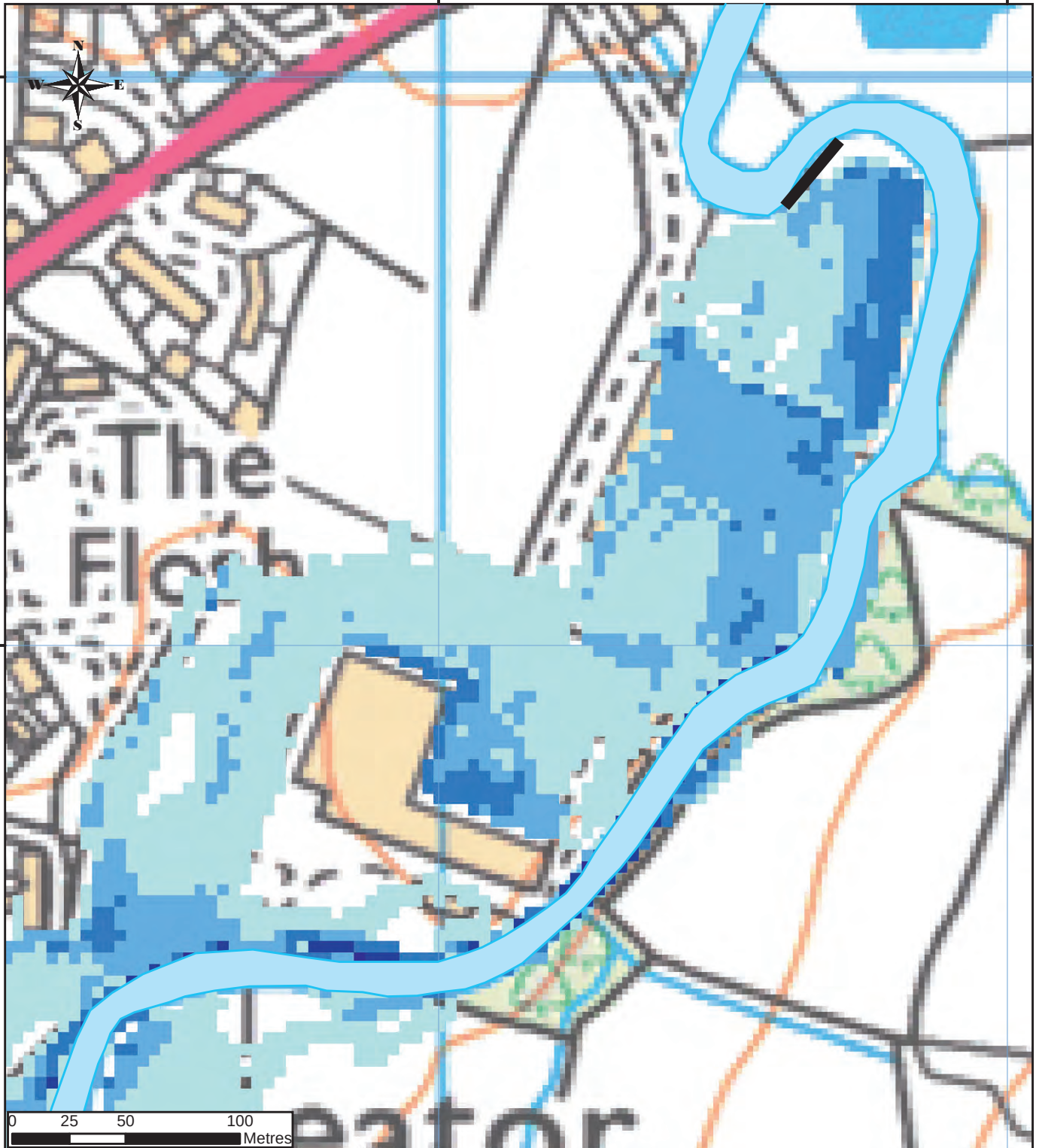
APPENDIX C
BREACH 1 FLOOD MAPS – FIGURES 6A, 6B, 6C AND 6D

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302250

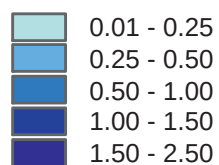
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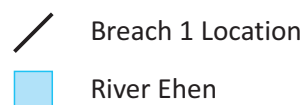


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Flood Depth (m)



KEY

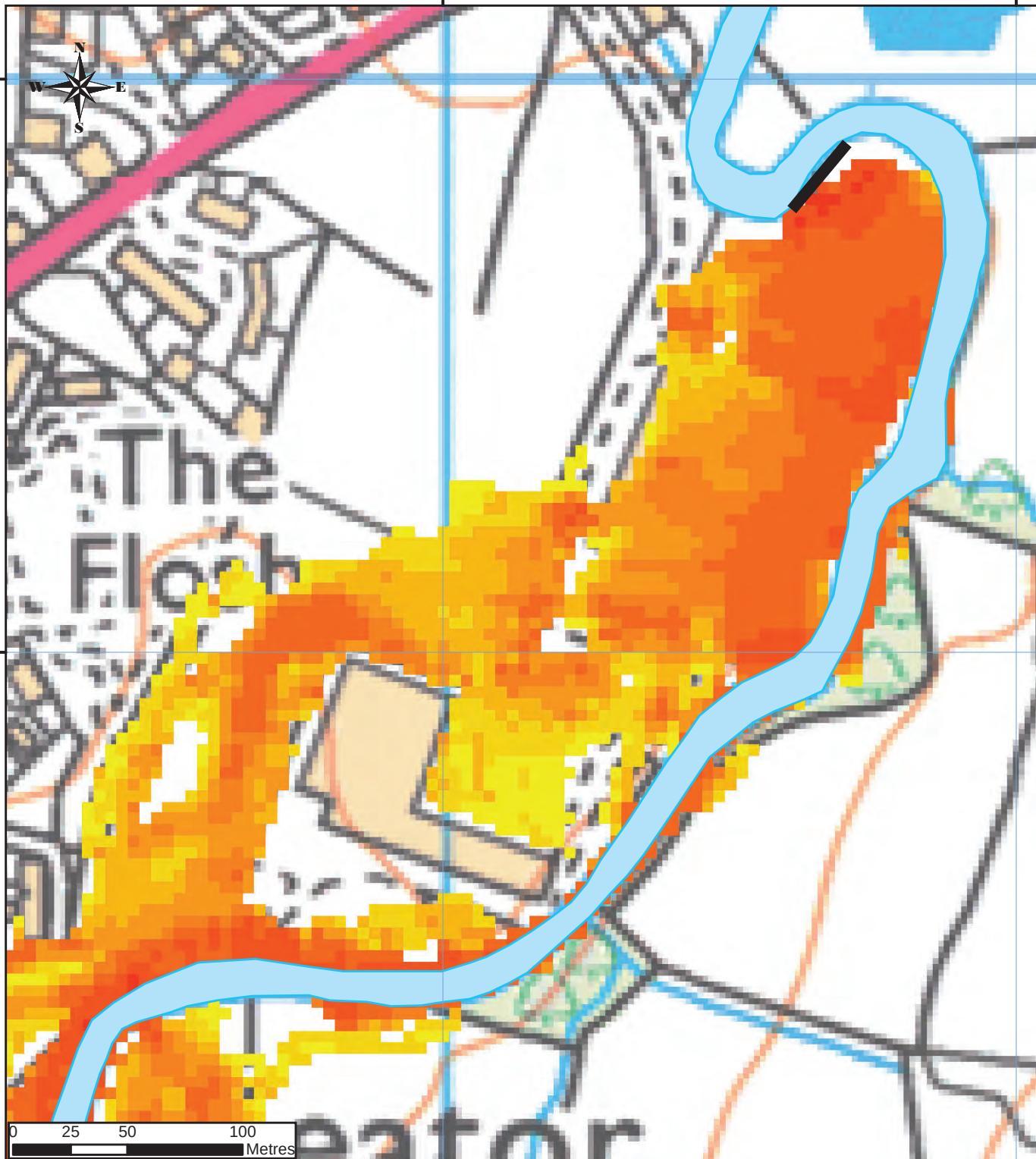


302000

302250

514000

513750



KEY

Velocity (m/s)

	< 0.1		0.5 - 1.0
	0.1 - 0.2		1.0 - 2.0
	0.2 - 0.3		2.0 - 3.0
	0.3 - 0.4		> 3
	0.4 - 0.5		

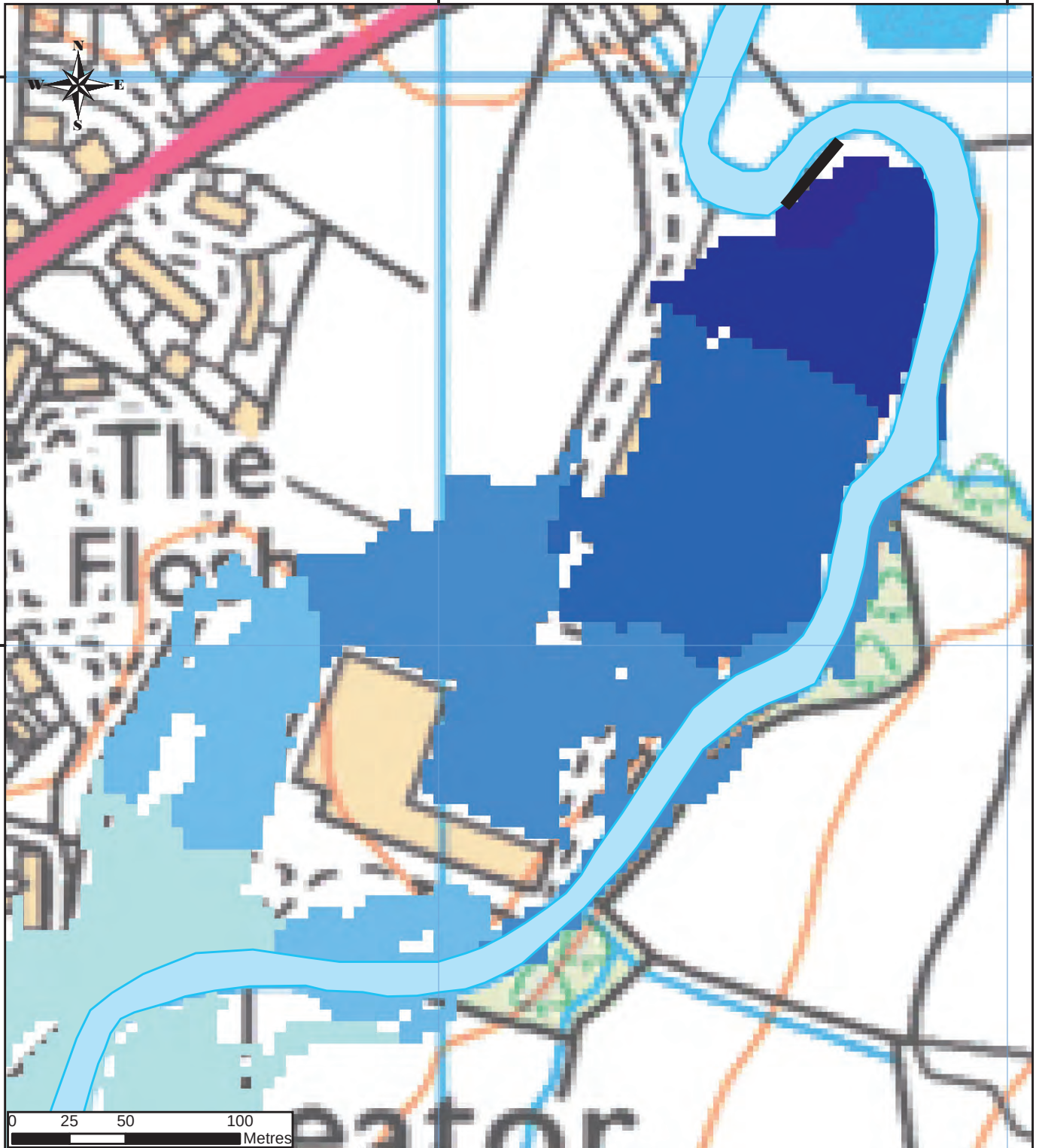
- Breach 1 Location
- River Ehen

302000

302250

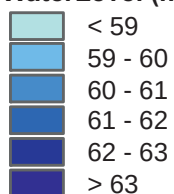
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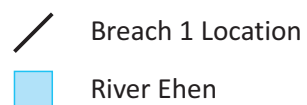


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WaterLevel (mAOD)



KEY

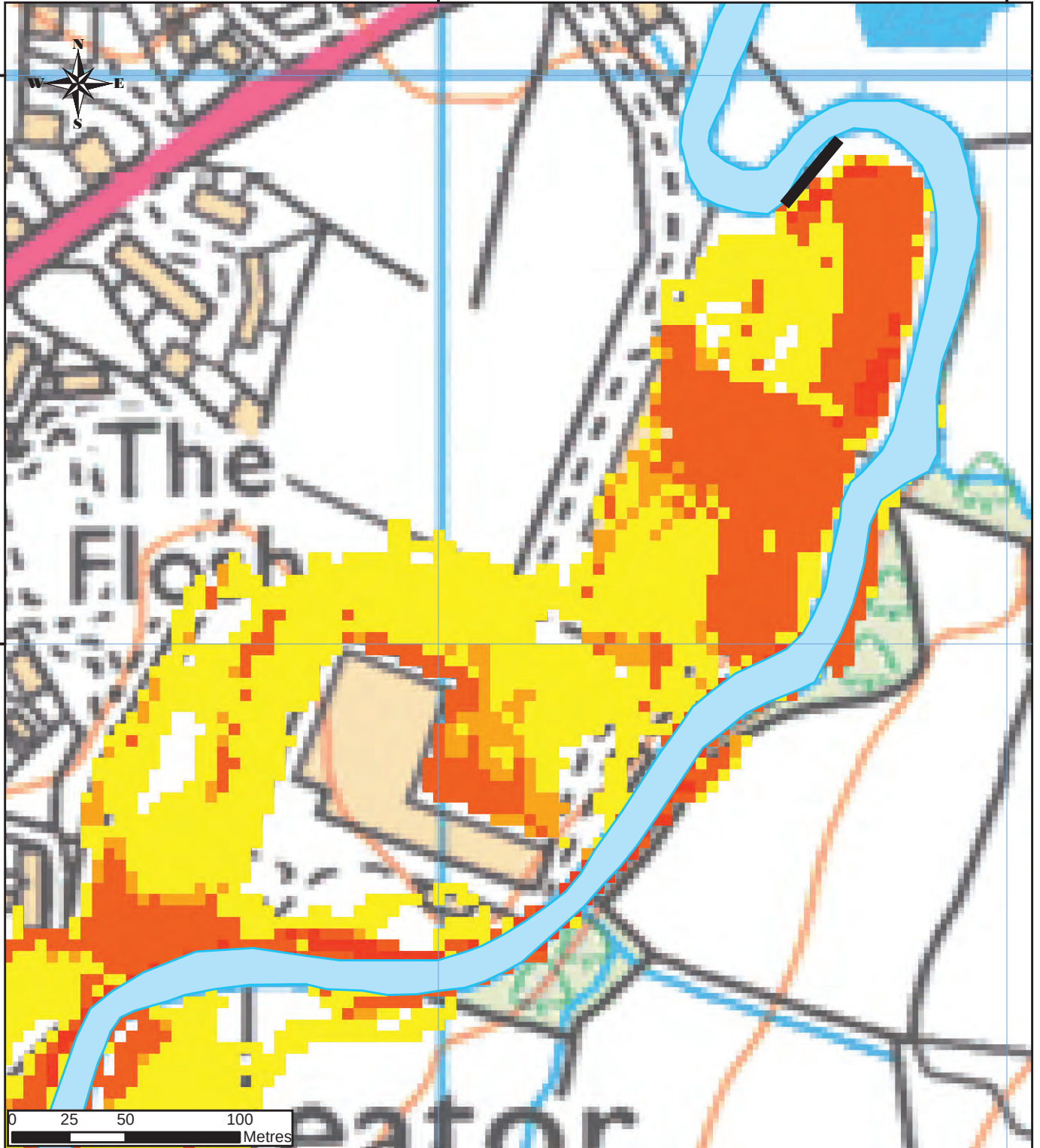


302000

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514000

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Flood Hazard Category

- Low
- Moderate
- Significant
- Extreme

KEY

- Breach 1 Location
- River Ehen

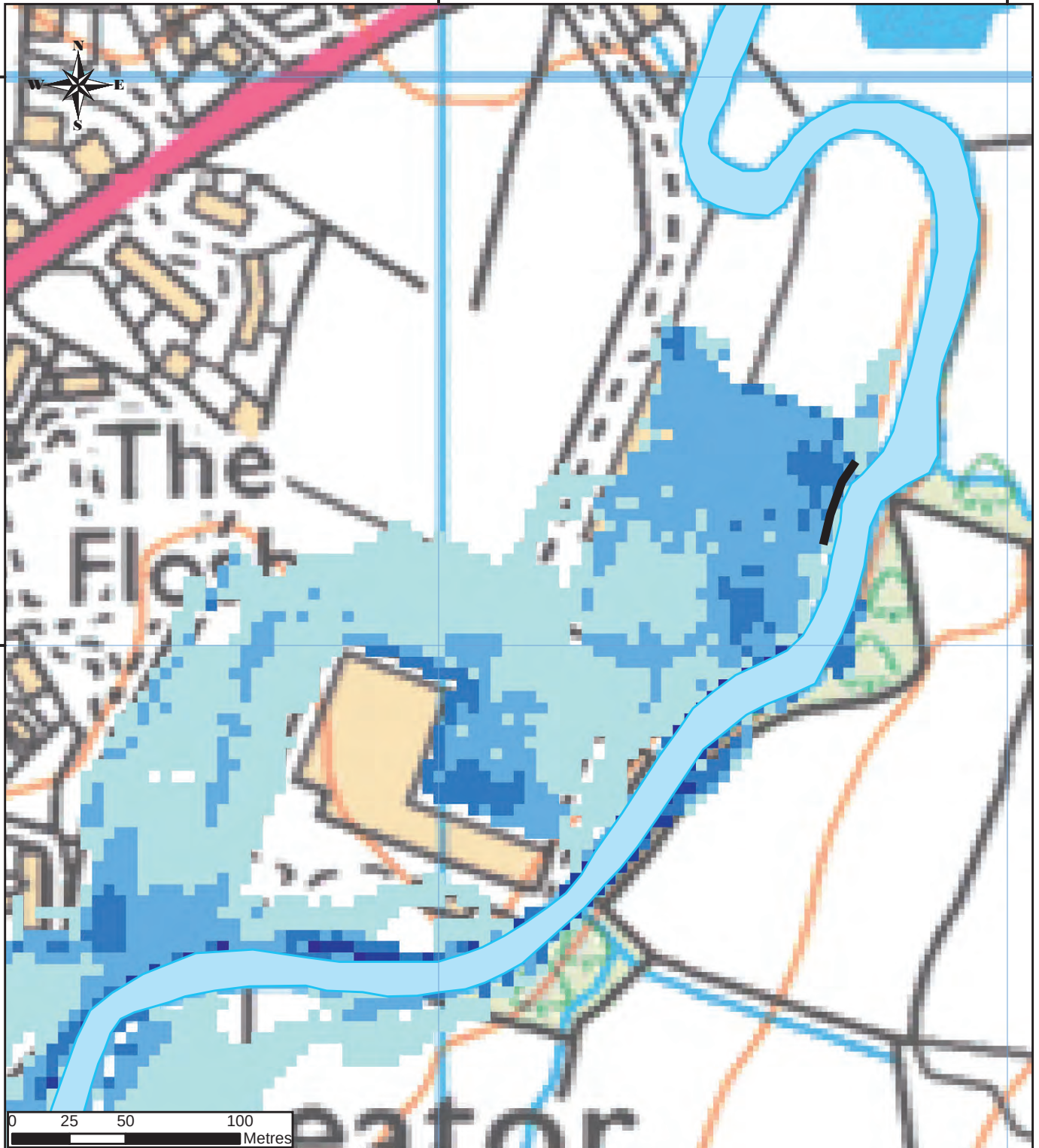
APPENDIX C
BREACH 2 FLOOD MAPS – FIGURES 7A, 7B, 7C AND 7D

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302250

514000

513750



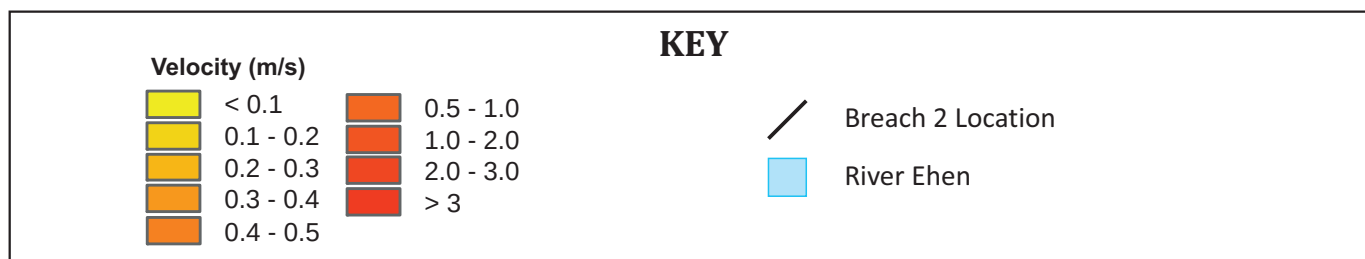
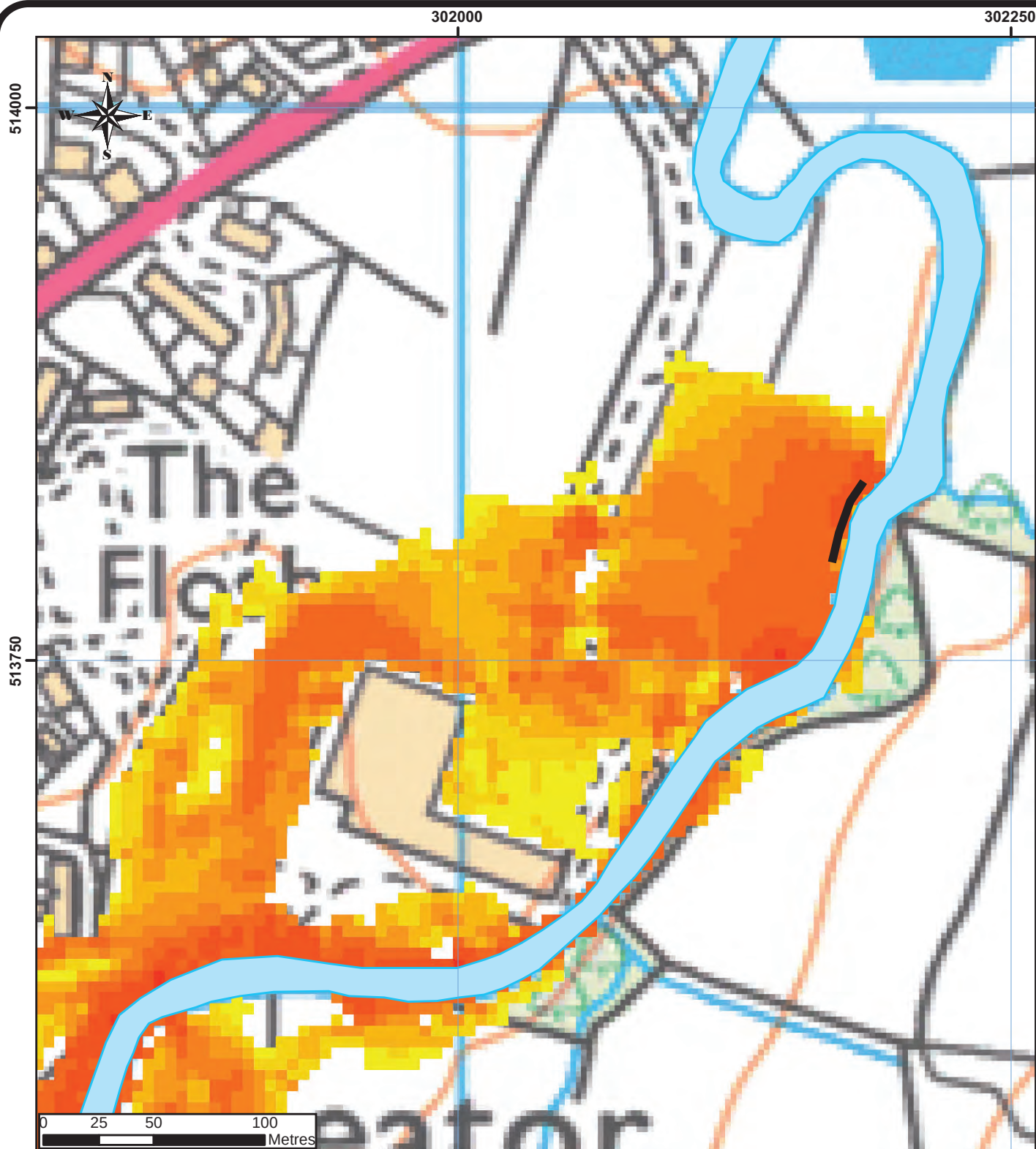
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Flood Depth (m)

0.01 - 0.25
0.25 - 0.50
0.50 - 1.00
1.00 - 1.50
1.50 - 2.50

KEY

	Breach 2 Location
	River Ehen

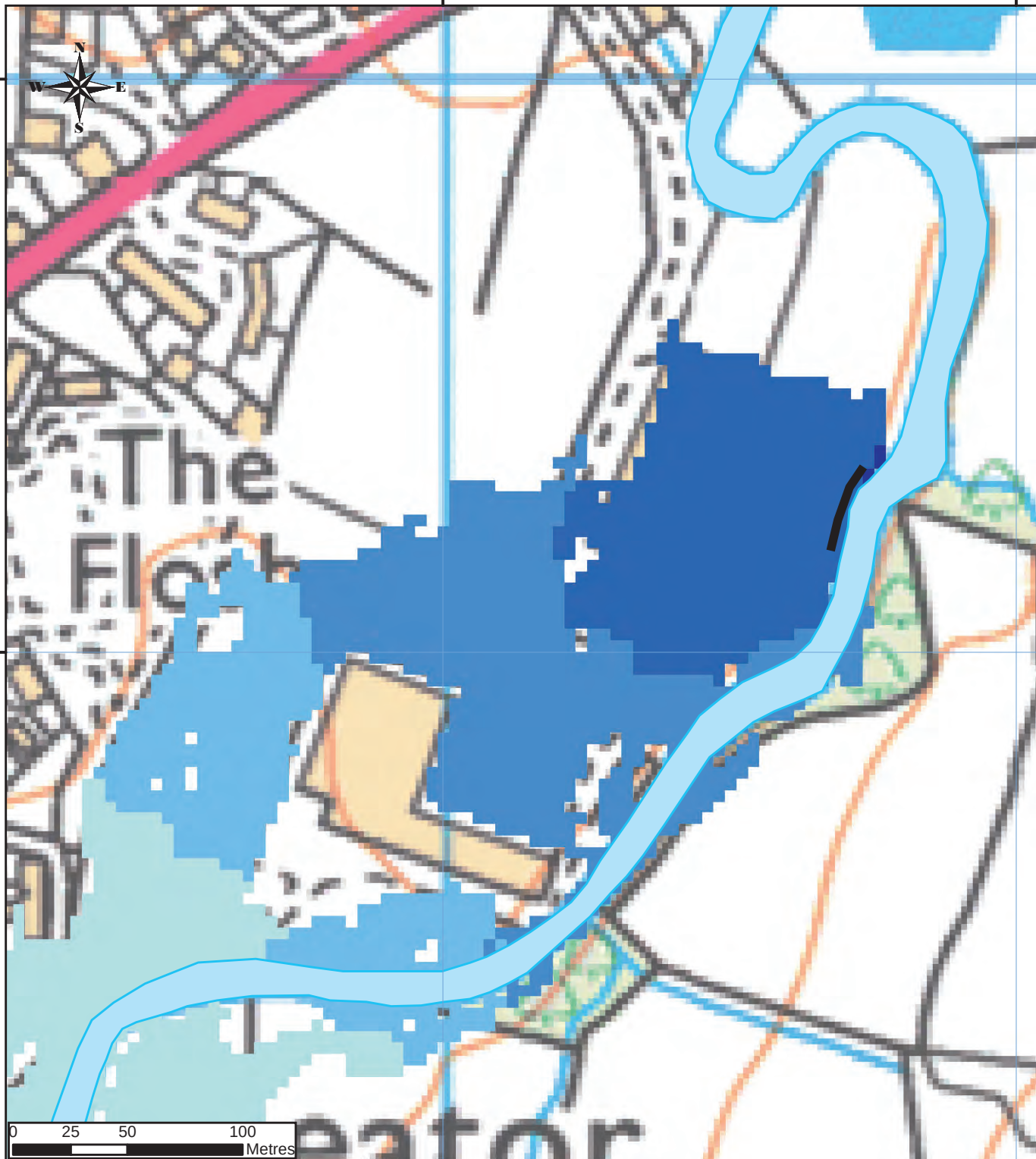


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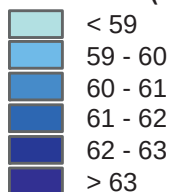
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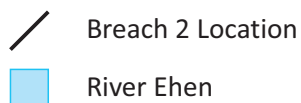


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WaterLevel (mAOD)



KEY

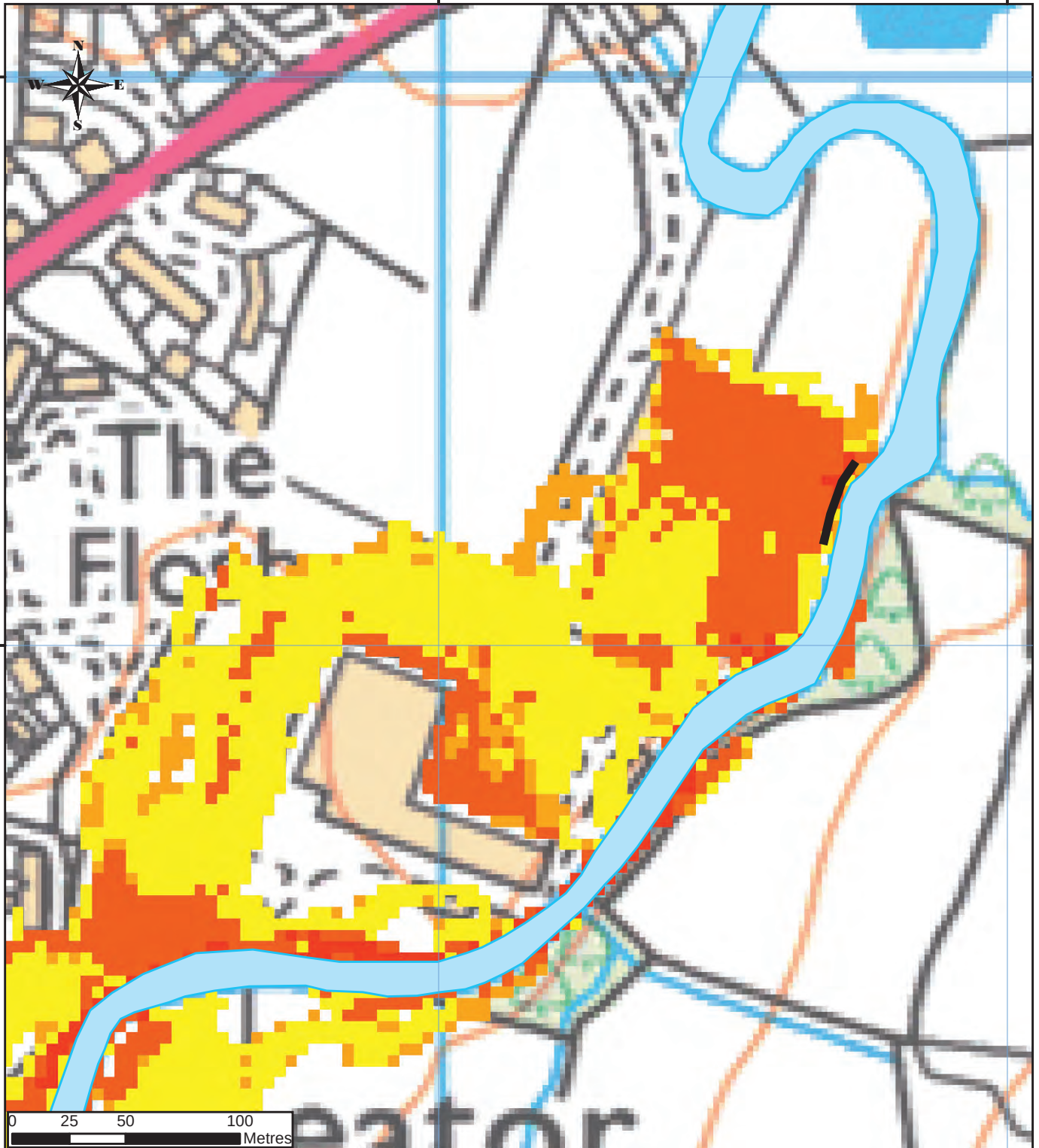


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Flood Hazard Category

- Low
- Moderate
- Significant
- Extreme

KEY

- Breach 2 Location
- River Ehen

Appendix F Watercourse Model



Figure 1: Tributary Flood Velocity 20 year
Cleator Mills

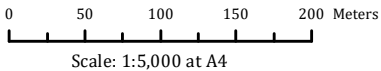


Maximum Velocity (m/s)

- < 0.1
- 0.1 - 0.25
- 0.25 - 0.5
- 0.5 - 0.75
- 0.75 - 1.0
- > 1.0

Notes:

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31 August 2022
NGR: 302,130 E / 513,903 N

Project No. P21-281
Client: RWO Assocaites
Drawn by: RH
Ref: 20yrV



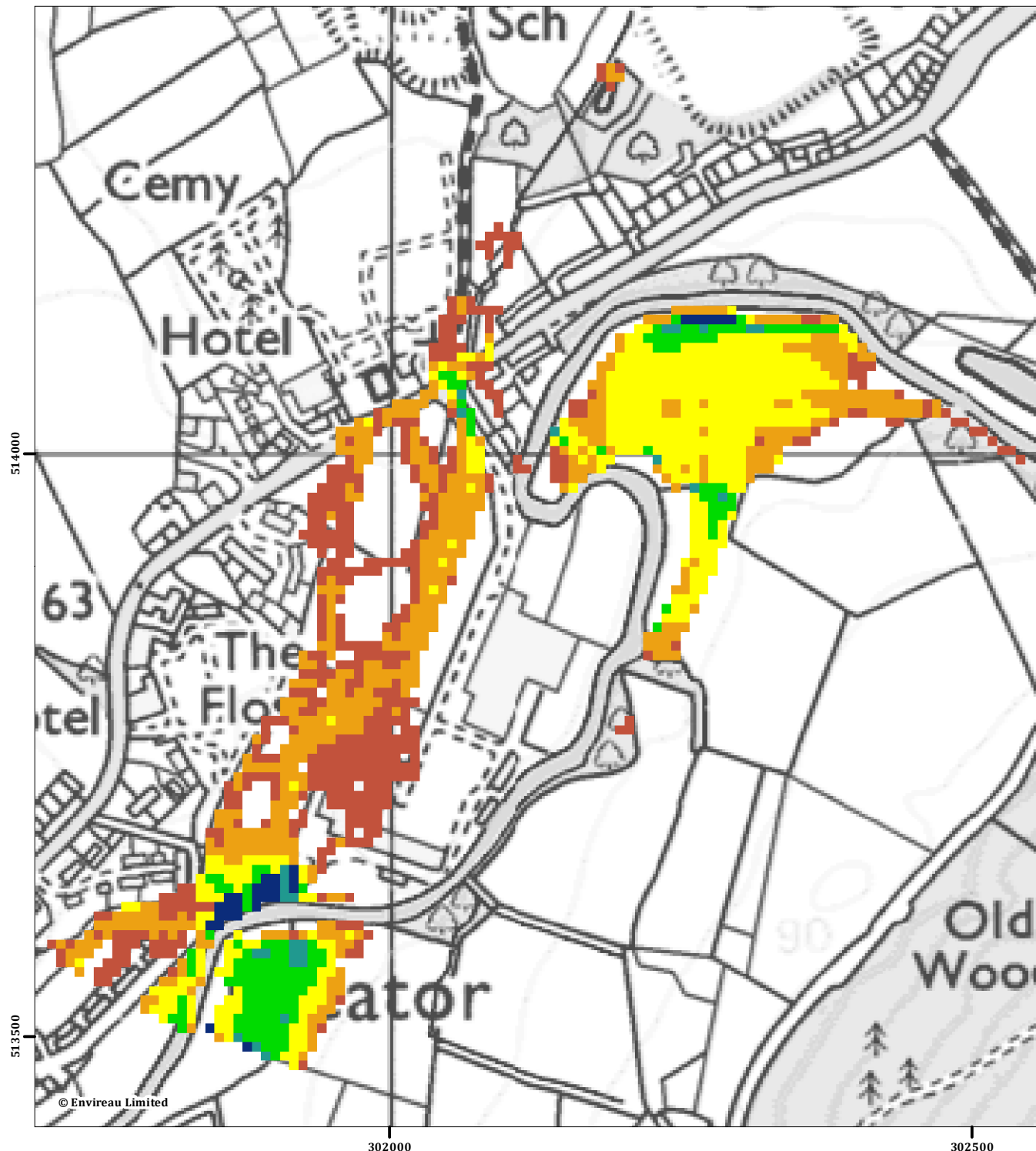


Figure 2: Tributary Flood Velocity 100 year

Cleator Mills

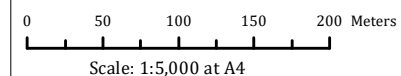


Maximum Velocity (m/s)

- < 0.1
- 0.1 - 0.25
- 0.25 - 0.5
- 0.5 - 0.75
- 0.75 - 1.0
- > 1.0

Notes:

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31 August 2022

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Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 100yrV

envireau
WATER



Figure 3: Tributary Flood Velocity 100 year + CC

Cleator Mills



Maximum Velocity (m/s)

- < 0.1
- 0.1 - 0.25
- 0.25 - 0.5
- 0.5 - 0.75
- 0.75 - 1.0
- > 1.0

Notes:

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0 50 100 150 200 Meters
Scale: 1:5,000 at A4

31 August 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Associates

Drawn by: RH

Ref: 100yrCCV

envireau
WATER

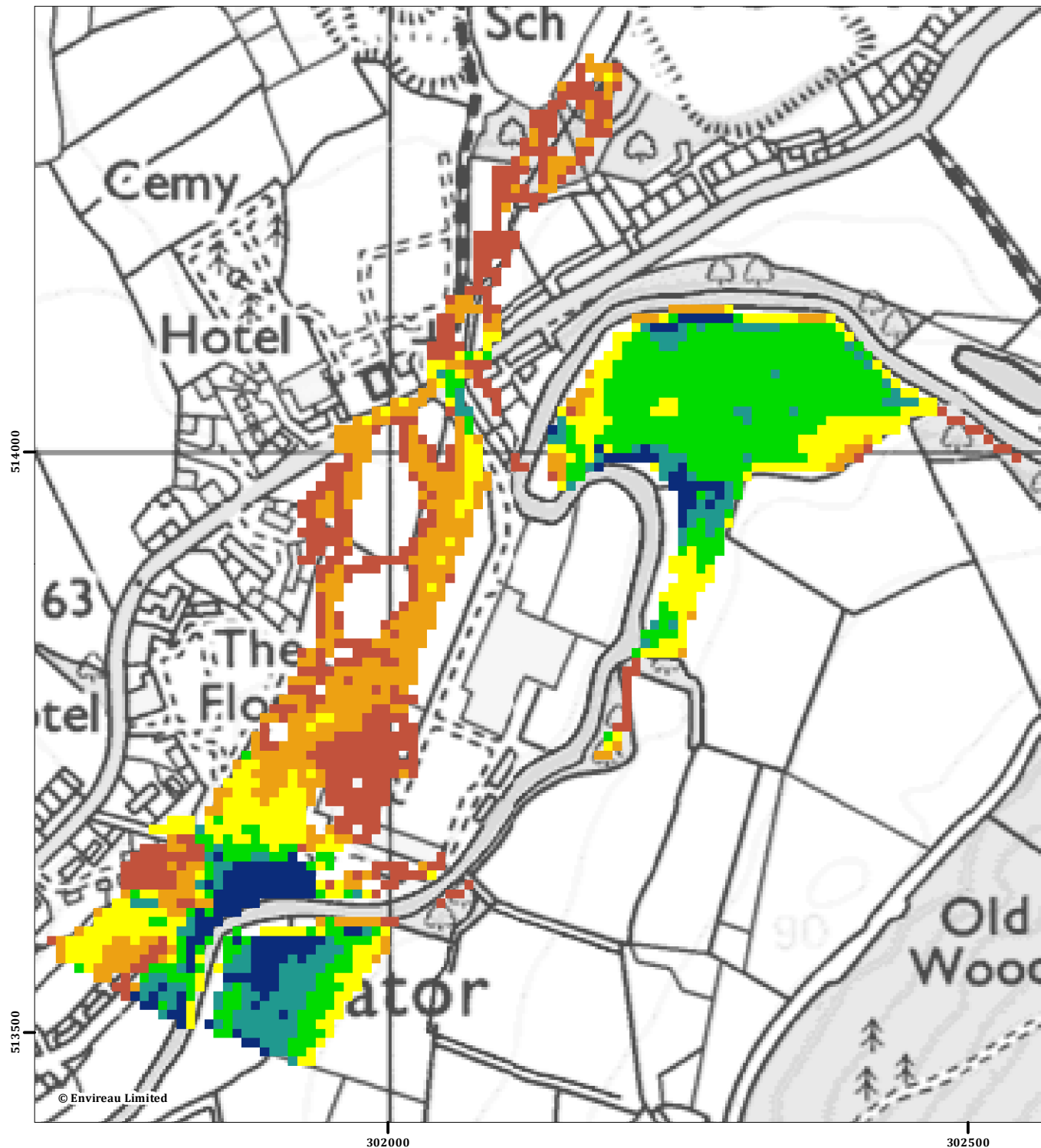


Figure 4: Tributary Flood Velocity 1,000 year

Cleator Mills

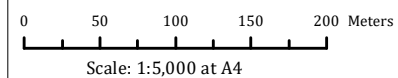


Maximum Velocity (m/s)

-  < 0.1
-  0.1 - 0.25
-  0.25 - 0.5
-  0.5 - 0.75
-  0.75 - 1.0
-  > 1.0

Notes:

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31 August 2022

NGR: 302,130 E / 513,903 N

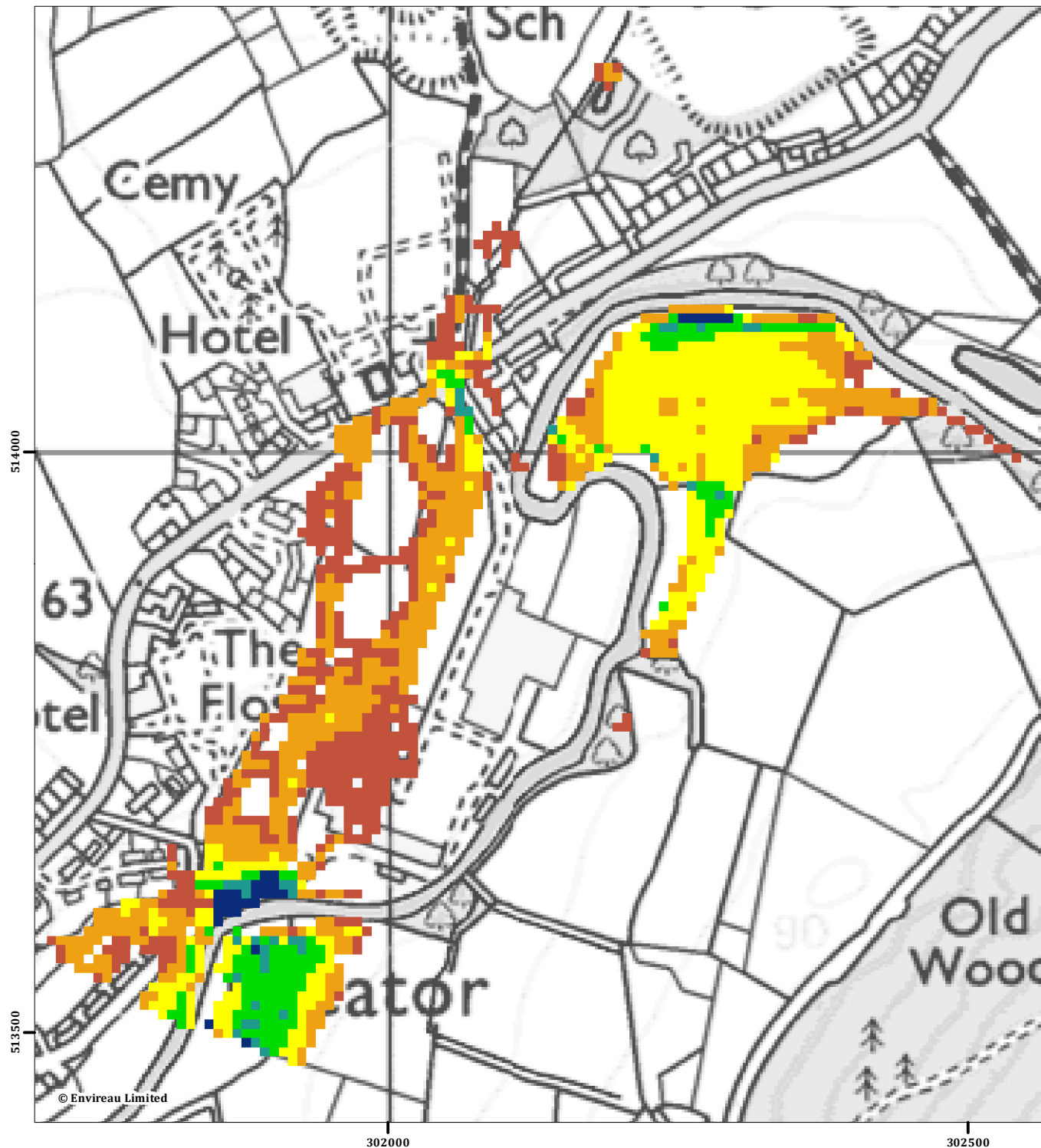
Project No. P21-281

Client: RWO Associates

Drawn by: RH

Ref: 1000yrV

envireau
WATER



**Figure 5: Tributary Flood Velocity 100 year
90% Blockage**

Cleator Mills

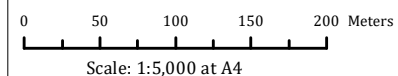
Maximum Velocity (m/s)

- < 0.1
- 0.1 - 0.25
- 0.25 - 0.5
- 0.5 - 0.75
- 0.75 - 1.0
- > 1.0



Notes:

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31 August 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Associates

Drawn by: RH

Ref: 100yr90%BlockedV

envireau
WATER



**Figure 5: Tributary Flood Velocity 100 year + CC
90% Blockage**

Cleator Mills

Maximum Velocity (m/s)

- < 0.1
- 0.1 - 0.25
- 0.25 - 0.5
- 0.5 - 0.75
- 0.75 - 1.0
- > 1.0

Notes:

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0 50 100 150 200 Meters
Scale: 1:5,000 at A4

31 August 2022
NGR: 302,130 E / 513,903 N

Project No. P21-281
Client: RWO Assocaites
Drawn by: RH
Ref: 100yrCC90%BlockedV

envireau
WATER

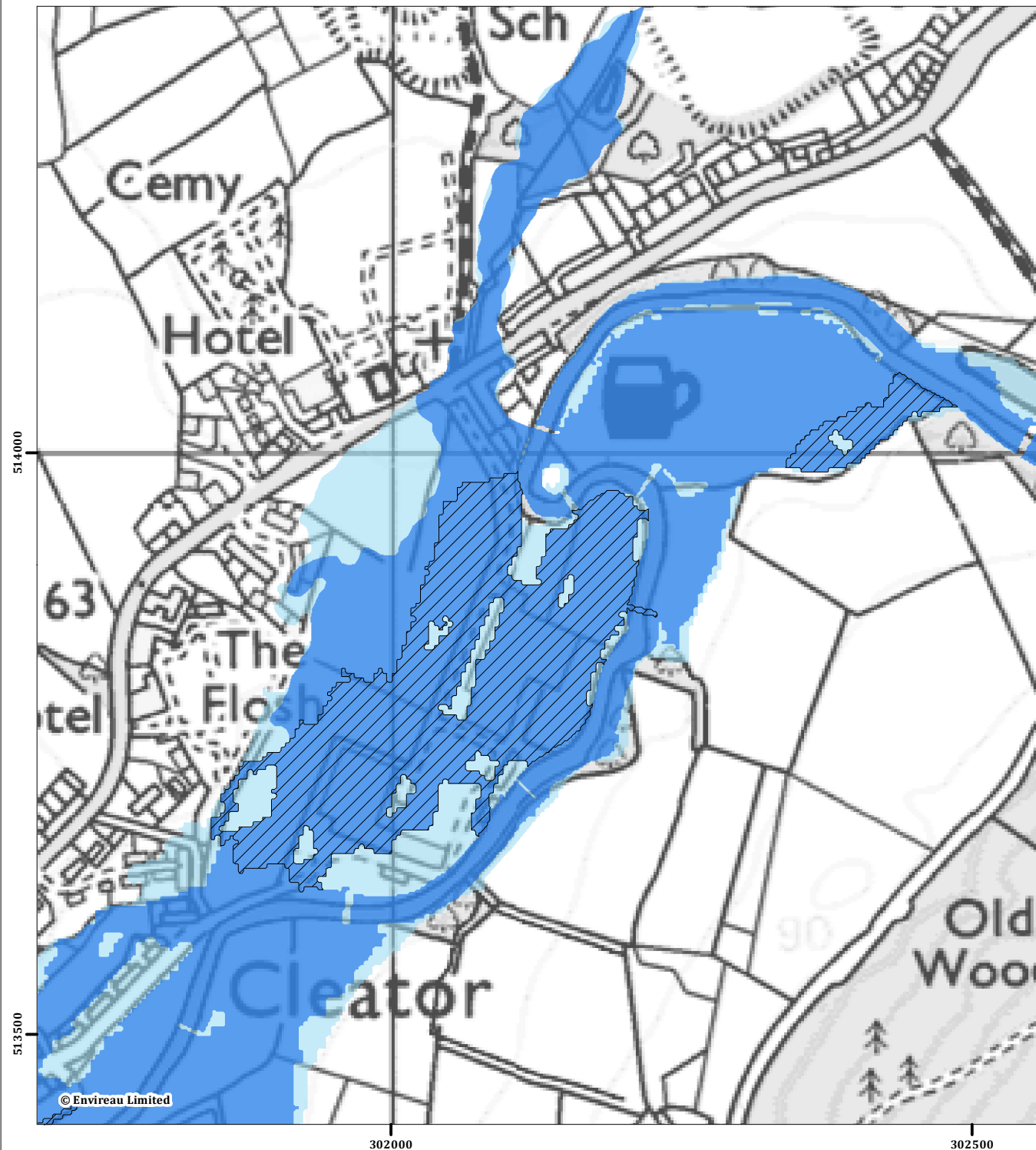


Figure 1: Environment Agency Mapped Flood Risk 
Cleator Mills

-  Areas Benefiting from Flood Defences
-  Environment Agency Flood Zone 3
-  Environment Agency Flood Zone 2

Notes:

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0 50 100 150 200 Meters
Scale: 1:5,000 at A4

30 June 2022
NGR: 302,130 E / 513,903 N

Project No. P21-281
Client: RWO Assocaites
Drawn by: RH
Ref: EAFloodRisk

envireau 
WATER



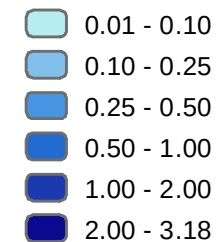


Figure 2: Tributary Flood Risk 20 year

Cleator Mills

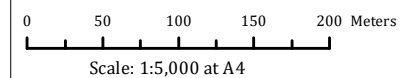


Maximum Flood Depth (m)



Notes:

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 20yr





Figure 3: Tributary Flood Risk 100 year
Cleator Mills

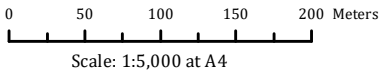


Maximum Flood Depth (m)

- 0.01 - 0.10
- 0.10 - 0.25
- 0.25 - 0.50
- 0.50 - 1.00
- 1.00 - 2.00
- 2.00 - 3.18

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 100yr



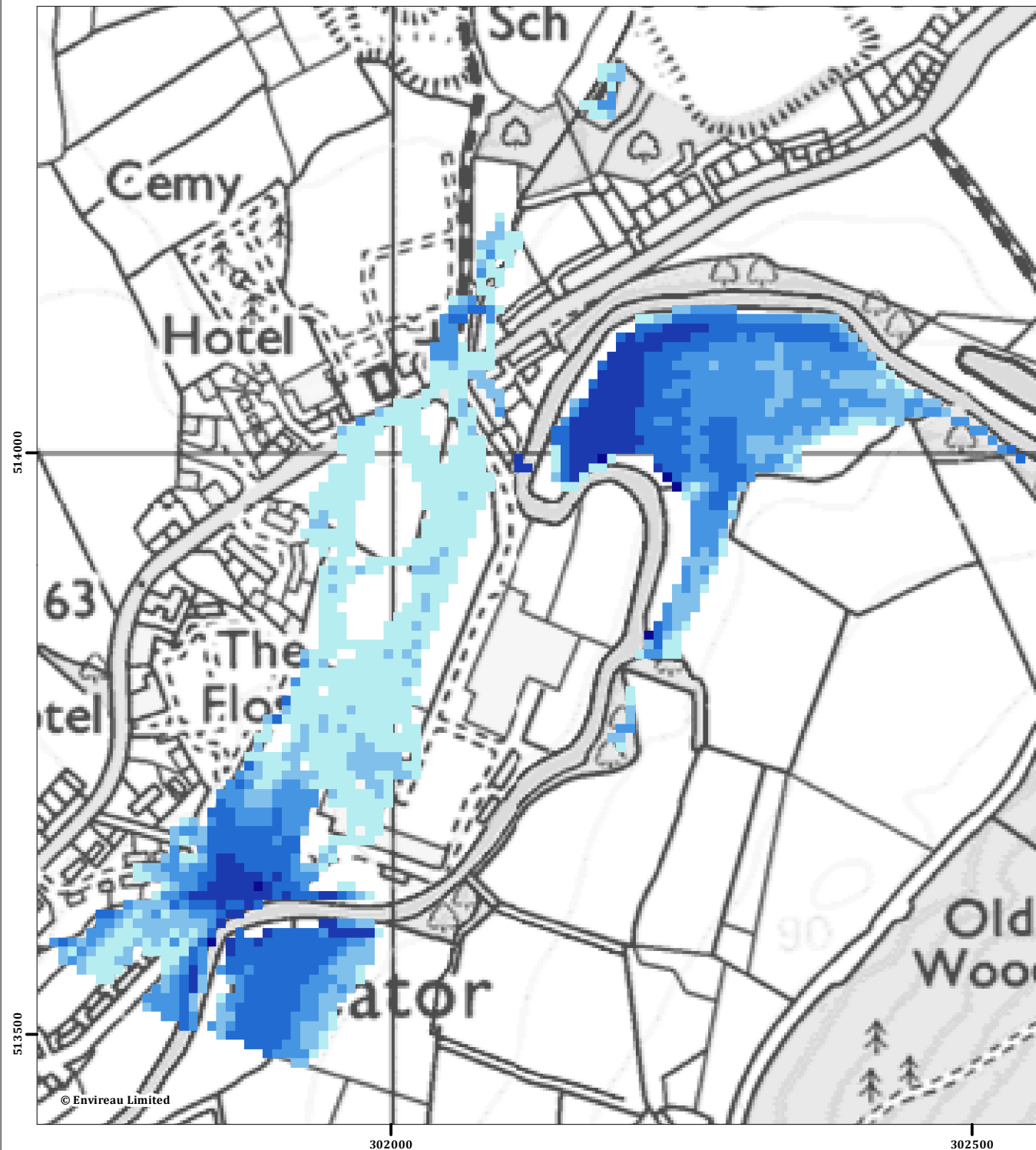
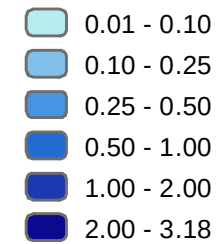


Figure 4: Tributary Flood Risk 100 year plus CC

Cleator Mills

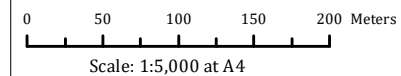


Maximum Flood Depth (m)



Notes:

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 100yrCC



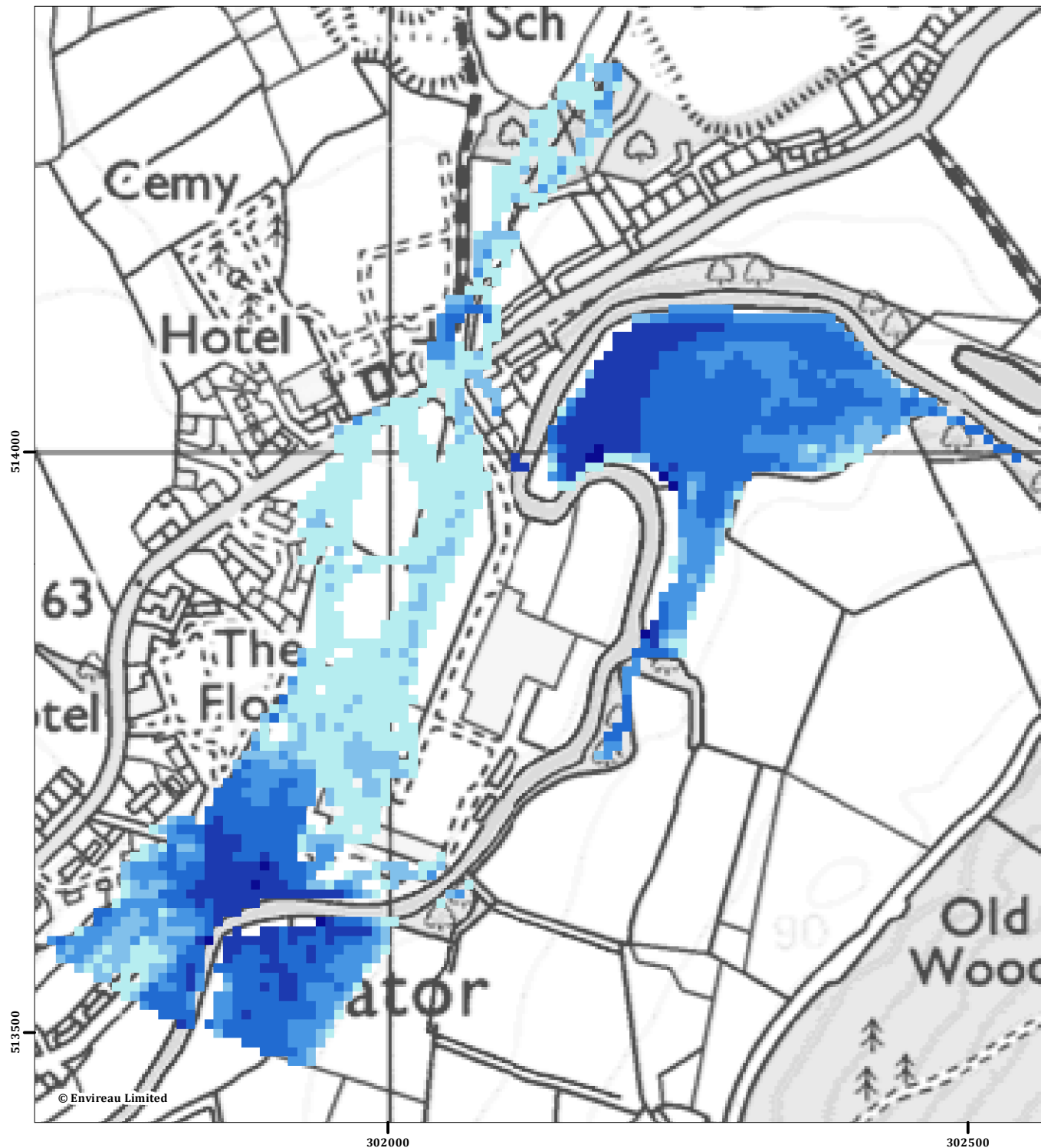
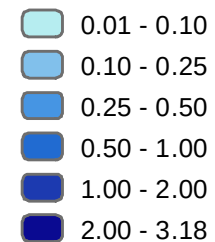


Figure 5: Tributary Flood Risk 1,000 year

Cleator Mills

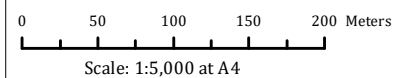


Maximum Flood Depth (m)



Notes:

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 1000yr



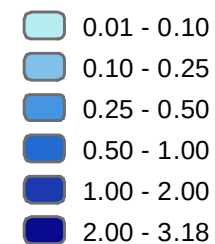


**Figure 6: Tributary Flood Risk 100 year
90% Blocked**



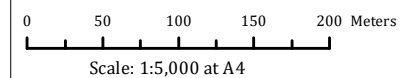
Cleator Mills

Maximum Flood Depth (m)



Notes:

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 100yr90%blocked

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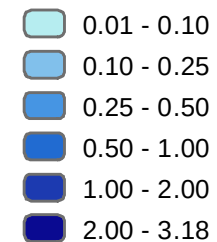


**Figure 7: Tributary Flood Risk 100 year plus CC
90% Blocked**



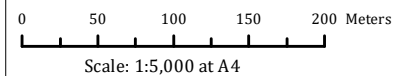
Cleator Mills

Maximum Flood Depth (m)



Notes:

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30 June 2022

NGR: 302,130 E / 513,903 N

Project No. P21-281

Client: RWO Assocaites

Drawn by: RH

Ref: 100yrCC90%blocked



Appendix G Environment Agency Flood Data

Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

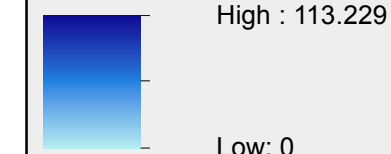
NGR: 301,733 514,107

Key

 Main River

1 in 30 Undefended Scenario

mAOD

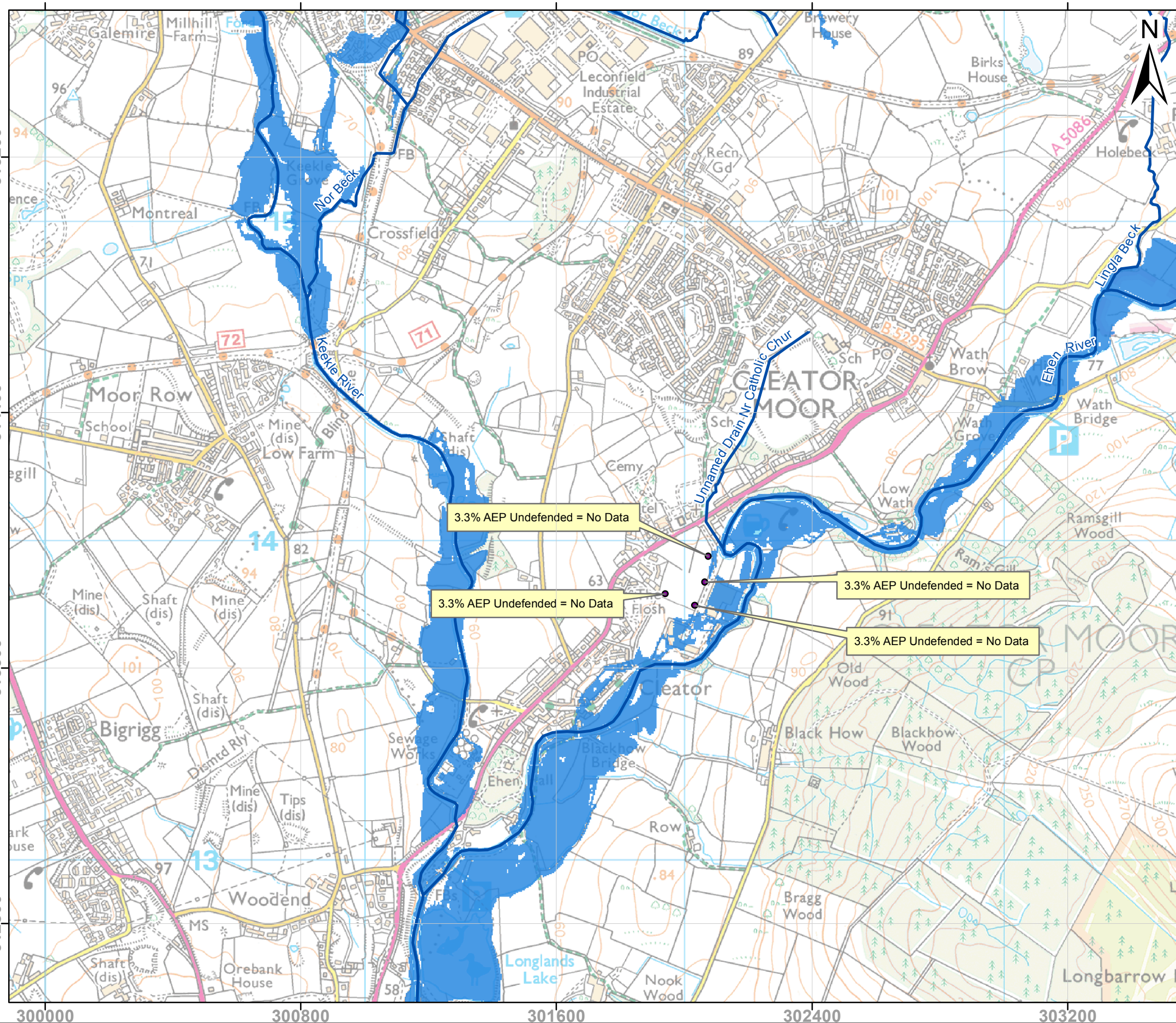


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

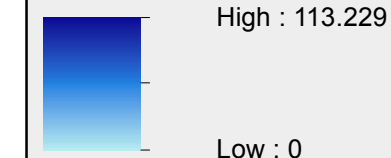
NGR: 301,733 514,107

Key

 Main River

1 in 30 Defended Scenario

mAOD

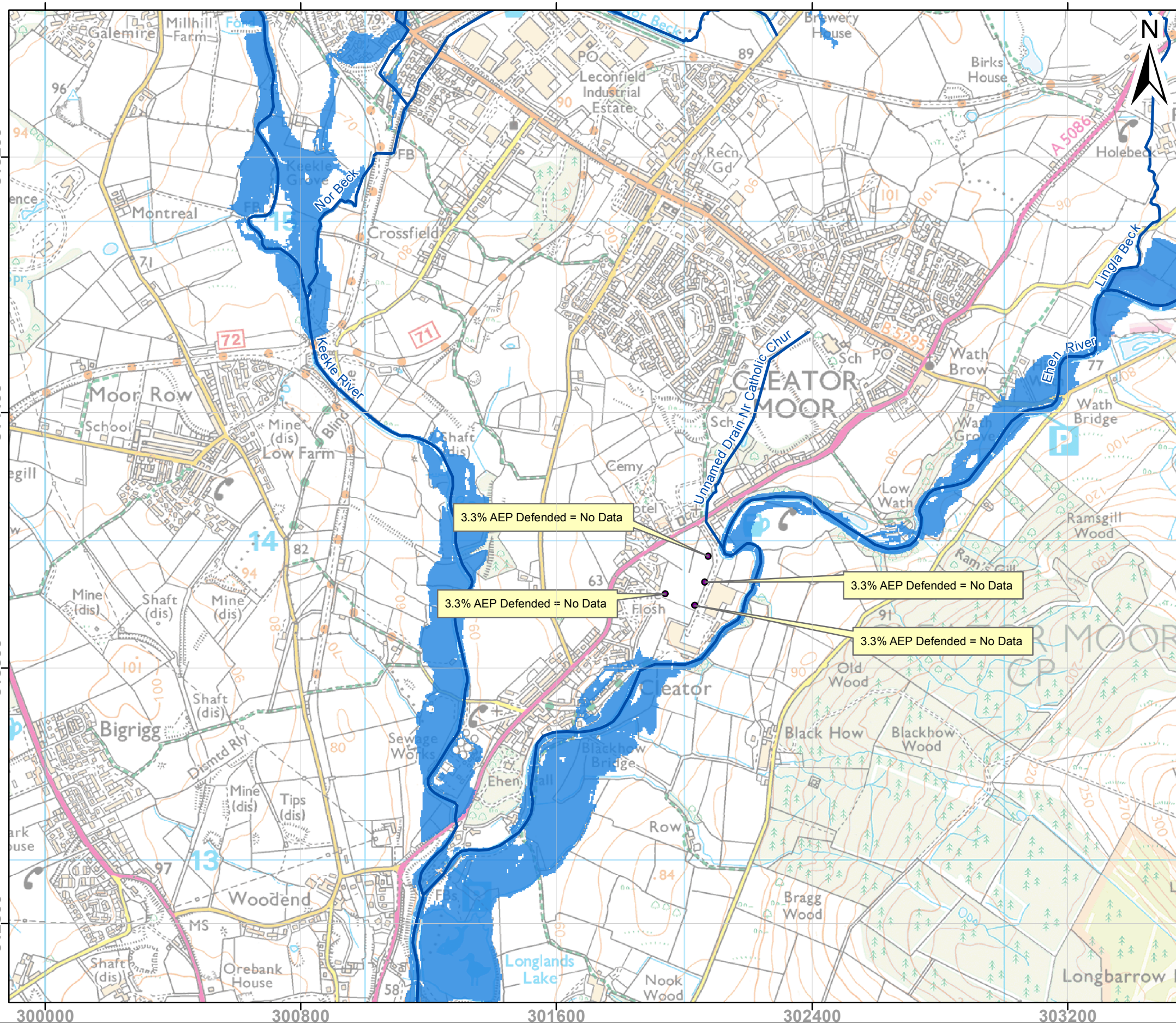


Flood Zone 3 shows the area that could be affected by flooding:

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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 09 July 2019

Our Ref: CL132929

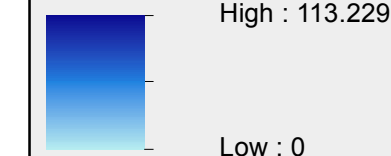
NGR: 301,526 513,720

Key

 Main River

1 in 50 Undefended Scenario

mAOD

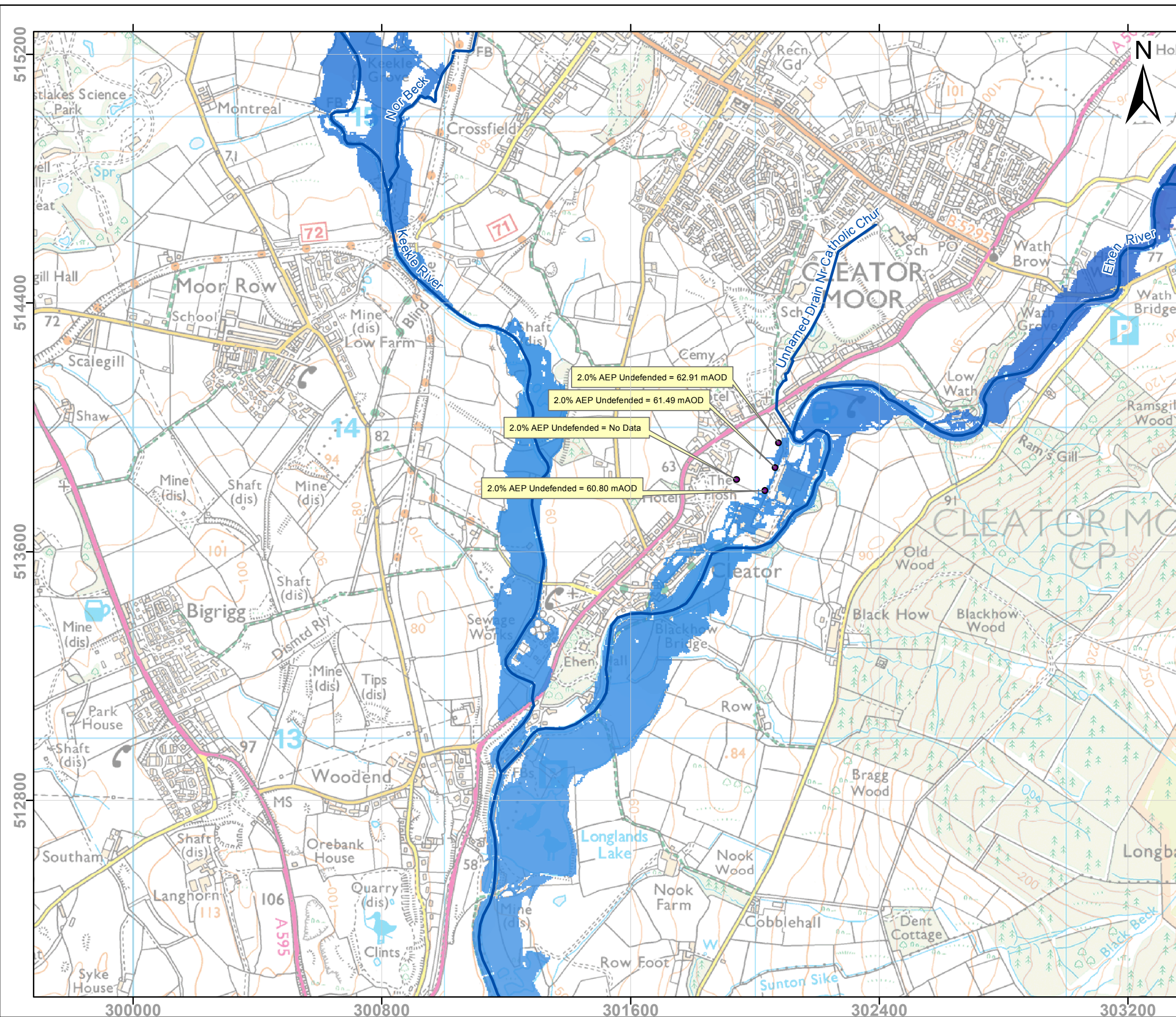


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

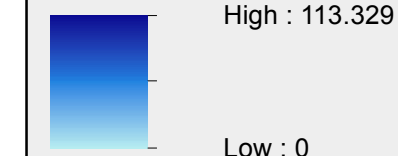
NGR: 301,720 514,026

Key

 Main River

1 in 50 Defended Scenario

mAOD

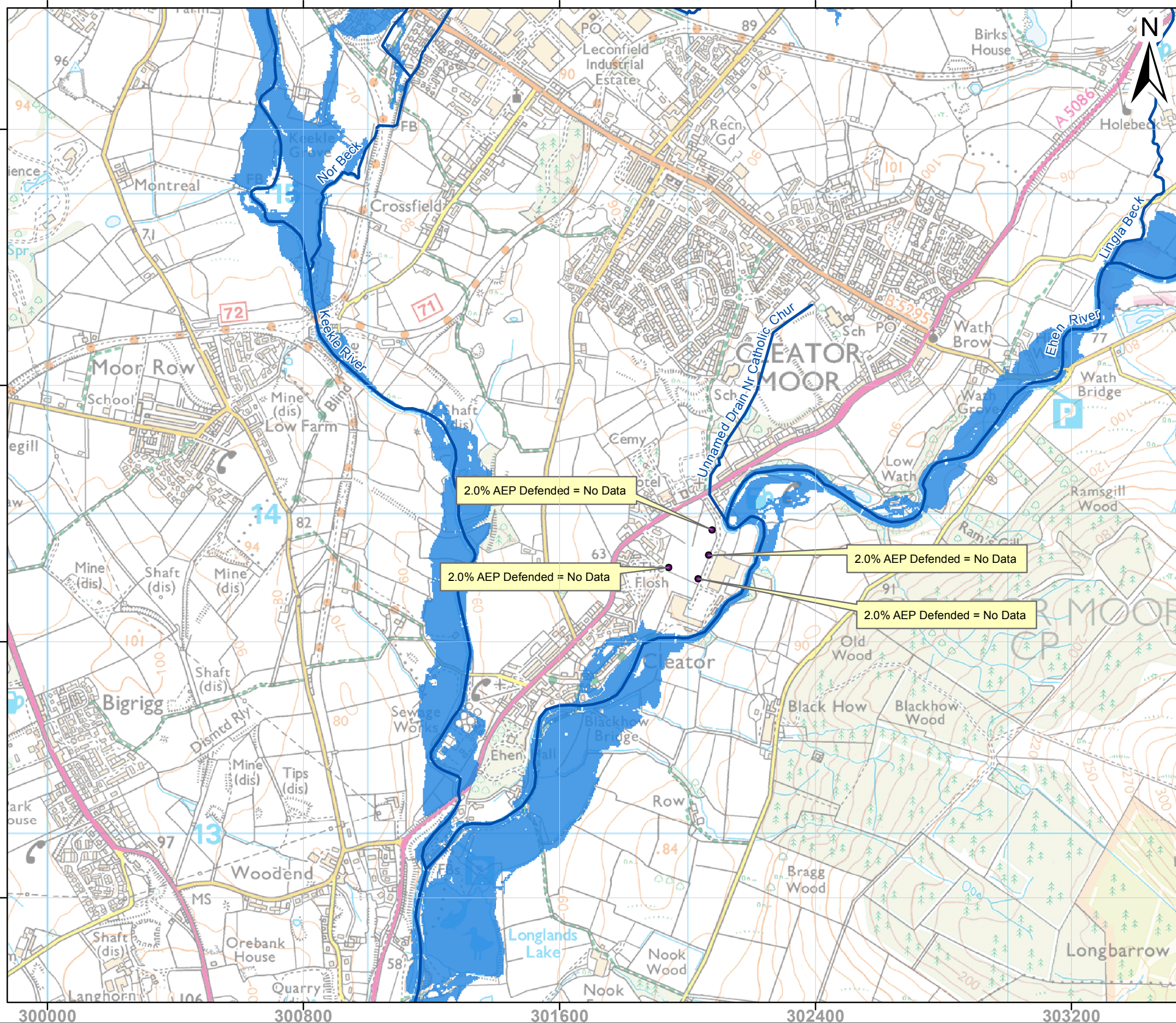


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Produced: 09 July 2019

Our Ref: CL132929

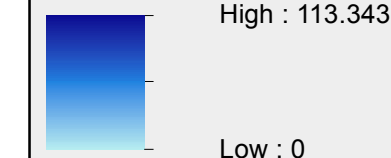
NGR: 301,526 513,720

Key

 Main River

1 in 100 Undefended Scenario

mAOD

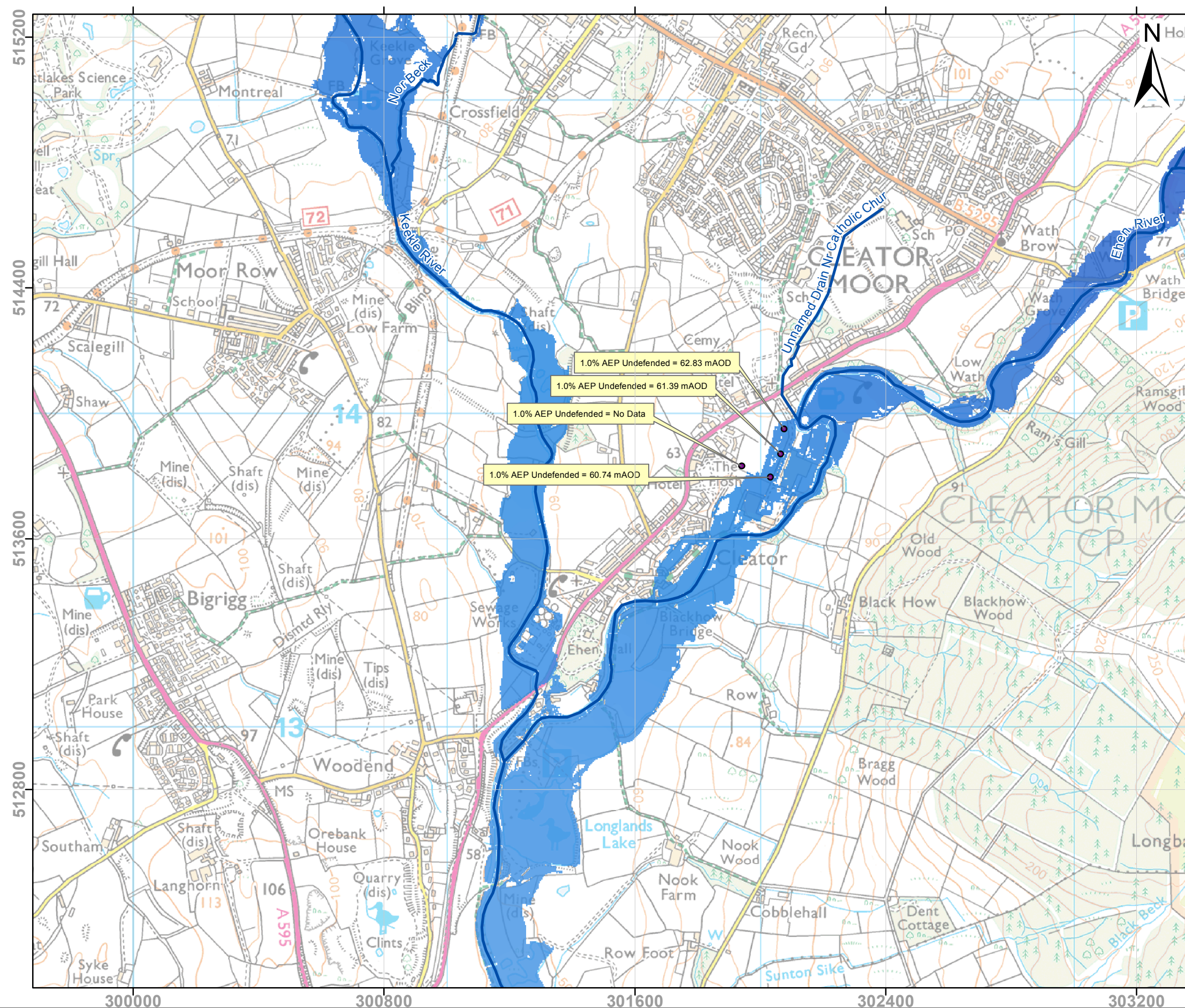
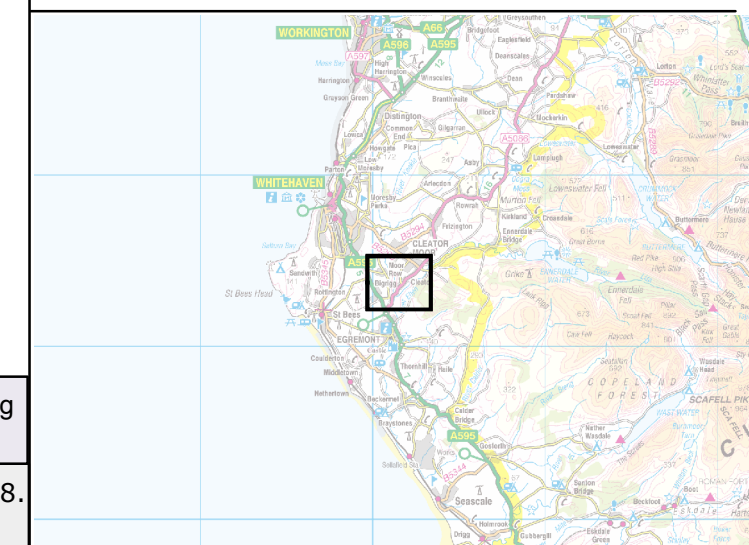


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Produced: 10 July 2019

Our Ref: CL132929

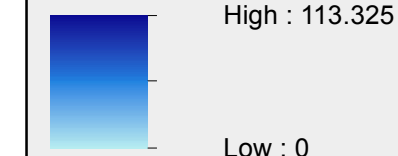
NGR: 301,720 514,026

Key

 Main River

1 in 100 Defended Scenario

mAOD

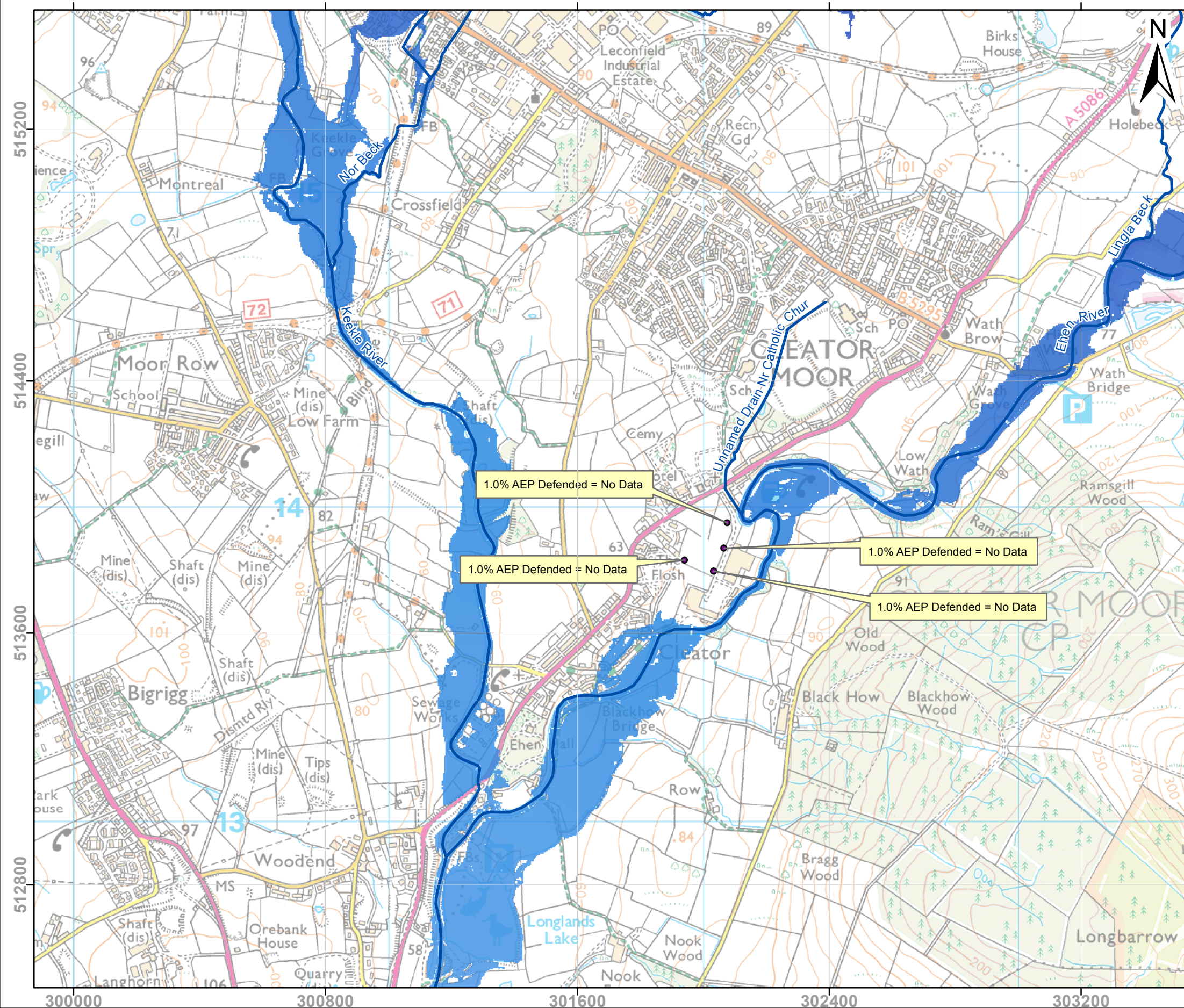


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 09 July 2019

Our Ref: CL132929

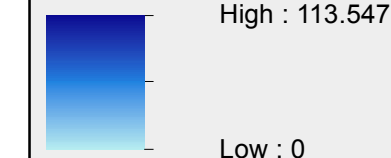
NGR: 301,526 513,720

Key

 Main River

1 in 100 + CC Undefended

mAOD

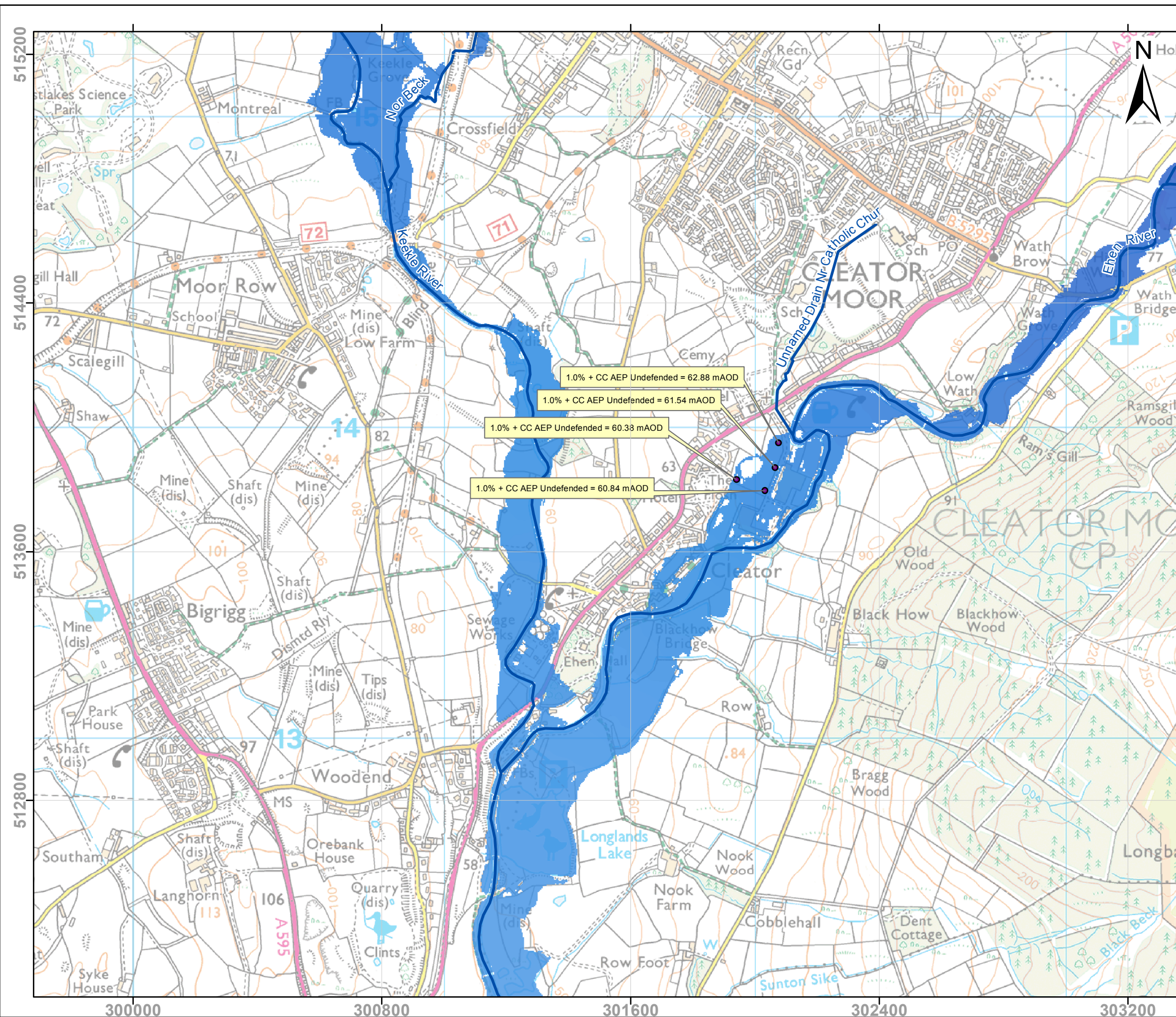


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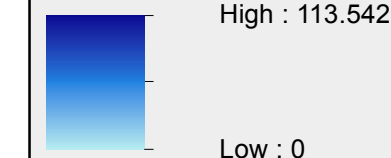
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Key

 Main River

1 in 100 + CC Defended Scenario

mAOD

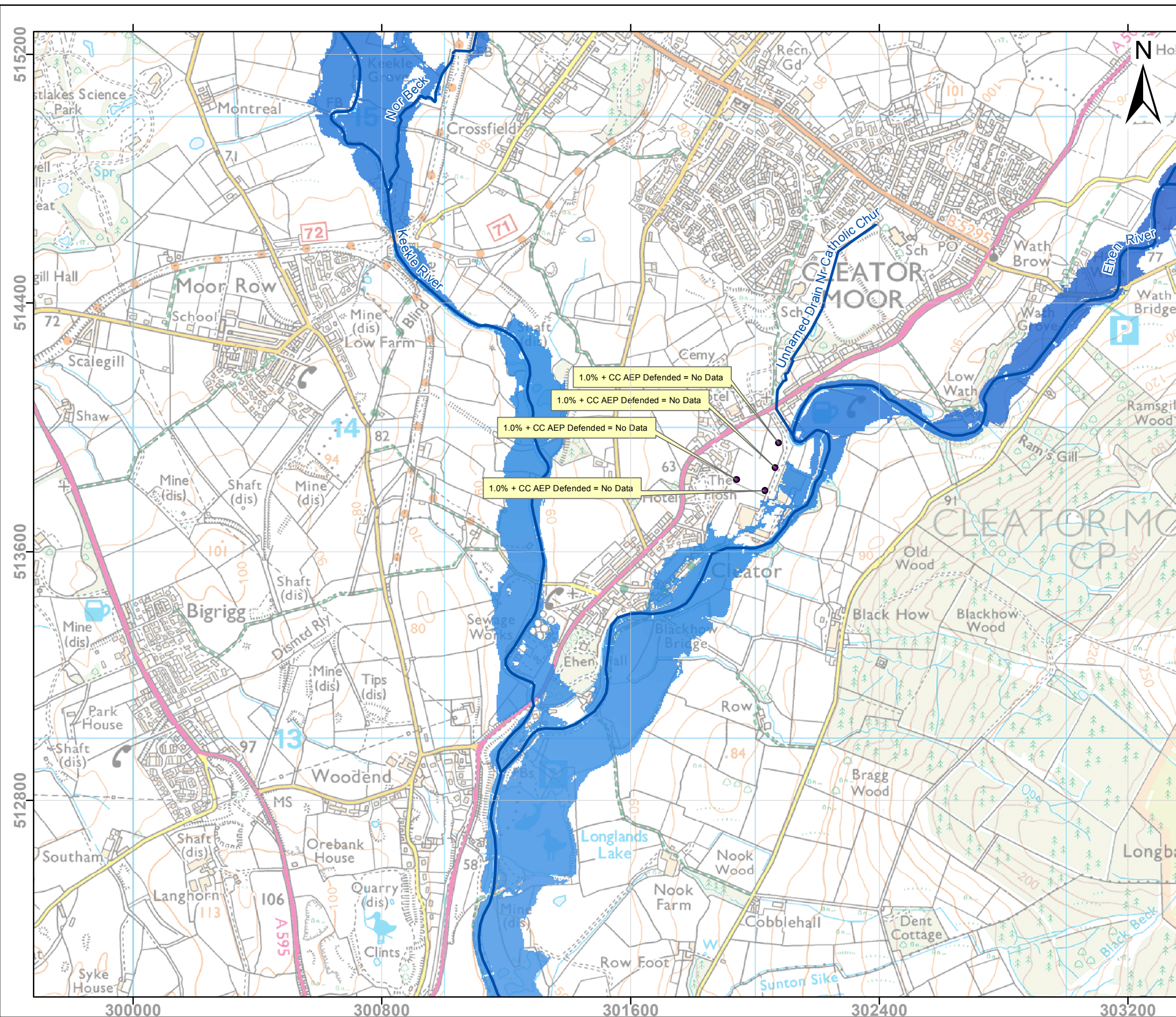
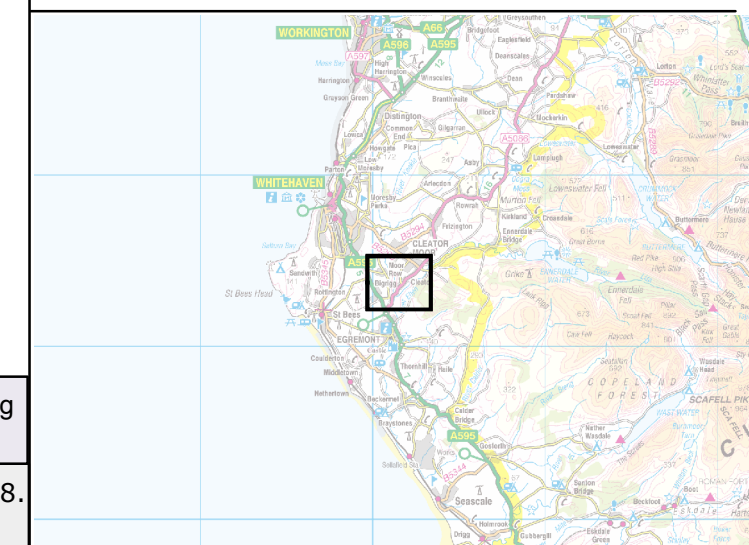


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 09 July 2019

Our Ref: CL132929

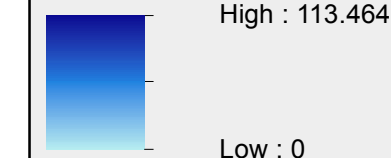
NGR: 301,526 513,720

Key

 Main River

1 in 200 Undefended Scenario

mAOD

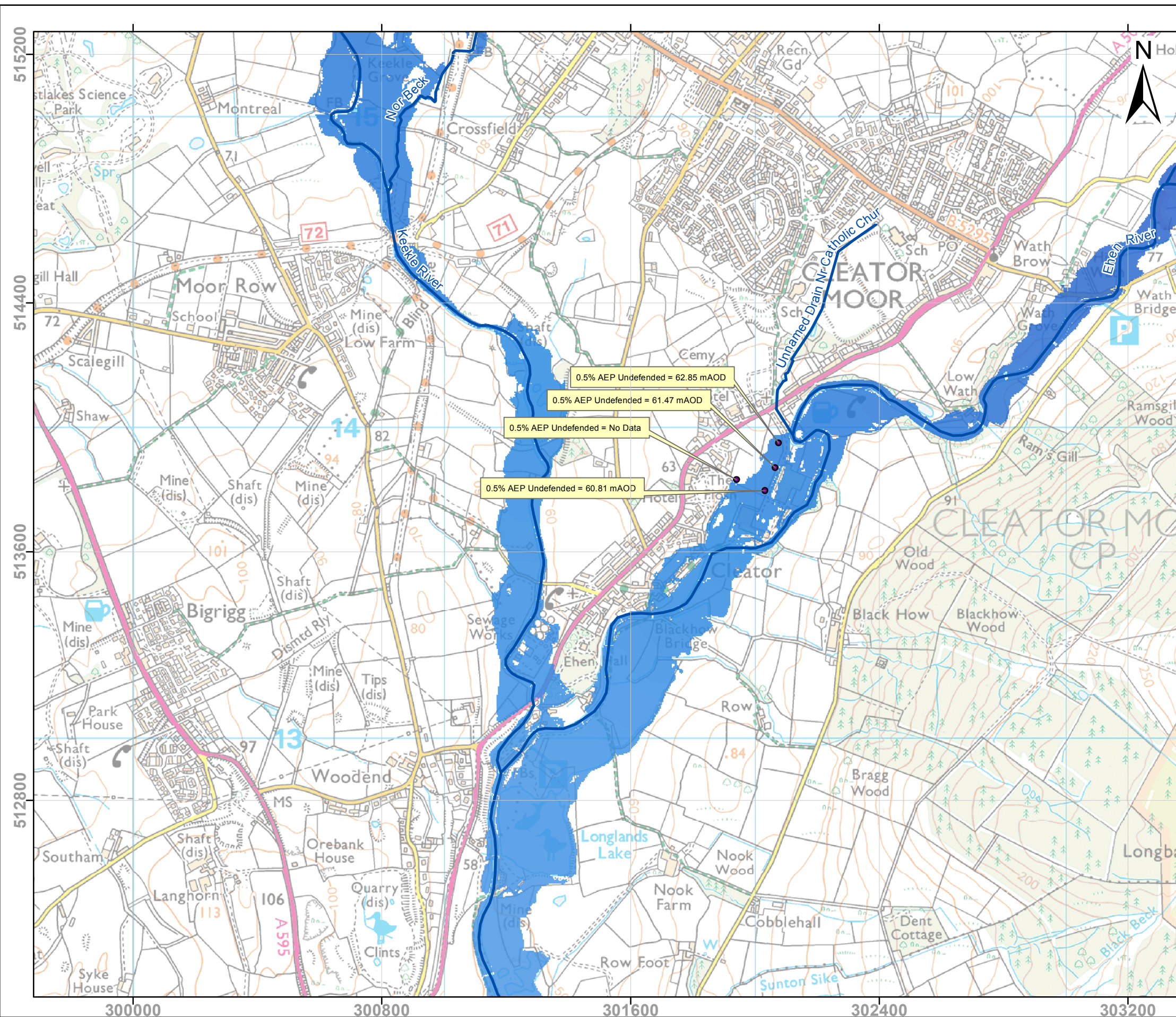
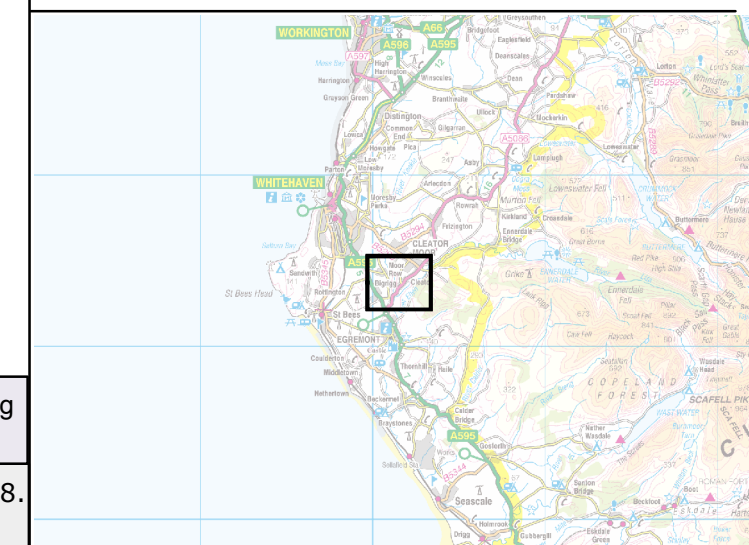


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Produced: 10 July 2019

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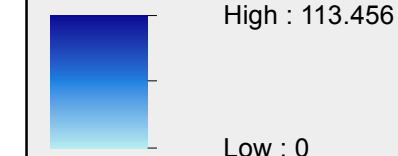
NGR: 301,720 514,026

Key

 Main River

1 in 200 Defended Scenario

mAOD

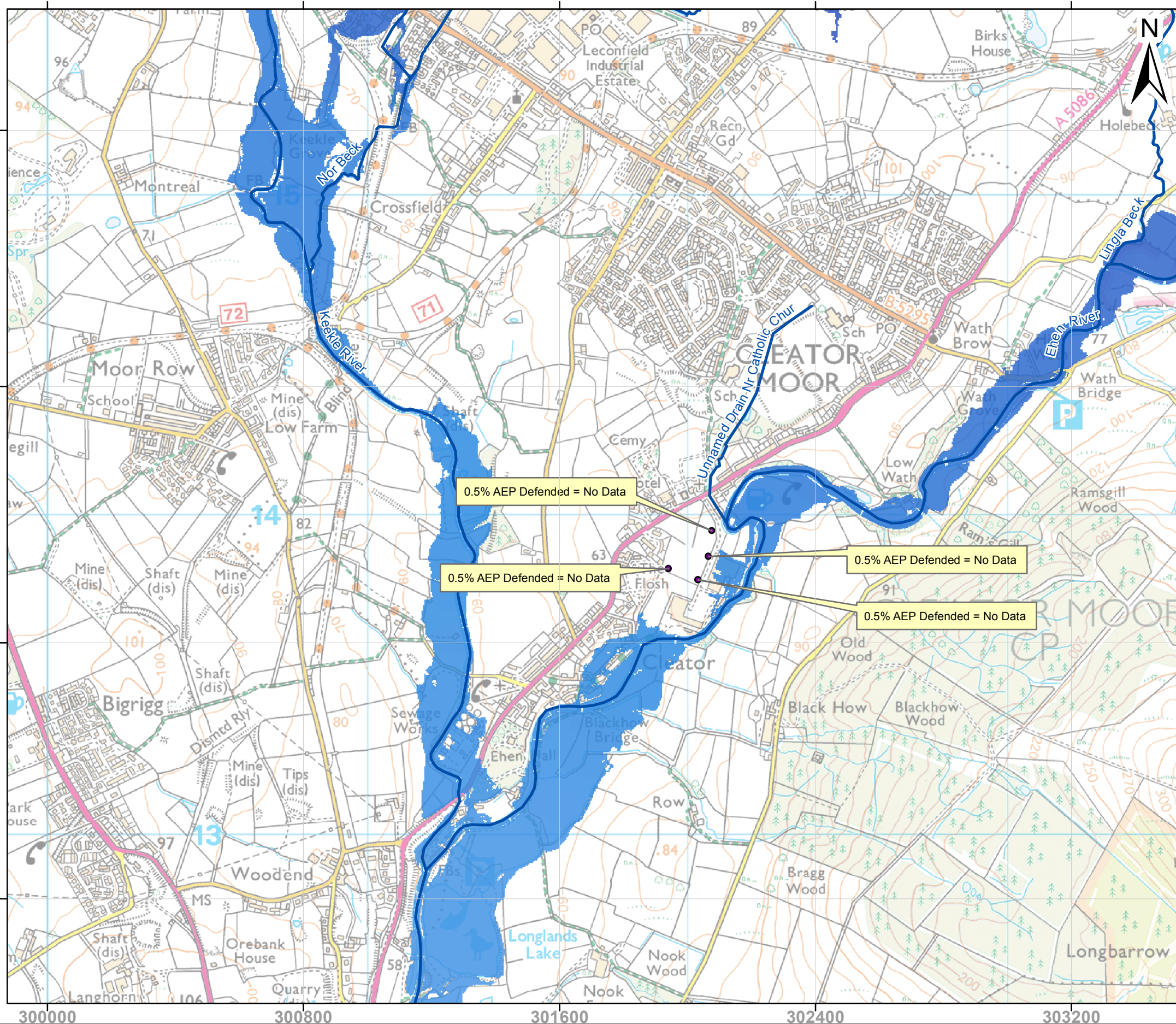


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

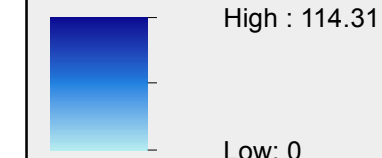
NGR: 301,720 514,026

Key

 Main River

1 in 1000 Undefended Scenario

mAOD

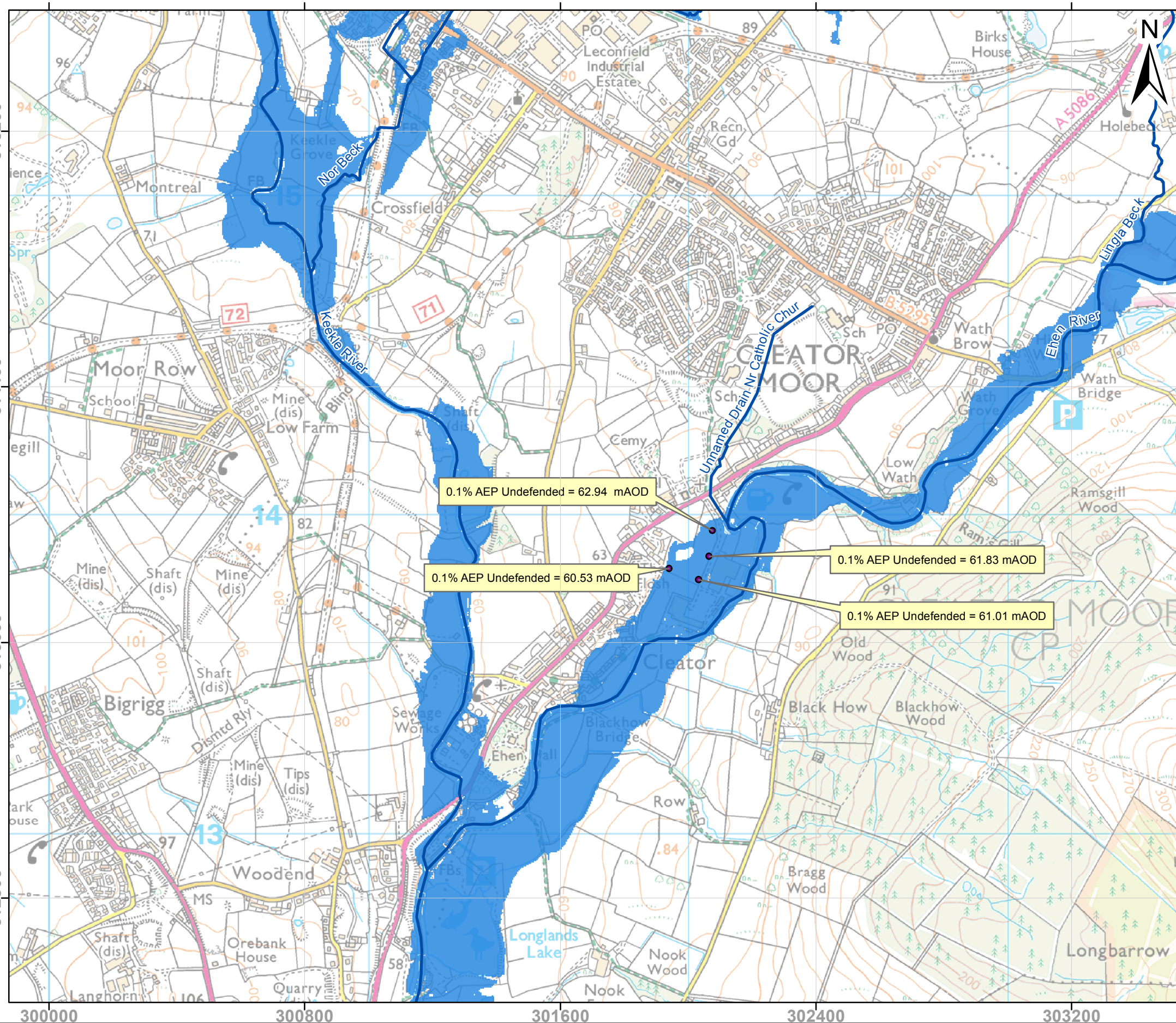


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Fluvial Model Level Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

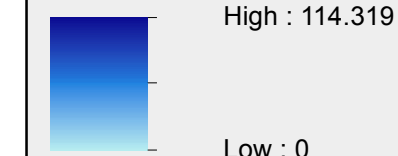
NGR: 301,720 514,026

Key

 Main River

1 in 1000 Defended Scenario

mAOD

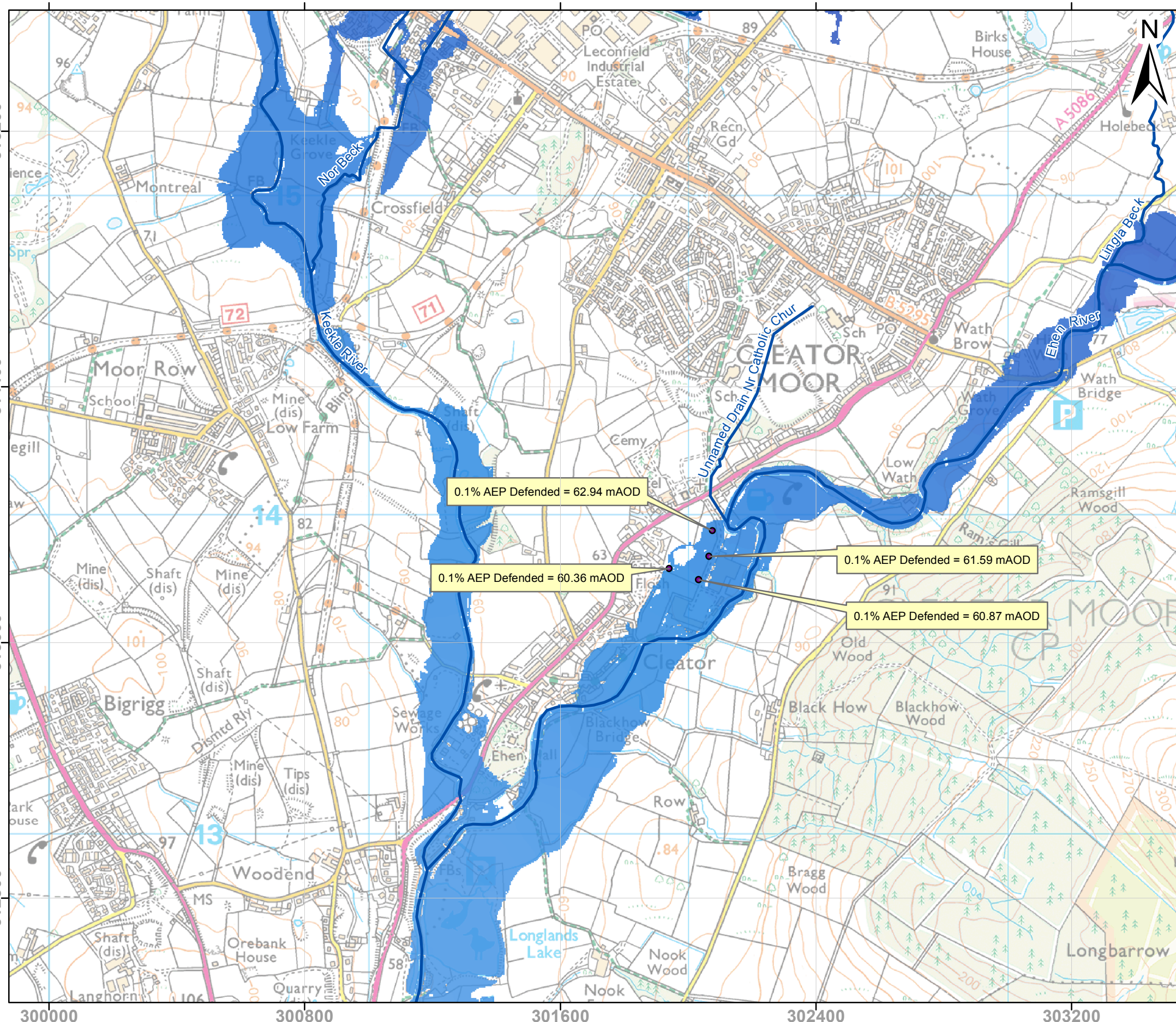


Flood Zone 3 shows the area that could be affected by flooding:

- from the sea with a 0.5% or greater chance of happening each year
- or from a river with a 1.0% or greater chance of happening each year.

Flood Zone 2 shows the extent of an extreme flood from rivers or the sea with up to 0.1% chance of occurring each year.

ABDs (Areas Benefiting from Defences) show the area benefiting from defences during a 0.5% tidal, or 1.0% fluvial flood event.



Modelled water levels with climate change using +20% flow allowances are not suitable for the majority of planning purposes. New climate change allowances can be checked on the following website; www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances.

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Node Point Location Map: Cleator Mills, Cleator, CA23 3DU

Produced: 10 July 2019

Our Ref: CL132929

NGR: 301,720 514,026

Key

• Modelled Node Point

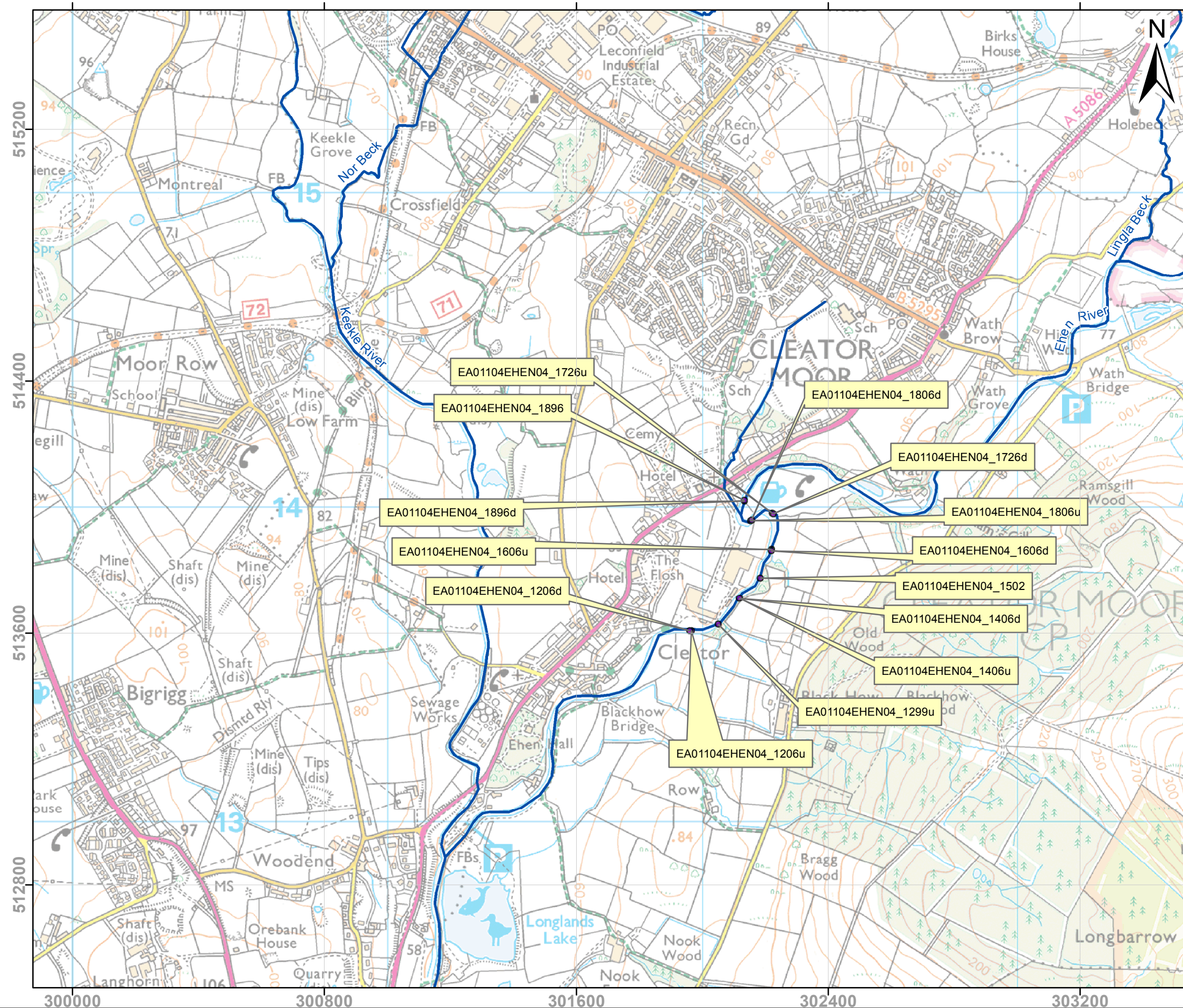
~ Main River

Flood Zone 3 shows the area that could be affected by flooding:

- from the sea with a 0.5% or greater chance of happening each year
- or from a river with a 1.0% or greater chance of happening each year.

Flood Zone 2 shows the extent of an extreme flood from rivers or the sea with up to 0.1% chance of occurring each year.

ABDs (Areas Benefiting from Defences) show the area benefiting from defences during a 0.5% tidal, or 1.0% fluvial flood event.



Modelled water levels with climate change using +20% flow allowances are not suitable for the majority of planning purposes. New climate change allowances can be checked on the following website; www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances.

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Node Point ID	Model Flood group	Return Period(Yrs)	Water Level (maod	Flow (cumecs)
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	10	62.013	85.003
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	25	62.223	101.675
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	50	62.32	111.803
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	75	62.42	122.091
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	100	62.472	127.207
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	100+CC	62.692	143.88
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	200	63.383	140.216
EA01104EHEN4_1726d	EA1104FRMEHEN2015_def	1000	63.685	173.534
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	10	62.772	67.006
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	25	62.972	101.675
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	50	63.086	111.803
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	75	63.198	122.091
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	100	63.251	127.207
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	100+CC	63.419	143.88
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	200	63.779	92.749
EA01104EHEN4_1726u	EA1104FRMEHEN2015_def	1000	64.135	100.247
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	10	63.052	77.551
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	25	63.284	86.275
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	50	63.418	89.701
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	75	63.553	91.197
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	100	63.621	91.358
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	100+CC	63.823	93.242
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	200	63.779	92.749
EA01104EHEN4_1806d	EA1104FRMEHEN2015_def	1000	64.135	100.247
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	10	63.948	76.434
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	25	64.086	85.916
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	50	64.146	90.072

EA01104EHEN4_1896	EA1104FRMEHEN2015_def	75	64.194	92.974
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	100	64.223	94.056
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	100+CC	64.291	98.815
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	200	64.015	100.488
EA01104EHEN4_1896	EA1104FRMEHEN2015_def	1000	64.152	116.027
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	10	63.74	77.543
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	25	63.852	87.567
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	50	63.898	92.126
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	75	63.941	95.293
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	100	63.972	96.513
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	100+CC	64.029	101.484
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	200	64.7	120.715
EA01104EHEN4_1896d	EA1104FRMEHEN2015_def	1000	64.939	147.259
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	10	63.052	77.551
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	25	63.284	86.275
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	50	63.418	89.701
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	75	63.553	91.197
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	100	63.621	91.358
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	100+CC	63.823	93.242
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	200	64.276	97.704
EA01104EHEN4_1806u	EA1104FRMEHEN2015_def	1000	63.754	86.424
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	10	61.545	85.032
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	25	61.765	101.24
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	50	61.882	111.013
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	75	61.994	121.169
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	100	62.052	126.737
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	100+CC	62.231	145.965
EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	200	62.192	141.565

EA01104EHEN4_1606u	EA1104FRMEHEN2015_def	1000	62.545	185.438
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	10	60.834	85.032
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	25	61.064	101.24
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	50	61.208	111.013
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	75	61.354	121.169
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	100	61.427	126.737
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	100+CC	61.666	145.965
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	200	61.61	129.311
EA01104EHEN4_1606d	EA1104FRMEHEN2015_def	1000	62.193	165.107
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	10	60.275	85.057
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	25	60.504	101.728
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	50	60.626	111.889
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	75	60.744	122.965
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	100	60.808	129.137
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	100+CC	61.001	151.25
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	200	60.953	146.021
EA01104EHEN4_1502	EA1104FRMEHEN2015_def	1000	61.398	198.323
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	10	59.892	85.08
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	25	60.118	101.697
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	50	60.224	111.657
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	75	60.379	122.255
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	100	60.451	128.097
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	100+CC	60.559	149.927
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	200	60.56	144.657
EA01104EHEN4_1406d	EA1104FRMEHEN2015_def	1000	61.039	202.596
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	10	59.892	85.08
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	25	60.118	101.697
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	50	60.244	111.657

EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	75	60.379	122.255
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	100	60.451	128.097
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	100+CC	60.599	149.927
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	200	60.953	146.021
EA01104EHEN4_1406u	EA1104FRMEHEN2015_def	1000	61.398	198.323
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	10	59.379	85.106
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	25	59.549	101.801
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	50	59.64	111.974
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	75	59.733	123.071
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	100	59.775	129.253
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	100+CC	59.912	152.206
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	200	60.56	144.657
EA01104EHEN4_1299u	EA1104FRMEHEN2015_def	1000	61.039	202.596
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	10	58.826	85.128
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	25	58.938	101.546
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	50	58.992	111.299
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	75	59.044	121.701
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	100	59.056	127.645
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	100+CC	59.075	150.014
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	200	59.88	146.482
EA01104EHEN4_1206u	EA1104FRMEHEN2015_def	1000	60.205	210.945
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	10	58.826	85.128
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	25	58.938	101.546
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	50	58.992	111.299
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	75	59.044	121.701
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	100	59.056	127.645
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	100+CC	59.075	150.014
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	200	59.071	144.439
EA01104EHEN4_1206d	EA1104FRMEHEN2015_def	1000	59.234	203.897

Node Point ID	Model Flood group	Return Period(Yrs)	Water Level (maod)	Flow (cumecs)
EA01104EHEN4_1726d	EA1104FRMEHEN2015	10	62.024	85.635
EA01104EHEN4_1726d	EA1104FRMEHEN2015	25	62.203	98.295
EA01104EHEN4_1726d	EA1104FRMEHEN2015	50	62.29	104.334
EA01104EHEN4_1726d	EA1104FRMEHEN2015	75	62.392	109.629
EA01104EHEN4_1726d	EA1104FRMEHEN2015	100	62.443	112.064
EA01104EHEN4_1726d	EA1104FRMEHEN2015	100+CC	62.208	119.508
EA01104EHEN4_1726d	EA1104FRMEHEN2015	200	62.241	140.216
EA01104EHEN4_1726d	EA1104FRMEHEN2015	1000	63.035	135.814
EA01104EHEN4_1726u	EA1104FRMEHEN2015	10	62.78	85.635
EA01104EHEN4_1726u	EA1104FRMEHEN2015	25	62.933	98.295
EA01104EHEN4_1726u	EA1104FRMEHEN2015	50	63.003	104.334
EA01104EHEN4_1726u	EA1104FRMEHEN2015	75	63.062	109.629
EA01104EHEN4_1726u	EA1104FRMEHEN2015	100	63.089	112.064
EA01104EHEN4_1726u	EA1104FRMEHEN2015	100+CC	63.17	119.508
EA01104EHEN4_1726u	EA1104FRMEHEN2015	200	63.383	118.004
EA01104EHEN4_1726u	EA1104FRMEHEN2015	1000	63.339	135.814
EA01104EHEN4_1806d	EA1104FRMEHEN2015	10	63.097	67.006
EA01104EHEN4_1806d	EA1104FRMEHEN2015	25	63.284	69.381
EA01104EHEN4_1806d	EA1104FRMEHEN2015	50	63.367	71.016
EA01104EHEN4_1806d	EA1104FRMEHEN2015	75	63.438	72.753
EA01104EHEN4_1806d	EA1104FRMEHEN2015	100	63.469	73.652
EA01104EHEN4_1806d	EA1104FRMEHEN2015	100+CC	63.563	76.122
EA01104EHEN4_1806d	EA1104FRMEHEN2015	200	63.544	75.778
EA01104EHEN4_1806d	EA1104FRMEHEN2015	1000	63.754	86.424
EA01104EHEN4_1896	EA1104FRMEHEN2015	10	63.778	64.737
EA01104EHEN4_1896	EA1104FRMEHEN2015	25	63.844	66.953
EA01104EHEN4_1896	EA1104FRMEHEN2015	50	63.887	68.838

EA01104EHEN4_1896	EA1104FRMEHEN2015	75	63.929	71.243
EA01104EHEN4_1896	EA1104FRMEHEN2015	100	63.949	72.743
EA01104EHEN4_1896	EA1104FRMEHEN2015	100+CC	64.016	78.371
EA01104EHEN4_1896	EA1104FRMEHEN2015	200	64.002	77.1
EA01104EHEN4_1896	EA1104FRMEHEN2015	1000	64.458	112.23
EA01104EHEN4_1896d	EA1104FRMEHEN2015	10	63.601	65.878
EA01104EHEN4_1896d	EA1104FRMEHEN2015	25	63.667	68.625
EA01104EHEN4_1896d	EA1104FRMEHEN2015	50	63.707	70.898
EA01104EHEN4_1896d	EA1104FRMEHEN2015	75	63.743	73.527
EA01104EHEN4_1896d	EA1104FRMEHEN2015	100	63.758	75.168
EA01104EHEN4_1896d	EA1104FRMEHEN2015	100+CC	63.805	81.063
EA01104EHEN4_1896d	EA1104FRMEHEN2015	200	63.794	79.925
EA01104EHEN4_1896d	EA1104FRMEHEN2015	1000	63.925	97.461
EA01104EHEN4_1806u	EA1104FRMEHEN2015	10	63.097	67.006
EA01104EHEN4_1806u	EA1104FRMEHEN2015	25	63.284	69.381
EA01104EHEN4_1806u	EA1104FRMEHEN2015	50	63.367	71.016
EA01104EHEN4_1806u	EA1104FRMEHEN2015	75	63.438	72.753
EA01104EHEN4_1806u	EA1104FRMEHEN2015	100	63.469	73.652
EA01104EHEN4_1806u	EA1104FRMEHEN2015	100+CC	63.563	76.122
EA01104EHEN4_1806u	EA1104FRMEHEN2015	200	63.544	75.778
EA01104EHEN4_1806u	EA1104FRMEHEN2015	1000	63.754	86.424
EA01104EHEN4_1606u	EA1104FRMEHEN2015	10	61.556	85.791
EA01104EHEN4_1606u	EA1104FRMEHEN2015	25	61.738	99.175
EA01104EHEN4_1606u	EA1104FRMEHEN2015	50	61.834	106.938
EA01104EHEN4_1606u	EA1104FRMEHEN2015	75	61.928	115.064
EA01104EHEN4_1606u	EA1104FRMEHEN2015	100	61.974	119.209
EA01104EHEN4_1606u	EA1104FRMEHEN2015	100+CC	62.107	132.378
EA01104EHEN4_1606u	EA1104FRMEHEN2015	200	62.077	129.311

EA01104EHEN4_1606u	EA1104FRMEHEN2015	1000	62.468	165.107
EA01104EHEN4_1606d	EA1104FRMEHEN2015	10	60.846	85.791
EA01104EHEN4_1606d	EA1104FRMEHEN2015	25	61.066	99.175
EA01104EHEN4_1606d	EA1104FRMEHEN2015	50	61.219	106.938
EA01104EHEN4_1606d	EA1104FRMEHEN2015	75	61.368	115.064
EA01104EHEN4_1606d	EA1104FRMEHEN2015	100	61.442	119.209
EA01104EHEN4_1606d	EA1104FRMEHEN2015	100+CC	61.658	132.378
EA01104EHEN4_1606d	EA1104FRMEHEN2015	200	61.61	141.565
EA01104EHEN4_1606d	EA1104FRMEHEN2015	1000	62.193	165.107
EA01104EHEN4_1502	EA1104FRMEHEN2015	10	60.291	85.849
EA01104EHEN4_1502	EA1104FRMEHEN2015	25	60.51	100.509
EA01104EHEN4_1502	EA1104FRMEHEN2015	50	60.632	109.947
EA01104EHEN4_1502	EA1104FRMEHEN2015	75	60.75	120.011
EA01104EHEN4_1502	EA1104FRMEHEN2015	100	60.814	125.364
EA01104EHEN4_1502	EA1104FRMEHEN2015	100+CC	60.984	143.259
EA01104EHEN4_1502	EA1104FRMEHEN2015	200	60.947	139.137
EA01104EHEN4_1502	EA1104FRMEHEN2015	1000	61.321	193.319
EA01104EHEN4_1406d	EA1104FRMEHEN2015	10	59.906	86.039
EA01104EHEN4_1406d	EA1104FRMEHEN2015	25	60.115	101.387
EA01104EHEN4_1406d	EA1104FRMEHEN2015	50	60.238	110.983
EA01104EHEN4_1406d	EA1104FRMEHEN2015	75	60.397	121.057
EA01104EHEN4_1406d	EA1104FRMEHEN2015	100	60.435	126.415
EA01104EHEN4_1406d	EA1104FRMEHEN2015	100+CC	60.562	144.742
EA01104EHEN4_1406d	EA1104FRMEHEN2015	200	60.549	140.363
EA01104EHEN4_1406d	EA1104FRMEHEN2015	1000	61.039	194.063
EA01104EHEN4_1406u	EA1104FRMEHEN2015	10	59.09	86.039
EA01104EHEN4_1406u	EA1104FRMEHEN2015	25	60.115	101.387
EA01104EHEN4_1406u	EA1104FRMEHEN2015	50	60.238	110.983

EA01104EHEN4_1406u	EA1104FRMEHEN2015	75	60.367	121.057
EA01104EHEN4_1406u	EA1104FRMEHEN2015	100	60.435	126.415
EA01104EHEN4_1406u	EA1104FRMEHEN2015	100+CC	60.562	144.742
EA01104EHEN4_1406u	EA1104FRMEHEN2015	200	60.549	140.363
EA01104EHEN4_1406u	EA1104FRMEHEN2015	1000	60.998	194.063
EA01104EHEN4_1299u	EA1104FRMEHEN2015	10	59.39	86.067
EA01104EHEN4_1299u	EA1104FRMEHEN2015	25	59.547	101.558
EA01104EHEN4_1299u	EA1104FRMEHEN2015	50	59.634	111.404
EA01104EHEN4_1299u	EA1104FRMEHEN2015	75	59.725	121.991
EA01104EHEN4_1299u	EA1104FRMEHEN2015	100	59.767	127.705
EA01104EHEN4_1299u	EA1104FRMEHEN2015	100+CC	59.881	1146.854
EA01104EHEN4_1299u	EA1104FRMEHEN2015	200	59.854	142.423
EA01104EHEN4_1299u	EA1104FRMEHEN2015	1000	60.162	201.548
EA01104EHEN4_1206u	EA1104FRMEHEN2015	10	58.833	86.088
EA01104EHEN4_1206u	EA1104FRMEHEN2015	25	58.937	101.308
EA01104EHEN4_1206u	EA1104FRMEHEN2015	50	58.989	110.761
EA01104EHEN4_1206u	EA1104FRMEHEN2015	75	59.039	120.695
EA01104EHEN4_1206u	EA1104FRMEHEN2015	100	59.059	126.069
EA01104EHEN4_1206u	EA1104FRMEHEN2015	100+CC	59.088	144.551
EA01104EHEN4_1206u	EA1104FRMEHEN2015	200	59.08	140.338
EA01104EHEN4_1206u	EA1104FRMEHEN2015	1000	59.218	195.285
EA01104EHEN4_1206d	EA1104FRMEHEN2015	10	58.833	86.088
EA01104EHEN4_1206d	EA1104FRMEHEN2015	25	58.937	101.308
EA01104EHEN4_1206d	EA1104FRMEHEN2015	50	58.989	110.761
EA01104EHEN4_1206d	EA1104FRMEHEN2015	75	59.039	120.695
EA01104EHEN4_1206d	EA1104FRMEHEN2015	100	59.059	126.069
EA01104EHEN4_1206d	EA1104FRMEHEN2015	100+CC	59.088	144.551
EA01104EHEN4_1206d	EA1104FRMEHEN2015	200	59.08	140.338
EA01104EHEN4_1206d	EA1104FRMEHEN2015	1000	59.218	195.285

Historic Flood Map: Cleator Mills, Cleator, CA23 3DU

Produced: 09 July 2019

Our Ref: CL132929

NGR: 301,526 513,720

Key



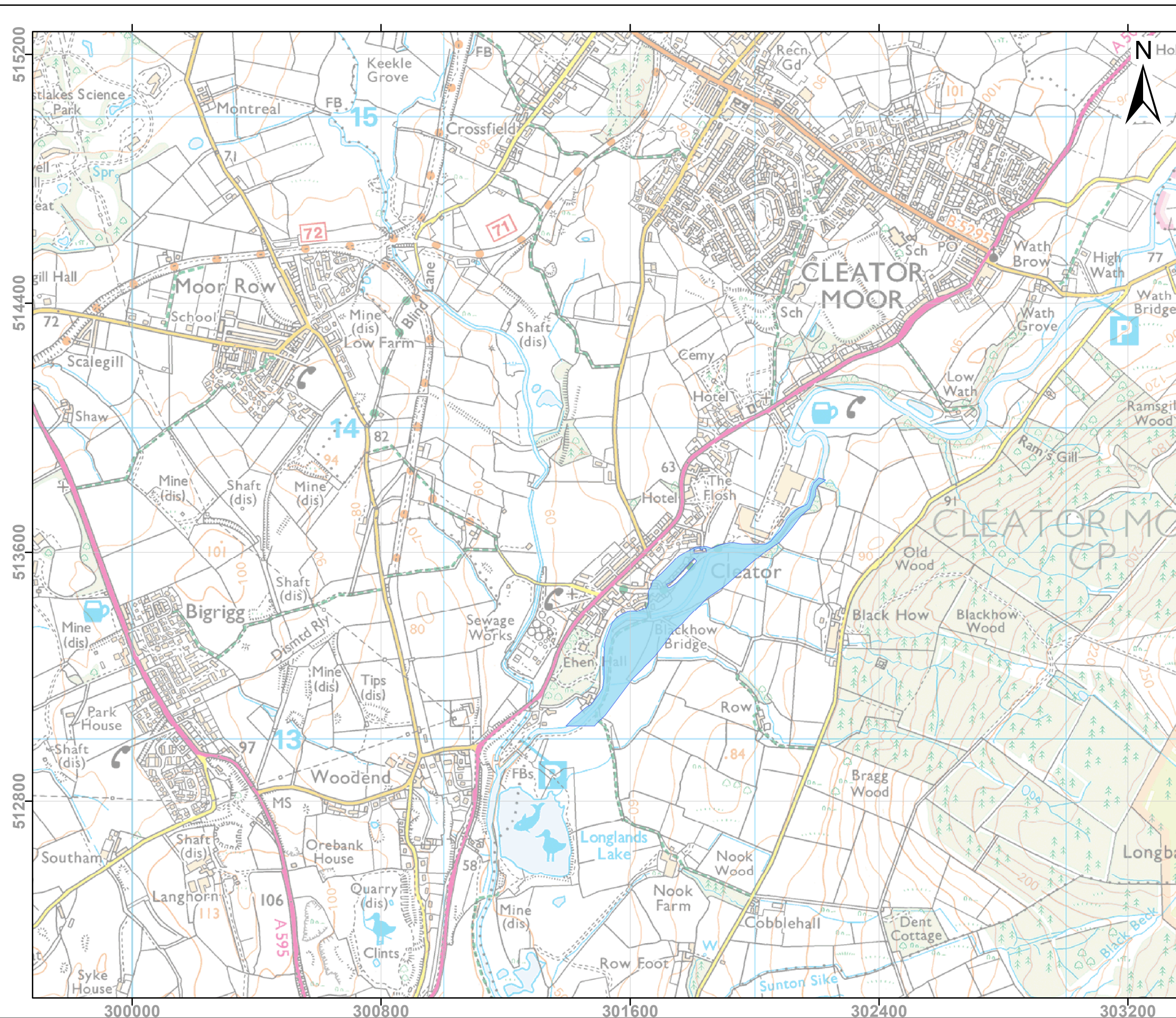
November 2009 Recorded Flood
Outline

Flood Zone 3 shows the area that could be affected by flooding:

- from the sea with a 0.5% or greater chance of happening each year
- or from a river with a 1.0% or greater chance of happening each year.

Flood Zone 2 shows the extent of an extreme flood from rivers or the sea with up to 0.1% chance of occurring each year.

ABDs (Areas Benefiting from Defences) show the area benefiting from defences during a 0.5% tidal, or 1.0% fluvial flood event.



Modelled water levels with climate change using +20% flow allowances are not suitable for the majority of planning purposes. New climate change allowances can be checked on the following website; www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances.

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Contact Us: National Customer Contact Centre, PO Box 544, Rotherham, S60 1BY. Tel: 03708 506 506 (Mon-Fri 8-6). Email: enquiries@environment-agency.gov.uk

Historic Flood Map: Cleator Mills, Cleator, CA23 3DU

Produced: 09 July 2019

Our Ref: CL132929

NGR: 301,526 513,720

Key



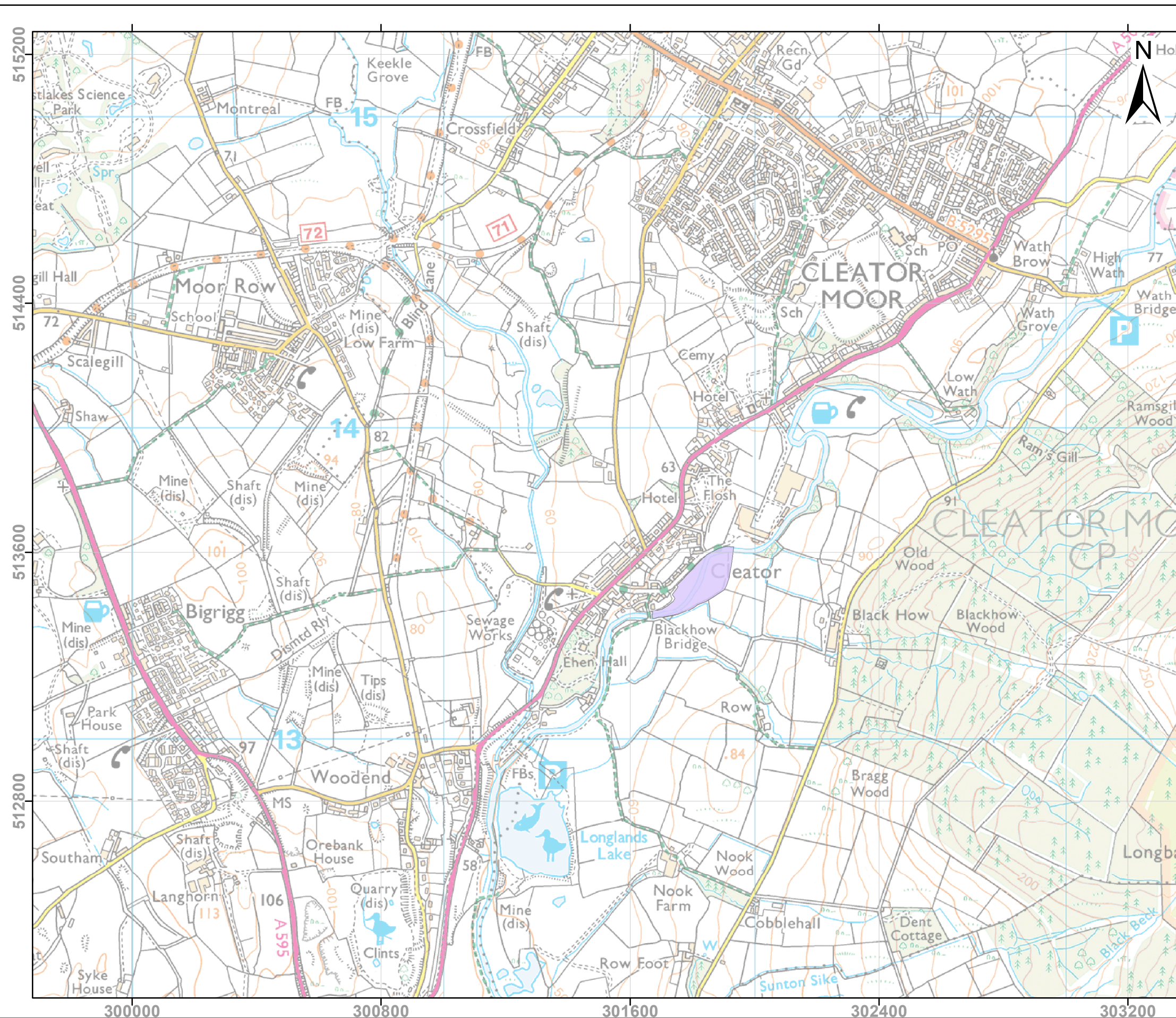
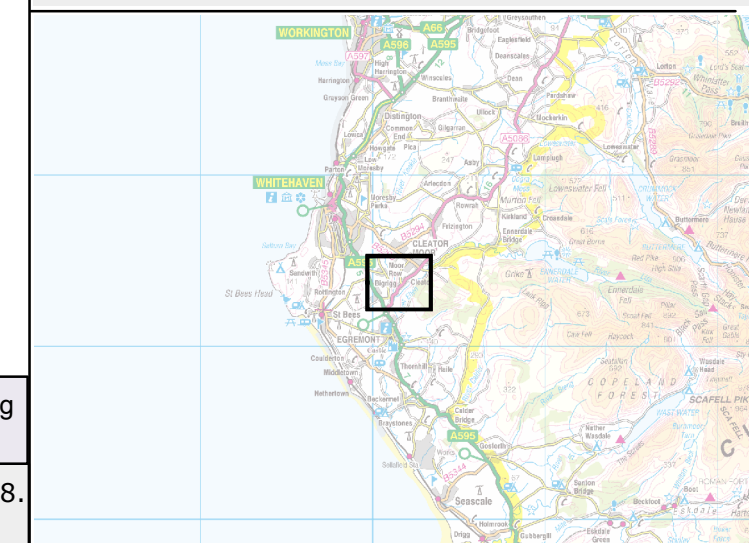
October 2017 Recorded Flood
Outline

Flood Zone 3 shows the area that could be affected by flooding:

- from the sea with a 0.5% or greater chance of happening each year
- or from a river with a 1.0% or greater chance of happening each year.

Flood Zone 2 shows the extent of an extreme flood from rivers or the sea with up to 0.1% chance of occurring each year.

ABDs (Areas Benefiting from Defences) show the area benefiting from defences during a 0.5% tidal, or 1.0% fluvial flood event.



Modelled water levels with climate change using +20% flow allowances are not suitable for the majority of planning purposes. New climate change allowances can be checked on the following website; www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances.

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Contact Us: National Customer Contact Centre, PO Box 544, Rotherham, S60 1BY. Tel: 03708 506 506 (Mon-Fri 8-6). Email: enquiries@environment-agency.gov.uk

Appendix H Topographical Survey



KEY

LINE TYPES

- VERGE
- FENCE - CHAIN LINK
- FENCE - METAL
- FENCE - WOODEN
- FENCE - POST & RAIL
- WALL
- BARRIER
- CHANNEL LINE

CONCRETE EDGE

FOOTPATH

ROAD

BUILDING

TREE

GATE

SURVEY STATION

EAVES

UTILITY KEY

	BT BELOW GROUND		WATER BELOW GROUND
	BT ABOVE GROUND		WATER ABOVE GROUND
	BT ASSUMED ROUTE		WATER ASSUMED ROUTE
	CATV BELOW GROUND		UNKNOWN BELOW GROUND
	CATV ABOVE GROUND		UNKNOWN ABOVE GROUND
	CATV ASSUMED ROUTE		GPI BELOW GROUND
	COMMER BELOW GROUND		COMBINED WATER SEWER
	COMMER ABOVE GROUND		ASSUMED COMBINED WATER SEWER ROUTE
	COMMER ASSUMED ROUTE		FQAL WATER SEWER
	GAS BELOW GROUND		ASSUMED FQAL WATER SEWER ROUTE
	GAS ABOVE GROUND		STORM WATER SEWER
	GAS ASSUMED ROUTE		ASSUMED STORM WATER SEWER ROUTE
	ELECTRIC BELOW GROUND		REPRESENTATION SCAR
	ELECTRIC ABOVE GROUND		SURVEY BOUNDARY
	ELECTRIC ASSUMED ROUTE		

ABBREVIATIONS		INTERCEPTOR	
AS21	ASSIGNED CONNECTION	INT	INTERCEPTOR
AX	AXIAL	INT-1	INTERCEPTOR
AXU	AXIALS UNIT	LAB	LABORATORY
AB	ABOVE HORIZON	LAB-1	LABORATORY
ABCS	ABORTS CEMENT	LAB-2	LABORATORY
ABV	ABOVE VOLUME	LAB-3	LABORATORY
BD	BELOW RANGE	LV	LOW VOLTAGE
BD	BELOW RANGE	LV-1	LOW VOLTAGE
BD	BELOW RANGE	LV-2	LOW VOLTAGE
BD	BELOW RANGE	LV-3	LOW VOLTAGE
BD	BELOW RANGE	LV-4	LOW VOLTAGE
BD	BELOW RANGE	LV-5	LOW VOLTAGE
BD	BELOW RANGE	LV-6	LOW VOLTAGE
BD	BELOW RANGE	LV-7	LOW VOLTAGE
BD	BELOW RANGE	LV-8	LOW VOLTAGE
BD	BELOW RANGE	LV-9	LOW VOLTAGE
BD	BELOW RANGE	LV-10	LOW VOLTAGE
BD	BELOW RANGE	LV-11	LOW VOLTAGE
BD	BELOW RANGE	LV-12	LOW VOLTAGE
BD	BELOW RANGE	LV-13	LOW VOLTAGE
BD	BELOW RANGE	LV-14	LOW VOLTAGE
BD	BELOW RANGE	LV-15	LOW VOLTAGE
BD	BELOW RANGE	LV-16	LOW VOLTAGE
BD	BELOW RANGE	LV-17	LOW VOLTAGE
BD	BELOW RANGE	LV-18	LOW VOLTAGE
BD	BELOW RANGE	LV-19	LOW VOLTAGE
BD	BELOW RANGE	LV-20	LOW VOLTAGE
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BD	BELOW RANGE	LV-22	LOW VOLTAGE
BD	BELOW RANGE	LV-23	LOW VOLTAGE
BD	BELOW RANGE	LV-24	LOW VOLTAGE
BD	BELOW RANGE	LV-25	LOW VOLTAGE
BD	BELOW RANGE	LV-26	LOW VOLTAGE
BD	BELOW RANGE	LV-27	LOW VOLTAGE
BD	BELOW RANGE	LV-28	LOW VOLTAGE
BD	BELOW RANGE	LV-29	LOW VOLTAGE
BD	BELOW RANGE	LV-30	LOW VOLTAGE
BD	BELOW RANGE	LV-31	LOW VOLTAGE
BD	BELOW RANGE	LV-32	LOW VOLTAGE
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BD	BELOW RANGE	LV-36	LOW VOLTAGE
BD	BELOW RANGE	LV-37	LOW VOLTAGE
BD	BELOW RANGE	LV-38	LOW VOLTAGE
BD	BELOW RANGE	LV-39	LOW VOLTAGE
BD	BELOW RANGE	LV-40	LOW VOLTAGE
BD	BELOW RANGE	LV-41	LOW VOLTAGE
BD	BELOW RANGE	LV-42	LOW VOLTAGE
BD	BELOW RANGE	LV-43	LOW VOLTAGE
BD	BELOW RANGE	LV-44	LOW VOLTAGE
BD	BELOW RANGE	LV-45	LOW VOLTAGE
BD	BELOW RANGE	LV-46	LOW VOLTAGE
BD	BELOW RANGE	LV-47	LOW VOLTAGE
BD	BELOW RANGE	LV-48	LOW VOLTAGE
BD	BELOW RANGE	LV-49	LOW VOLTAGE
BD	BELOW RANGE	LV-50	LOW VOLTAGE
BD	BELOW RANGE	LV-51	LOW VOLTAGE
BD	BELOW RANGE	LV-52	LOW VOLTAGE
BD	BELOW RANGE	LV-53	LOW VOLTAGE
BD	BELOW RANGE	LV-54	LOW VOLTAGE
BD	BELOW RANGE	LV-55	LOW VOLTAGE
BD	BELOW RANGE	LV-56	LOW VOLTAGE
BD	BELOW RANGE	LV-57	LOW VOLTAGE
BD	BELOW RANGE	LV-58	LOW VOLTAGE
BD	BELOW RANGE	LV-59	LOW VOLTAGE
BD	BELOW RANGE	LV-60	LOW VOLTAGE
BD	BELOW RANGE	LV-61	LOW VOLTAGE
BD	BELOW RANGE	LV-62	LOW VOLTAGE
BD	BELOW RANGE	LV-63	LOW VOLTAGE
BD	BELOW RANGE	LV-64	LOW VOLTAGE
BD	BELOW RANGE	LV-65	LOW VOLTAGE
BD	BELOW RANGE	LV-66	LOW VOLTAGE
BD	BELOW RANGE	LV-67	LOW VOLTAGE
BD	BELOW RANGE	LV-68	LOW VOLTAGE
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BD	BELOW RANGE	LV-70	LOW VOLTAGE
BD	BELOW RANGE	LV-71	LOW VOLTAGE
BD	BELOW RANGE	LV-72	LOW VOLTAGE
BD	BELOW RANGE	LV-73	LOW VOLTAGE
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BD	BELOW RANGE	LV-77	LOW VOLTAGE
BD	BELOW RANGE	LV-78	LOW VOLTAGE
BD	BELOW RANGE	LV-79	LOW VOLTAGE
BD	BELOW RANGE	LV-80	LOW VOLTAGE
BD	BELOW RANGE	LV-81	LOW VOLTAGE
BD	BELOW RANGE	LV-82	LOW VOLTAGE
BD	BELOW RANGE	LV-83	LOW VOLTAGE
BD	BELOW RANGE	LV-84	LOW VOLTAGE
BD	BELOW RANGE	LV-85	LOW VOLTAGE
BD	BELOW RANGE	LV-86	LOW VOLTAGE
BD	BELOW RANGE	LV-87	LOW VOLTAGE
BD	BELOW RANGE	LV-88	LOW VOLTAGE
BD	BELOW RANGE	LV-89	LOW VOLTAGE
BD	BELOW RANGE	LV-90	LOW VOLTAGE
BD	BELOW RANGE	LV-91	LOW VOLTAGE
BD	BELOW RANGE	LV-92	LOW VOLTAGE
BD	BELOW RANGE	LV-93	LOW VOLTAGE
BD	BELOW RANGE	LV-94	LOW VOLTAGE
BD	BELOW RANGE	LV-95	LOW VOLTAGE
BD	BELOW RANGE	LV-96	LOW VOLTAGE
BD	BELOW RANGE	LV-97	LOW VOLTAGE
BD	BELOW RANGE	LV-98	LOW VOLTAGE
BD	BELOW RANGE	LV-99	LOW VOLTAGE
BD	BELOW RANGE	LV-100	LOW VOLTAGE

DISCLAIMER

Unless otherwise stated, all services shown on this plan have been surveyed using approved detectors and the connections between manholes, if not traced, are assumed to be direct.

No guarantee can be given that all services have been shown.

Utilities traced using GPR techniques show depths approximately from ground level to the top of the utility. Utilities traced using Electromagnetic techniques provide an estimated depth which is measured from ground level to the centre of the utility. Drainage and water mains (water, sewage, stormwater, etc.) are not detected. All information is displayed on a computer screen.

Where services are shown as 'Taken From Records' on the drawing we are not liable for any loss that may arise due to a lack of accuracy in that guided information.

Reference should be made to the methodology used on site as detailed within the latest version of SiteScan Procedures for Utility Inspection Surveys.

SiteScan recommend that all excavations are to be carried out in accordance with HSG 47 (Avoiding Danger from Underground Services).

Plan accuracies of the order of + or - 150mm may be achieved but this figure will depend on the depth of the service below ground level. Where similar services run in close proximity, separation may be impossible. Successful tracing of non-metallic pipes may be limited.

Existing record information showing underground services is often incomplete and of doubtful accuracy. It should be regarded only as an indication and cannot be guaranteed.

NOTES

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REV	AMENDMENT	DRAWN	CHECKED
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SITESCAN

Vita House, Fish Quay, North Shields, Tyne & Wear, NE30 1JA
www.sitescanltd.com info@sitescanltd.com
Tel: 0191 2572911

RWO

CLIENT

KANGOL FACTORY
CLEATER

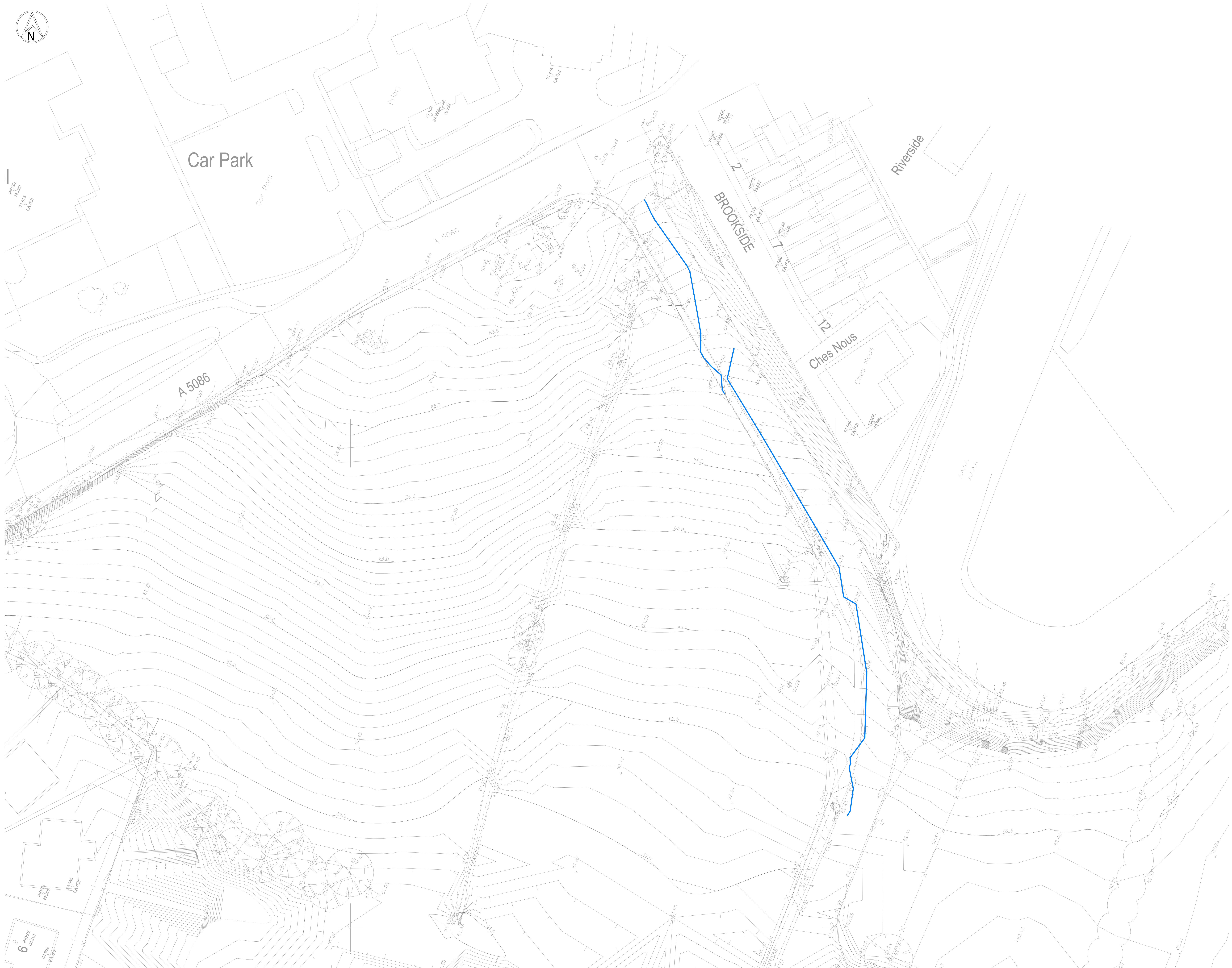
PROJECT TITLE

DRAINAGE SURVEY

ADDRESS AND CITY

NTS		JUN 2013			
SCALE P. 20		DATE		ORIENTATION	
JRD		JRD		NC	
SURVEYED BY		DRAWN BY		APPROVED	
CLE/RWO/DRAIN				1 of 1	A
PROJECT NO.				SHEET NO.	REV.

Appendix I Overland Flow Route



KEY



Date	Revisions	Drawn	Checked	Rev
09/04/2021				
INFORMATION				
NORTH EAST 0191 256632				
YORKSHIRE 0113 335 3500				
Client GLEESON HOMES				
Project CLEATOR MILLS				
Title OVERLAND FLOW ROUTE PLAN				
DO NOT SCALE	Scale @ A3: 1:200	Drawn: AGM	Checked:	Date: 12.07.2021
Job No: 19002	Drawn No: SK003	Rev:		

Appendix J Soil Infiltration Test Results



GEO

Environmental Engineering

FAO Ross Oakley
RWO Associates Ltd
6A
Union Quay
North Shields
NE30 1HJ

****Sent by Email****

21st October 2013

Dear Ross,

Re: Land at Cleator Mills – Soakaway Test Letter Report

Please find attached to this letter the following information:

- Exploratory Hole Location Plan (TP01 to TP06)
- Trial Pit Logs
- Soakaway Test Workbook Extracts (SA01 to SA06 inclusive)

From the trial pit logs it can be seen that the ground conditions typically comprised grass and topsoil over sand and gravel with many cobbles and boulders to the terminal depths of the trial pits between c.1.50m and c.2.00m below current ground levels. No water ingress was noted within the trial pits, although the sand and gravel materials were generally unstable with the materials posing a risk of sidewall collapse.

As requested in-situ soakaway tests were undertaken at the six trial pit locations at depths varying between c.0.50m and c.2.00m below ground levels. All the trial pits successfully drained completely within 2 hours of commencing the tests.

I trust the above and attached is to your satisfaction and if you have any questions or then please call or email.

Yours Faithfully

.....
Curtis R. Evans *B.Sc (Hons) FGS*

Director

For and On Behalf Of Geo Environmental Engineering Ltd

Visit our *NEW* Website: www.geoenvironmentalengineering.com Email: info@geoenvironmentalengineering.com

Tel: 08456 768 895, Mob: 07883 440 186

“Without Site Investigation Ground is a Hazard”

Site Investigation Steering Group (SISG), 1993

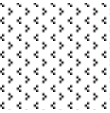
GEO Environmental Engineering Ltd
North West (Registered Office):
4 Culgarth Avenue, Cockermouth, Cumbria CA13 9PL
North East:
6A Union Quay, North Shields, Tyne & Wear NE30 1HJ

Telephone: 08456 768 895
Email: info@geoenvironmentalengineering.com
Website: www.geoenvironmentalengineering.com
Company No.: 07180338
VAT No.: GB 986617072

GEO2013-776: Exploratory Hole Location Plan (Approximate Locations – Not to Scale)



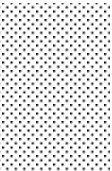
GEO2013-776: TP01

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.40	TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets.		
0.40	2.00	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		0.50m Soakaway Test (results on SA01)
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.1.50m Soakaway test completed from c.0.50m to c.1.50m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

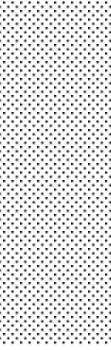
GEO2013-776: TP02

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.30	TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets.		
0.30	0.70	Red brown slightly gravelly SAND.		
0.70	2.00	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		1.00m Soakaway Test (results on SA02)
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.1.50m Soakaway test completed from c.1.00m to c.2.00m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

GEO2013-776: TP03

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.20	TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets.		
0.20	0.80	Red brown slightly gravelly SAND.		
0.80	2.00	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		1.00m Soakaway Test (results on SA03)
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.0.80m Soakaway test completed from c.1.00m to c.2.00m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

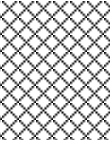
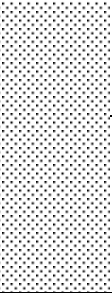
GEO2013-776: TP04

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.30	TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets.		
0.30	1.50	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		0.50m Soakaway Test (results on SA04)
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.1.00m Soakaway test completed from c.0.50m to c.1.50m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

GEO2013-776: TP05

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.35	TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets.		
0.35	0.60	Red brown slightly gravelly SAND.		
0.60	2.00	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		1.00m Soakaway Test (results on SA05)
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.1.50m Soakaway test completed from c.1.00m to c.2.00m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

GEO2013-776: TP06

Depth From (m)	Depth To (m)	Strata Description	Legend	Testing / Samples
0.00	0.50	MADE GROUND: TURF over TOPSOIL: Grass over dark brown sandy gravelly clayey topsoil with some rootlets and rare brick pieces.		
0.50	0.90	Red brown slightly gravelly SAND.		0.50m Soakaway Test (results on SA06)
0.90	1.50	Medium dense appearing reddish brown SAND and GRAVEL. Many cobbles and boulders noted throughout.		
		End of trial pit Trial pit remained dry on completion Trial pit noted as unstable below c.1.00m Soakaway test completed from c.0.50m to c.1.50m		
Site: Land at Cleator Mills Client Reference: N/A Engineer: CE Plant: JCB3CX		Log Notes: Spt = Standard Penetration test (blows per 300mm n300) HSV = Hand Shear Vane (result in kN/m ²) CBR = California Bearing Ratio by Mexe Cone Penetrometer (result as percentage) LP = Limited Penetration (HSV/CBR) NP = No penetration (HSV/CBR) B = Bulk Bag, J = Amber Glass Jar, T = Plastic Tub		

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
DATE	21-Oct-13	CHECKED BY	CRE/GE
		REV	P1

REF										OUTPUT										
Calculation of soil infiltration rate in accordance with BRE Digest 365																				
Length of trial pit				=	L_{TP}		=	3.000 m												
Width of trial pit				=	W_{TP}		=	0.450 m												
Effective Depth				=	D_{TP}		=	1.500 m		(measured below incoming invert)										
75% Effective Depth of trial pit				=	D_{75}		=	($D_{TP} \times 0.75$)		=	1.125 m									
50% Effective Depth of trial pit				=	D_{50}		=	($D_{TP} \times 0.50$)		=	0.750 m									
25% Effective Depth of trial pit				=	D_{25}		=	($D_{TP} \times 0.25$)		=	0.375 m									
Pit Voids				=	PV		=	100 %		(For open pits, PV = 100%. For stone filled pits, PV = 30%)										
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth																				
Test No 1		time to fall from 75% to 25% eff depth						=	T_1		=	40.0 mins								
Test No 2		time to fall from 75% to 25% eff depth						=	T_2		=	mins								
Test No 3		time to fall from 75% to 25% eff depth						=	T_3		=	mins								
TAKE THE LONGEST OF THE 3 TESTS ABOVE								=	T_L		=	40.0 mins								
Volume of water escaping during this test between D_{75} and D_{25}																				
				=	V_{TP75_25}		=	($L_{TP} \times W_{TP} \times (D_{75} - D_{25}) \times PV$)		=	1.013 cu m.									
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.																				
ie		A_{P50}		= (Wet Base Area + 50% of Wet Sides Area)																
		A_{P50}		= ($L_{TP} \times W_{TP}$) + ($2L_{TP} + 2W_{TP}$) $\times D_{50}$																
		A_{P50}		= 1.350 + 5.175																
				A_{P50}		= 6.525 sq m														
Soil Infiltration Rate				=	f		=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$		m/s										
Soil Infiltration Rate = f = 6.46552E-05 m/s																				
Notes: Pit drained completely within 40 minutes.																				

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
DATE	21-Oct-13	CHECKED BY	CRE/GE
		REV	P1

REF											OUTPUT
Calculation of soil infiltration rate in accordance with BRE Digest 365											
Length of trial pit	=	L_{TP}	=	2.000	m						
Width of trial pit	=	W_{TP}	=	0.450	m						
Effective Depth	=	D_{TP}	=	2.000	m	(measured below incoming invert)					
75% Effective Depth of trial pit	=	D_{75}	=	($D_{TP} \times 0.75$)	=	1.500	m				
50% Effective Depth of trial pit	=	D_{50}	=	($D_{TP} \times 0.50$)	=	1.000	m				
25% Effective Depth of trial pit	=	D_{25}	=	($D_{TP} \times 0.25$)	=	0.500	m				
Pit Voids	=	PV	=	100	%	(For open pits, PV = 100%. For stone filled pits, PV = 30%)					
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth											
Test No 1	time to fall from 75% to 25% eff depth	=	T_1	=	52.0	mins					
Test No 2	time to fall from 75% to 25% eff depth	=	T_2	=		mins					
Test No 3	time to fall from 75% to 25% eff depth	=	T_3	=		mins					
TAKE THE LONGEST OF THE 3 TESTS ABOVE			=	T_L	=	52.0	mins				
Volume of water escaping during this test between D_{75} and D_{25}											
	=	V_{TP75_25}	=	($L_{TP} \times W_{TP} \times (D_{75} - D_{25}) \times PV$)	=	0.900	cu m.				
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.											
ie	A_{P50}	=	(Wet Base Area + 50% of Wet Sides Area)								
	A_{P50}	=	($L_{TP} \times W_{TP}$)	+	($2L_{TP} + 2W_{TP}$) $\times D_{50}$						
	A_{P50}	=	0.900	+	4.900						
			A_{P50}	=	5.800	sq m					
Soil Infiltration Rate	=	f	=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$	m/s						
Soil Infiltration Rate = f = 4.97347E-05 m/s											
Notes: Pit drained completely within 52 minutes.											

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
SHEET No	SA 03	CHECKED BY	CRE/GE
DATE	21-Oct-13	REV	P1

REF										OUTPUT									
Calculation of soil infiltration rate in accordance with BRE Digest 365																			
Length of trial pit		=	L_{TP}		=	2.500 m													
Width of trial pit		=	W_{TP}		=	0.500 m													
Effective Depth		=	D_{TP}		=	2.000 m		(measured below incoming invert)											
75% Effective Depth of trial pit		=	D_{75}		=	$(D_{TP} \times 0.75)$		=	1.500 m										
50% Effective Depth of trial pit		=	D_{50}		=	$(D_{TP} \times 0.50)$		=	1.000 m										
25% Effective Depth of trial pit		=	D_{25}		=	$(D_{TP} \times 0.25)$		=	0.500 m										
Pit Voids		=	PV		=	100 %		(For open pits, PV = 100%. For stone filled pits, PV = 30%)											
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth																			
Test No 1		time to fall from 75% to 25% eff depth			=	T_1		=	120.0 mins										
Test No 2		time to fall from 75% to 25% eff depth			=	T_2		=	mins										
Test No 3		time to fall from 75% to 25% eff depth			=	T_3		=	mins										
TAKE THE LONGEST OF THE 3 TESTS ABOVE					=	T_L		=	120.0 mins										
Volume of water escaping during this test between D_{75} and D_{25}																			
		=	V_{TP75_25}		=	$(L_{TP} \times W_{TP} \times (D_{75} - D_{25}) \times PV)$		=	1.250 cu m.										
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.																			
ie		A_{P50}		=	(Wet Base Area + 50% of Wet Sides Area)														
		A_{P50}		=	$(L_{TP} \times W_{TP})$		+	$(2L_{TP} + 2W_{TP}) \times D_{50}$											
		A_{P50}		=	1.250		+	6.000											
				A_{P50}		=	7.250		sq m										
Soil Infiltration Rate		=	f		=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$		m/s											
Soil Infiltration Rate = f = 2.39464E-05 m/s																			
Notes: Pit drained completely within 120 minutes.																			

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
DATE	21-Oct-13	CHECKED BY	CRE/GE
		REV	P1

REF										OUTPUT										
Calculation of soil infiltration rate in accordance with BRE Digest 365																				
Length of trial pit				=	L_{TP}		=	2.600 m												
Width of trial pit				=	W_{TP}		=	0.500 m												
Effective Depth				=	D_{TP}		=	1.500 m		(measured below incoming invert)										
75% Effective Depth of trial pit				=	D_{75}		=	(D_{TP} x 0.75)		=	1.125 m									
50% Effective Depth of trial pit				=	D_{50}		=	(D_{TP} x 0.50)		=	0.750 m									
25% Effective Depth of trial pit				=	D_{25}		=	(D_{TP} x 0.25)		=	0.375 m									
Pit Voids				=	PV		=	100 %		(For open pits, PV = 100%. For stone filled pits, PV = 30%)										
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth																				
Test No 1		time to fall from 75% to 25% eff depth						=	T_1		=	120.0 mins								
Test No 2		time to fall from 75% to 25% eff depth						=	T_2		=	mins								
Test No 3		time to fall from 75% to 25% eff depth						=	T_3		=	mins								
TAKE THE LONGEST OF THE 3 TESTS ABOVE								=	T_L		=	120.0 mins								
Volume of water escaping during this test between D_{75} and D_{25}																				
				=	V_{TP75_25}		=	(L_{TP} x W_{TP} x (D_{75} - D_{25}) x PV)		=	0.975 cu m.									
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.																				
ie		A_{P50}		=	(Wet Base Area + 50% of Wet Sides Area)															
		A_{P50}		=	(L_{TP} x W_{TP})		+	($2L_{TP}$ + $2W_{TP}$) x D_{50}												
		A_{P50}		=	1.300		+	4.650												
				A_{P50}		=	5.950		sq m											
Soil Infiltration Rate				=	f		=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$		m/s										
Soil Infiltration Rate = f = 2.27591E-05 m/s																				
Notes: Pit drained completely within 120 minutes.																				

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
DATE	21-Oct-13	CHECKED BY	CRE/GE
		REV	P1

REF										OUTPUT									
Calculation of soil infiltration rate in accordance with BRE Digest 365																			
Length of trial pit					=	L_{TP}		=	2.700 m										
Width of trial pit					=	W_{TP}		=	0.450 m										
Effective Depth					=	D_{TP}		=	2.000 m		(measured below incoming invert)								
75% Effective Depth of trial pit					=	D_{75}		=	($D_{TP} \times 0.75$)		=	1.500 m							
50% Effective Depth of trial pit					=	D_{50}		=	($D_{TP} \times 0.50$)		=	1.000 m							
25% Effective Depth of trial pit					=	D_{25}		=	($D_{TP} \times 0.25$)		=	0.500 m							
Pit Voids					=	PV		=	100 %		(For open pits, PV = 100%. For stone filled pits, PV = 30%)								
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth																			
Test No 1		time to fall from 75% to 25% eff depth					=	T_1		=	120.0 mins								
Test No 2		time to fall from 75% to 25% eff depth					=	T_2		=	mins								
Test No 3		time to fall from 75% to 25% eff depth					=	T_3		=	mins								
TAKE THE LONGEST OF THE 3 TESTS ABOVE					=	T_L		=	120.0 mins										
Volume of water escaping during this test between D_{75} and D_{25}																			
					=	V_{TP75_25}		=	($L_{TP} \times W_{TP} \times (D_{75} - D_{25}) \times PV$)		=	1.215 cu m.							
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.																			
ie		A_{P50}		= (Wet Base Area + 50% of Wet Sides Area)															
		A_{P50}		= ($L_{TP} \times W_{TP}$) + ($2L_{TP} + 2W_{TP}$) $\times D_{50}$															
		A_{P50}		= 1.215 + 6.300															
				A_{P50}		= 7.515 sq m													
Soil Infiltration Rate					=	f		=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$		m/s								
Soil Infiltration Rate = f = 2.24551E-05 m/s																			
Notes: Pit drained completely within 120 minutes.																			

CALCULATIONS/SKETCHES

PROJECT GEO2013-776 Land at Cleator Mills			
JOB No	2013-776	PREPARED BY	CRE
SHEET No	SA 06	CHECKED BY	CRE/GE
DATE	21-Oct-13	REV	P1

REF											OUTPUT
Calculation of soil infiltration rate in accordance with BRE Digest 365											
Length of trial pit	=	L_{TP}	=	2.500	m						
Width of trial pit	=	W_{TP}	=	0.450	m						
Effective Depth	=	D_{TP}	=	1.500	m	(measured below incoming invert)					
75% Effective Depth of trial pit	=	D_{75}	=	(D_{TP} x 0.75)	=	1.125	m				
50% Effective Depth of trial pit	=	D_{50}	=	(D_{TP} x 0.50)	=	0.750	m				
25% Effective Depth of trial pit	=	D_{25}	=	(D_{TP} x 0.25)	=	0.375	m				
Pit Voids	=	PV	=	100	%	(For open pits, PV = 100%. For stone filled pits, PV = 30%)					
Carry out 3 tests, each measuring the time taken for water levels to fall from 75% effective depth to 25% effective depth											
Test No 1	time to fall from 75% to 25% eff depth	=	T_1	=	60.0	mins					
Test No 2	time to fall from 75% to 25% eff depth	=	T_2	=		mins					
Test No 3	time to fall from 75% to 25% eff depth	=	T_3	=		mins					
TAKE THE LONGEST OF THE 3 TESTS ABOVE			=	T_L	=	60.0	mins				
Volume of water escaping during this test between D_{75} and D_{25}											
	=	V_{TP75_25}	=	(L_{TP} x W_{TP} x (D_{75} - D_{25}) x PV)	=	0.844	cu m.				
The mean surface area through which the above volume escapes, is the <i>wetted area</i> . Only 50% of the effective depth is allowed in the calculation.											
ie	A_{P50}	=	(Wet Base Area + 50% of Wet Sides Area)								
	A_{P50}	=	(L_{TP} x W_{TP})	+	($2L_{TP}$ + $2W_{TP}$) x D_{50}						
	A_{P50}	=	1.125	+	4.425						
			A_{P50}	=	5.550	sq m					
Soil Infiltration Rate	=	f	=	$\frac{V_{TP75_25}}{A_{P50} \times 60 \times T_L}$	m/s						
Soil Infiltration Rate = f = 4.22297E-05 m/s											
Notes: Pit drained completely within 60 minutes.											



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